

Contract NAS9-14318

User's Manual

Appendix H UNIVAC EXEC 8 EDITION

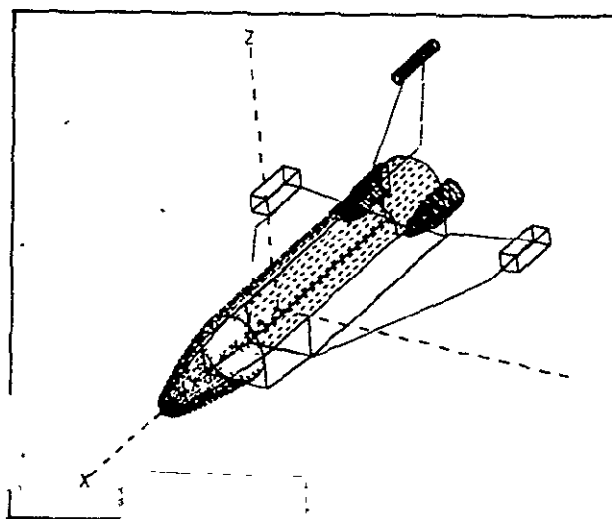
Sample Problems

JUNE 1978

NASA CR-

151825

Thermal Radiation Analysis System TRASYS II



(NASA-CR-151825): THERMAL RADIATION ANALYSIS
SYSTEM (TRASYS 2). USER'S MANUAL: APPENDIX
H: UNIVAC EXEC 8 EDITION: SAMPLE PROBLEMS/
(Martin Marietta Corp.) 455 f

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Unclas
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MARTIN MARIETTA

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APPENDIX H

Sample problems run on the NASA/JSC Univac 1110, Exec 8 system.

This entire section has been changed for Revision 1.

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Original (non-restart) run.

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(Restart, with source editing.)

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(No source editing.)

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SAMPLE CASE 1

-BED,R VOGT0.CASE1
 FILE IN FIELD 1 DISABLED---ACCEPTED
 FILE IN FIELD 1 IN USE BY ANOTHER RUN
 READ-ONLY MODE
 CASE UPPER ASSUMED
 ED 14.02-06/22-20:26-(0,)
 EDIT

1:0RUN,R/R RYMH01.3248-F261-C,ES3-N03711.07.150 NO DECK VOGT
 10:0ADD ES3-TRASYS°TRASYS.STARTH
 11:0SETC 0100
 12:0ADD PREPRO
 13:HEADER OPTIONS DATA
 14:TITLE SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/0BCAL/RKCAL - ORIGINAL RUN
 15: MODEL = SAMPLE
 16: RSO = RSTSAMI
 17:HEADER SURFACE DATA
 18:C
 19:C-----THIS SURFACE DATA BLOCK IS USED IN SAMPLE CASES 1 THROUGH 5
 20:C-----WITH VARIOUS PORTIONS OF IT BEING ACTIVATED FOR THE DIFFERENT
 21:C-----CASES.
 22:C
 23:BCS BOXINR
 24:S SURFN = 1
 25: TYPE = RECT
 26: ACTIVE = BOTTOM
 27: PROP = 0.9,0.9
 28: P1 = 1.0, 0.0, 1.0
 29: P2 = 1.0, 0.0, 0.0
 30: P3 = 1.0, 1.0, 0.0
 31: COM = * INNER RIGHT FRONT *
 32:S SURFN = 2
 33: TYPE = RECT
 34: ACTIVE = BOTTOM
 35: PROP = 0.9,0.9
 36: P1 = 1.0, 1.0, 1.0
 37: P2 = 1.0, 1.0, 0.0
 38: P3 = 0.0, 1.0, 0.0
 39: COM = * INNER RIGHT SIDE *
 40:S SURFN = 3
 41: TYPE = RECT
 42: ACTIVE = TOP
 43: PROP = 0.9,0.9
 44: P1 = 0.0, 0.0, 1.0
 45: P2 = 0.0, 0.0, 0.0
 46: P3 = 0.0, 1.0, 0.0
 47: COM = * INNER RIGHT BACK *
 48:S SURFN = 4
 49: TYPE = RECT
 50: ACTIVE = TOP
 51: PROP = 0.9,0.9
 52: P1 = 1.0, 1.0, 0.0
 53: COM = * INNER RIGHT BOTTOM *
 54:BCS BOXINL,INGBCS=BOXINR,NINC=10,IREFSF=1000
 55:C
 56:C-----THE FOREGOING CARD IMAGES DCS BOXINR IN REFERENCE PLANE 1000
 57:C-----TO CREATE BCS BOXINL. THE INTERIOR OF THE BOX WAS INPUT IN
 58:C-----THIS MANNER TO FACILITATE THE INPUT OF SAMPLE CASE 4 TO SHOW

59:C-----THE USE OF 'MESS' AND 'ERN' NODES.

60:C

61:R REFNO = 1000
 62: P1 = 1.0, 0.0, 1.0
 63: P2 = 1.0, 0.0, 0.0
 64: P3 = 0.0, 0.0, 0.0
 65: COM = * IMAGING PLANE *

66:BCS LIDINR

67:S SURFN = 5
 68: TYPE = RECT
 69: ACTIVE = BOTTOM
 70: PROP = 0.9,0.9
 71: P1 = 1.0, 1.0, 0.0
 72: COM = * INNER RIGHT LID *
 73:S SURFN = 15
 74: IMAGSF = 5
 75: IREFSF = 1000
 76: COM = * INNER LEFT LID *

77:BCS BOXOUT

78:S SURFN = 21
 79: TYPE = BOXS
 80: ACTIVE = OUT
 81: SHADE = NO
 82: PROP = 0.2,0.9
 83: P1 = 1.01,-1.01, 1.01
 84: P2 = 1.01, 1.01, 1.01
 85: P3 = -0.01, 1.01, 1.01
 86: P4 = -0.01, 1.01,-0.01
 87: COM = * OUTER SURFACES *

88:BCS LIDOUT

89:S SURFN = 28
 90: TYPE = RECT
 91: ACTIVE = TOP
 92: SHADE = NO
 93: PROP = 0.2,0.9
 94: P1 = 1.01,-1.01, 0.01
 95: P2 = 1.01, 1.01, 0.01
 96: P3 = -0.01, 1.01, 0.01
 97: COM = * OUTER SURFACE OF LID *

98:C

99:C-----THE NEXT TWO BCS'S (MESSR AND MESSL) ARE ACTIVATED IN SAMPLE

100:C-----CASE 4 ONLY.

101:C

102:BCS MESSR
 103:S SURFN = 101
 104: TYPE = RECT
 105: ACTIVE = TOP
 106: PROP = 1.0,1.0
 107: P1 = 1.0, 0.0, 1.0
 108: P2 = 1.0, 0.0, 0.0
 109: P3 = 0.0, 0.0, 0.0
 110: COM = * PRIMARY MESS NODE, RIGHT SIDE *

111:BCS MESSL

112:S SURFN = 111
 113: TYPE = RECT
 114: ACTIVE = BOTTOM
 115: PROP = 1.0,1.0

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116:      P1          = 1.0, 0.0, 1.0
117:      P2          = 1.0, 0.0, 0.0
118:      P3          = 0.0, 0.0, 0.0
119:      COM          = * PRIMARY MESS NODE, LEFT SIDE *
120:C
121:C-----THE FOLLOWING BCS (LIDSP) IS ACTIVATED IN SAMPLE CASE 3 ONLY.
122:C
123:BCS      LIDSP
124:S      SURFN      = 200
125:      TYPE        = RECT
126:      ACTIVE      = BOTTOM
127:      PROP        = 0.1,0.1
128:      SPRI        = 0.8
129:      SPRS        = 0.8
130:      P1          = 1.0,-1.0, 0.0
131:      P2          = 1.0, 1.0, 0.0
132:      P3          = 0.0, 1.0, 0.0
133:      COM          = * SPECULAR LID *
134:HEADER BCS DATA
135:BCS      BOXINR
136:BCS      BOXINL
137:BCS      LIDINR .0.,0.,1.,0.,-45.,0.
138:BCS      BOXOUT
139:BCS      LIDOUT .0.,0.,1.,0.,-45.,0.
140:BCS      MESSR
141:BCS      MESSL
142:BCS      LIDSP .0.,0.,1.,0.,-45.,0.
143:HEADER FORM FACTOR DATA
144:C
145:C-----ENTER KNOWN ZERO FORM FACTORS AND EQUIVALENT FORM FACTORS FOR
146:C-----CASE1.
147:C
148:FIO      CASE1
149:NODEA    1,2,3,4,11,12,13,14,5,15,21,22,23,24,25,26,END
150:BOTH     21,ZERO
151:      22,ZERO
152:      23,ZERO
153:      24,ZERO
154:      25,ZERO
155:      26,ZERO
156:      1,1,0.
157:      11,12,1,2
158:      11,13,1,3
159:      11,14,1,4
160:      11,15,1,5
161:      1,11,0.
162:      11,2,1,12
163:      11,3,1,13
164:      11,4,1,14
165:      11,5,1,15
166:      2,2,0.
167:      2,3,1,2
168:      2,4,1,4
169:      12,13,2,3
170:      12,14,2,4
171:      12,15,2,5
172:      12,3,2,13

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173:      12.4.2.14
174:      12.5.2.15
175:      3.3.0.
176:      3.4.1.4
177:      13.14.3.4
178:      13.15.3.5
179:      3.13.0.
180:      13.4.3.14
181:      13.5.3.15
182:      4.4.0.
183:      14.15.4.5
184:      4.14.0.
185:      14.5.4.15
186:      5.5.0.
187:      5.15.0.
188:HEADER CORRESPONDENCE DATA
189:C
190:C-----ENTER CORRESPONDENCE DATA FOR CASE 2
191:C
192:F10    CASE2
193:      1          = 1.11.22
194:      2          = 2.25
195:      3          = 3.13.24
196:      4          = 4.14.21
197:      5          = 5.15.26
198:      12         = 12.23
199:C
200:C-----ENTER CORRESPONDENCE DATA FOR CASE 3 TO COMBINE FORM FACTORS
201:C
202:F10    CASE3,FF
203:      1          = 1.11.22
204:      2          = 2.25
205:      3          = 3.13.24
206:      4          = 4.14.21
207:      5          = 5.15.26
208:      12         = 12.23
209:HEADER OPERATIONS DATA
210:C
211:C-----BUILD THE CASE 1 CONFIGURATION
212:C
213:BUILD CASE1,BOXINR,BOXINL,LIDINR,BOXOUT,LIDOUT
214:C
215:C-----PLOT THE CASE 1 CONFIGURATION INDICATING THE ACTIVE
216:C-----SIDES OF THE NODES.
217:C
218:      CALL NOATAS(0,0,0,YES,0)
219:L      NPL0T
220:C
221:C-----CALCULATE SHADOW FACTOR TABLES FOR SUBSEQUENT USE
222:C-----SAMPLE CASE 2 IN THE CALCULATION OF DIRECT FLUXES.
223:C
224:L      SFCAL
225:C
226:C-----CALCULATE THE FORM FACTOR MATRIX.
227:C
228:L      FFCAL
229:C

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230:C-----CALCULATE THE GRAY BODY MATRIX.
231:C
232:      CALL GBDATA(BOTH,0,FF)
233:L      GBCAL
234:C
235:C-----CALCULATE AND PUNCH RADIATION CONDUCTORS.
236:C
237:      CALL RKDATA(0.0,0.0,SPACE,999,0.0,0.0)
238:L      RKCAL
239:END OF DATA
240:8PHD,8LEP
241:8ASG,T/S RSO,8C,RSO,82,RSO APPENDIX H, CASE 1.
242:8ADD PROCSS
250:8FIN
NO CORRECTIONS APPLIED.

```

8FREE TPFS.

8ASG,T TPFS,.F4/0/TRX/400

QED ES3-TRASYS*TRASYS.PREPRON.TPF\$.PREPRO
CASE UPPER ASSUMED
ED 14.02-06/22-20:26-(0.)
EDIT
LINES:57 FIELDATA

0ED ES3-TRASYS*TRASYS.PROCSSH.TPFS.PROCSS
CASE UPPER ASSUMED
ED 14.02-06/22-20:26-(1.)
EDIT
LINES:103 FIELDATA

0SETC 0100

0SETC.1

0ASG,AQ ES3-TRASYS*LIBRYN.
FAC WARNING 040200004000

0ASG,T 1.,F4/0/TRK/600

0ASG,T 2.,F4/0/TRK/600

0ASG,T 3.,F4/0/TRK/600

0ASG,T DIR.,F17/0/POS/5

0ASG,T FFR.,F17/0/POS/9

0ASG,T GBIRR.,F17/0/POS/5

0ASG,T RIO.,F17/0/POS/9

0ASG,T SQNTL.,F17/0/TRK/10

IT
00 0ASG,T PLSR.,F17/0/TRK/320

0AS0.T TQR..F17/0/TRK/320

0USE 8.R10

0USE 14.RSI

0USE 16.SQNTL

0USE 21.FFR

0USE 22.DIR

0USE 23.OBIRR

0USE 25.PLSR

0USE 26.TQR

0XQT ES3-TRASYS*LIBRYN.CHECK

0TEST TNE/1/S3

0JUMP L1
INTERVENING STATEMENTS SKIPPED

0L1:AS0.T RI02..F17/0/POS/9

0AS0.T RI0S..F17/0/POS/20

0ASG,T DATAI.,F17/0/POS/9

0ASG,T CMPL.,F17/0/TRK/20

0ASG,T INFO

0ASG,T MAP.

0ASG,T MASS,F17/0/POS/20

0TEST TE/1/56

8JUMP L15
INTERVENING STATEMENTS SKIPPED

0L15:FREE 14

0USE 4,DATAI

0USE 9,RI05

0USE 10,RI02

0USE 11,INFO

0USE 12,CMERG

0USE 13,EMERG

0USE 14,MASSI

0USE 15,MASS

0USE 20,CRPL

0USE 27,MAP

0ASG,AQ ES3-TRASYS*COMPLRN.
FAC WARNING 040200004000

0DATA.I INFO.
DATA T7 RL70-5 06/22-20:26:21
END DATA. IMAGE COUNT: 20

0XQT ES3-TRASYS*COMPLRN.ABS

MASA/HARTIN HARIETTA THERMAL RADIATION ANALYSIS SYSTEM UNIVAC 1110/EXEC 8

TTTTTTTTTTTT
TTTTTTTTTTTT
TT TTT TT
TTT
TTT
TTT
TTT
TTT
TTT
TTTTTT

RRRRRRRR
RRRRRRRR
RRR RRR
RRR RRR
RRRRRRRR
RRR RRR
RRR RRR
RRR RRR
RRR RRR

AAAAAA
AAAAAA
AAAAAA
AAA AAA
AAA AAA
AAAAAA
AAA AAA
AAA AAA
AAA AAA
AAAAA AAAAA

SSSSSSSS
SSSSSSSSSS
SSS SS
SSS
SSSSSSSS
SSS
SS SS
SSSSSSSSSS
SSSSSSSS

TRASYS II

YYYY YYYY
YYY YYY
YYY YYY
YYY YYY
YYYYY
YYY
YYY
YYY
YYYYYY

SSSSSSSS
SSSSSSSSSS
SSS SS
SSS
SSSSSSSS
SSS
SS SS
SSSSSSSSSS
SSSSSSSS

PRE-PROCESSOR EXECUTION

VERSION.MODIFICATION ... UC2E3
MODIFICATION DATE 052878
DATE OF RUN 062278
TIME OF RUN 202623
JOB NUMBER RVNH01

DATE 062278 TIME 202625 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 8

MODEL = N/A
OPTION AND TITLE DATA BLOCKS

CARD ORIGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

INPUT HEADER OPTIONS DATA
INPUT TITLE SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/OBCAL/RKCAL - ORIGINAL RUN
INPUT MODEL = SAMPLE
INPUT RSO = RSTSAH1

DATE 062270 TIME 202625

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS), UNIVAC/EXC 8 VERSION

PAGE 2

MODEL = SAMPLE
TRASYS INFORMATION TO USER

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/QBCAL/RKCAL - ORIGINAL RUN

*
* A T T E N T I O N T R A S Y S U S E R S *
*

THIS SECTION OF THE TRASYS PRINTOUT WAS DEvised TO
INFORM THE TRASYS USERS OF THE STATUS OF THE TRASYS
PROGRAM WITHOUT HAVING TO PRINTOUT ALL THE STATUS
INFORMATION ON EVERY RUN. TO OBTAIN ADDITIONAL
INFORMATION ON HOW TO USE THIS SECTION OF THE TRASYS
PRINTOUT, PLACE A (INFO=INFO) IN THE OPTIONS DATA
BLOCK.

FOR TRASYS ASSISTANCE AND/OR POSSIBLE TRASYS PROGRAM
PROBLEMS, PLEASE CONTACT BOB VOOT AT JSC-2326.

NEWRL 08/29/77 DOCUMENTATION ADDITION

THE TRASYS -N- VERSION HAS BEEN UPDATED TO THE UC2E2
AND UL2E4 LEVEL.
SEE LATEST USERS MANUAL FOR INFORMATION ON USER-
CALLED SUBROUTINE, ARGUMENT CHANGES AND NEW
CAPABILITIES.

END OF TRASYS INFORMATION FILE

++NOTE++ DATA ORIGINATION FROM INPUT FILE, NO -RSI- SOURCE EDITING

DATE 062278 TIME 202628 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/ENC 8 VERSION PAGE 3

MODEL = SAMPLE
MODEL HISTORY

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

MODEL NAME SAMPLE

MODEL TITLE SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

MOD LABEL	RUN NUMBER	JOB DATA	RUN TIME	RSI TAPE	RSO TAPE	RTI TAPE	RTO TAPE	CNERO TAPE	EMERO TAPE	BCDOU TAPE	TRAJ TAPE	USER1 TAPE	USER2 TAPE
AA	RVHH01	062278	202625										

RSTSAM

DATE 062278 TIME 202626 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 4
 MODEL = SAMPLE SOURCE DATA EDIT DIRECTIVES SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/0BCAL/RKCAL - ORIGINAL RUN
 CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

INPUT	HEADER SURFACE DATA	1	AA
INPUT	C	2	AA
INPUT	C-----THIS SURFACE DATA BLOCK IS USED IN SAMPLE CASES 1 THROUGH 5	3	AA
INPUT	C-----WITH VARIOUS PORTIONS OF IT BEING ACTIVATED FOR THE DIFFERENT	4	AA
INPUT	C-----CASES.	5	AA
INPUT	C	6	AA
INPUT	BCS BOXINR	7	AA
INPUT	S SURFN = 1	8	AA
INPUT	TYPE = RECT	9	AA
INPUT	ACTIVE = BOTTOM	10	AA
INPUT	PROP = 0.9,0.9	11	AA
INPUT	P1 = 1.0, 0.0, 1.0	12	AA
INPUT	P2 = 1.0, 0.0, 0.0	13	AA
INPUT	P3 = 1.0, 1.0, 0.0	14	AA
INPUT	COM = * INNER RIGHT FRONT *	15	AA
INPUT	S SURFN = 2	16	AA
INPUT	TYPE = RECT	17	AA
INPUT	ACTIVE = BOTTOM	18	AA
INPUT	PROP = 0.9,0.9	19	AA
INPUT	P1 = 1.0, 1.0, 1.0	20	AA
INPUT	P2 = 1.0, 1.0, 0.0	21	AA
INPUT	P3 = 0.0, 1.0, 0.0	22	AA
INPUT	COM = * INNER RIGHT SIDE *	23	AA
INPUT	S SURFN = 3	24	AA
INPUT	TYPE = RECT	25	AA
INPUT	ACTIVE = TOP	26	AA
INPUT	PROP = 0.9,0.9	27	AA
INPUT	P1 = 0.0, 0.0, 1.0	28	AA
INPUT	P2 = 0.0, 0.0, 0.0	29	AA
INPUT	P3 = 0.0, 1.0, 0.0	30	AA
INPUT	COM = * INNER RIGHT BACK *	31	AA
INPUT	S SURFN = 4	32	AA
INPUT	TYPE = RECT	33	AA
INPUT	ACTIVE = TOP	34	AA
INPUT	PROP = 0.9,0.9	35	AA
INPUT	P1 = 1.0, 1.0, 0.0	36	AA
INPUT	COM = * INNER RIGHT BOTTOM *	37	AA
INPUT	BCS BOXINL,IMGBCS=BOXINR,NINC=10,IREFSF=1000	38	AA
INPUT	C	39	AA
INPUT	C-----THE FOREGOING CARD IMAGES BCS BOXINR IN REFERENCE PLANE 1000	40	AA
INPUT	C-----TO CREATE BCS BOXINL. THE INTERIOR OF THE BOX WAS INPUT IN	41	AA
INPUT	C-----THIS MANNER TO FACILITATE THE INPUT OF SAMPLE CASE 4 TO SHOW	42	AA
INPUT	C-----THE USE OF 'MESS' AND 'ERN' NODES.	43	AA
INPUT	C	44	AA

IMAGING SURFACE (1) BCS (BOXINR), GENERATING SURFACE (11) BCS (BOXINL)
IMAGING SURFACE (2) BCS (BOXINR), GENERATING SURFACE (12) BCS (BOXINL)
IMAGING SURFACE (3) BCS (BOXINR), GENERATING SURFACE (13) BCS (BOXINL)

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

		IMAGING SURFACE (4) BCS (BOXINR), GENERATING SURFACE (14) BCS (BOXINL)		
INPUT	R	REFNO = 1000	45	AA
INPUT		P1 = 1.0, 0.0, 1.0	46	AA
INPUT		P2 = 1.0, 0.0, 0.0	47	AA
INPUT		P3 = 0.0, 0.0, 0.0	48	AA
INPUT		COM = * IMAGING PLANE *	49	AA
INPUT	BCS	LIDINR	50	AA
INPUT	S	SURFN = 5	51	AA
INPUT		TYPE = RECT	52	AA
INPUT		ACTIVE = BOTTOM	53	AA
INPUT		PROP = 0.9,0.9	54	AA
INPUT		P1 = 1.0, 1.0, 0.0	55	AA
INPUT		COM = * INNER RIGHT LID *	56	AA
INPUT	S	SURFN = 15	57	AA
INPUT		IMAGSF = 5	58	AA
INPUT		IREFSF = 1000	59	AA
INPUT		COM = * INNER LEFT LID *	60	AA
INPUT	BCS	BOXOUT	61	AA
INPUT	S	SURFN = 21	62	AA
INPUT		TYPE = BOX5	63	AA
INPUT		ACTIVE = OUT	64	AA
INPUT		SHADE = NO	65	AA
INPUT		PROP = 0.2,0.9	66	AA
INPUT		P1 = 1.01,-1.01, 1.01	67	AA
INPUT		P2 = 1.01, 1.01, 1.01	68	AA
INPUT		P3 = -0.01, 1.01, 1.01	69	AA
INPUT		P4 = -0.01, 1.01,-0.01	70	AA
INPUT		COM = * OUTER SURFACES *	71	AA
INPUT	BCS	LIDOUT	72	AA
INPUT	S	SURFN = 26	73	AA
INPUT		TYPE = RECT	74	AA
INPUT		ACTIVE = TOP	75	AA
INPUT		SHADE = NO	76	AA
INPUT		PROP = 0.2,0.9	77	AA
INPUT		P1 = 1.01,-1.01, 0.01	78	AA
INPUT		P2 = 1.01, 1.01, 0.01	79	AA
INPUT		P3 = -0.01, 1.01, 0.01	80	AA
INPUT		COM = * OUTER SURFACE OF LID *	81	AA
INPUT	C		82	AA
INPUT		C-----THE NEXT TWO BCS'S (MESSR AND MESSL) ARE ACTIVATED IN SAMPLE	83	AA
INPUT		C-----CASE 4 ONLY.	84	AA
INPUT	C		85	AA
INPUT	BCS	MESSR	86	AA
INPUT	S	SURFN = 101	87	AA
INPUT		TYPE = RECT	88	AA
INPUT		ACTIVE = TOP	89	AA
INPUT		PROP = 1.0,1.0	90	AA

DATE 062278 TIME 202834 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC B VERSION PAGE 7

MODEL = SAMPLE SURFACE DATA INPUT BLOCK SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/OSCAL/RXCAL - ORIGINAL RUN

CARD ORIGIN	12345678 1	2345678 2	2345678 3	2345678 4	2345678 5	2345678 6	2345678 7	2345678 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	P1	= 1.0, 0.0, 1.0							91		AA
INPUT	P2	= 1.0, 0.0, 0.0							92		AA
INPUT	P3	= 0.0, 0.0, 0.0							93		AA
INPUT	COM	= * PRIMARY MESS NODE, RIGHT SIDE *							94		AA
INPUT	BCS	MESSL							95		AA
INPUT	S	SURFN	= 111						96		AA
INPUT		TYPE	= RECT						97		AA
INPUT		ACTIVE	= BOTTOM						98		AA
INPUT		PROP	= 1.0, 1.0						99		AA
INPUT	P1	= 1.0, 0.0, 1.0							100		AA
INPUT	P2	= 1.0, 0.0, 0.0							101		AA
INPUT	P3	= 0.0, 0.0, 0.0							102		AA
INPUT	COM	= * PRIMARY MESS NODE, LEFT SIDE *							103		AA
INPUT	C								104		AA
INPUT	C-----	THE FOLLOWING BCS (LIDSP) IS ACTIVATED IN SAMPLE CASE 5 ONLY.							105		AA
INPUT	C								106		AA
INPUT	BCS	LIDSP							107		AA
INPUT	S	SURFN	= 200						108		AA
INPUT		TYPE	= RECT						109		AA
INPUT		ACTIVE	= BOTTOM						110		AA
INPUT		PROP	= 0.1, 0.1						111		AA
INPUT		SPRI	= 0.0						112		AA
INPUT		SPRS	= 0.0						113		AA
INPUT	P1	= 1.0, -1.0, 0.0							114		AA
INPUT	P2	= 1.0, 1.0, 0.0							115		AA
INPUT	P3	= 0.0, 1.0, 0.0							116		AA
INPUT	COM	= * SPECULAR LID *							117		AA

DATE 062270 TIME 202642 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 0 VERSION PAGE 0

MODEL = SAMPLE
BCS DATA INPUT BLOCK

SAMPLE CASE 1 - MFL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

CARD ORIGIN	12345670 1	2345670 2	2345670 3	2345670 4	2345670 5	2345670 6	2345670 7	2345670 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	HEADER BCS DATA								118		AA
INPUT	BCS	BOXINR							119		AA
INPUT	BCS	BOXINL							120		AA
INPUT	BCS	LIDINR	.0..0..1..0..	-45..0.					121		AA
INPUT	BCS	BOXOUT							122		AA
INPUT	BCS	LIDOUT	.0..0..1..0..	-45..0.					123		AA
INPUT	BCS	HESSR							124		AA
INPUT	BCS	HESSL							125		AA
INPUT	BCS	LIDSP	.0..0..1..0..	-45..0.					126		AA

DATE 062270 TIME 202644 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 9

MODEL = SAMPLE SAMPLE CASE 1 - WPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

FORM FACTOR DATA INPUT BLOCK

CARD	ORIGIN	12345670 1 2345670 2 2345670 3 2345670 4 2345670 5 2345670 6 2345670 7 2345670 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	HEADER FORM FACTOR DATA		127		AA
INPUT	C		128		AA
INPUT	C-----ENTER KNOWN ZERO FORM FACTORS AND EQUIVALENT FORM FACTORS FOR		129		AA
INPUT	C-----CASE1.		130		AA
INPUT	C		131		AA
INPUT	FIG CASE1		132		AA
INPUT	NODEA 1,2,3,4,11,12,13,14,5,15,21,22,23,24,25,26.END		133		AA
INPUT	BOTH 21,ZERO		134		AA
INPUT	22,ZERO		135		AA
INPUT	23,ZERO		136		AA
INPUT	24,ZERO		137		AA
INPUT	25,ZERO		138		AA
INPUT	26,ZERO		139		AA
INPUT	1,1,0.		140		AA
INPUT	11,12,1,2		141		AA
INPUT	11,13,1,3		142		AA
INPUT	11,14,1,4		143		AA
INPUT	11,15,1,5		144		AA
INPUT	1,11,0.		145		AA
INPUT	11,2,1,12		146		AA
INPUT	11,3,1,13		147		AA
INPUT	11,4,1,14		148		AA
INPUT	11,5,1,15		149		AA
INPUT	2,2,0.		150		AA
INPUT	2,3,1,2		151		AA
INPUT	2,4,1,4		152		AA
INPUT	12,13,2,3		153		AA
INPUT	12,14,2,4		154		AA
INPUT	12,15,2,5		155		AA
INPUT	12,3,2,13		156		AA
INPUT	12,4,2,14		157		AA
INPUT	12,5,2,15		158		AA
INPUT	3,3,0.		159		AA
INPUT	3,4,1,4		160		AA
INPUT	13,14,3,4		161		AA
INPUT	13,15,3,5		162		AA
INPUT	3,13,0.		163		AA
INPUT	13,4,3,14		164		AA
INPUT	13,5,3,15		165		AA
INPUT	4,4,0.		166		AA
INPUT	14,15,4,5		167		AA
INPUT	4,14,0.		168		AA
INPUT	14,5,4,15		169		AA
INPUT	5,5,0.		170		AA
INPUT	5,15,0.		171		AA

MODEL = SAMPLE
CORRESPONDENCE DATA INPUT BLOCK

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

CARD	ORIGIN	12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	HEADER CORRESPONDENCE DATA		172		AA
INPUT	C		173		AA
INPUT	C-----ENTER CORRESPONDENCE DATA FOR CASE 2		174		AA
INPUT	C		175		AA
INPUT	F10 CASE2		176		AA
INPUT	1 = 1.11,22		177		AA
INPUT	2 = 2.25		178		AA
INPUT	3 = 3.13,24		179		AA
INPUT	4 = 4.14,21		180		AA
INPUT	5 = 5.15,26		181		AA
INPUT	12 = 12.23		182		AA
INPUT	C		183		AA
INPUT	C-----ENTER CORRESPONDENCE DATA FOR CASE 3 TO COMBINE FORM FACTORS		184		AA
INPUT	C		185		AA
INPUT	F10 CASE3,FF		186		AA
INPUT	1 = 1.11,22		187		AA
INPUT	2 = 2.25		188		AA
INPUT	3 = 3.13,24		189		AA
INPUT	4 = 4.14,21		190		AA
INPUT	5 = 5.15,26		191		AA
INPUT	12 ; = 12.23		192		AA

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MODEL = SAMPLE SAMPLE CASE 1 - RPLOT/SFCAL/FFCAL/GBAL/RKCAL - ORIGINAL RUN
OPERATION DATA INPUT BLOCK (PASS 1)

CARD ORIGIN	12345670 1	2345670 2	2345670 3	2345670 4	2345670 5	2345670 6	2345670 7	2345670 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	HEADER OPERATIONS DATA								193		AA

+++++ OPERATIONS DATA BLOCK (PASS 1) COMPLETE +++++

MODEL = SAMPLE SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
 OPERATION DATA INPUT BLOCK (PASS 2)

CARD ORGIN	12345670 1 2345670 2 2345670 3 2345670 4 2345670 5 2345670 6 2345670 7 2345670 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	C	194		AA
INPUT	C-----BUILD THE CASE 1 CONFIGURATION	195		AA
INPUT	C	196		AA
PROG	STEP -1	0		
INPUT	BUILD CASE1,BOXINR,BOXINL,LIDINR,BOXOUT,LIDOUT	197		AA
PROG	CALL BUILDG (BOXINR,6HCASE1)	0		
PROG	CALL ADD (BOXINL)	0		
PROG	CALL ADD (LIDINR)	0		
PROG	CALL ADD (BOXOUT)	0		
PROG	CALL ADD (LIDOUT)	0		
INPUT	C	198		AA
INPUT	C-----PLOT THE CASE 1 CONFIGURATION INDICATING THE ACTIVE	199		AA
INPUT	C-----SIDES OF THE NODES.	200		AA
INPUT	C	201		AA
INPUT	CALL NDATA(0.0,0.YES.0)	202		AA
INPUT	L NPLOT	203		AA
INPUT	C	204		AA
INPUT	C-----CALCULATE SHADOW FACTOR TABLES FOR SUBSEQUENT USE	205		AA
INPUT	C-----SAMPLE CASE 2 IN THE CALCULATION OF DIRECT FLUXES.	206		AA
INPUT	C	207		AA
INPUT	L SFCAL	208		AA
INPUT	C	209		AA
INPUT	C-----CALCULATE THE FORM FACTOR MATRIX.	210		AA
INPUT	C	211		AA
INPUT	L FFCAL	212		AA
INPUT	C	213		AA
INPUT	C-----CALCULATE THE GRAY BODY MATRIX.	214		AA
INPUT	C	215		AA
INPUT	CALL GBDATA(BOTH,0,FF)	216		AA
INPUT	L GBCAL	217		AA
INPUT	C	218		AA
INPUT	C-----CALCULATE AND PUNCH RADIATION CONDUCTORS.	219		AA
INPUT	C	220		AA
INPUT	CALL RKDATA(0.0,0.0,SPACE,999,0.0,0.0)	221		AA
INPUT	L RKCAL	222		AA
INPUT	END OF DATA	223		AA

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MODEL = SAMPLE
PROCESSOR CORE ALLOCATION

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

THE FOLLOWING IS THE PROCESSOR CORE ALLOCATION FOR THOSE SEGMENTS WHICH WILL BE LOADED IN THIS EXECUTION (APPROX.) ...

OCTAL/DECIMAL

TRASYS (Q) SEGMENT	121204/ 41604
OPERATIONS DATA (NOT KNOWN AT THIS TIME)	175000/ 64000
INITIALIZATION SEGMENT	122300/ 42176
FORM FACTOR SEGMENT	136100/ 48192
SHADOW FACTOR SEGMENT	136000/ 48128
NODE PLOTTER SEGMENT	123600/ 42880
GRAY BODY SEGMENT	124000/ 43008
RADATION CONDUCTOR SEGMENT	125500/ 43840
GRAY BODY DYNAMIC COMMON	000276/ 190
RADATION CONDUCTOR DYNAMIC COMMON	000574/ 380
GRAY BODY MINIMUM - MAXIMUM CORE	123557/ 42863 - 123707/ 42951
RADATION CONDUCTOR MINIMUM - MAXIMUM CORE	125212/ 43658 - 125456/ 43822
MINIMUM CORE NEEDED FOR PROCESSOR EXECUTION	136100/ 48192
MAXIMUM CORE NEEDED FOR PROCESSOR EXECUTION	136100/ 48192
AMOUNT OF CORE THAT WILL BE USED BY PROCESSOR .	136100/ 48192

MODEL = SAMPLE
 WRAP UP OF THE PRE-PROCESSOR

SAMPLE CASE 1 - MFL0T/SFCAL/FFCAL/OBCAL/RKCAL - ORIGINAL RUN

PRE-PROCESSOR ACCOUNTING INFORMATION	CP-SEC	DYN-STORAGE
SOURCE EDITING	1.262	676
DOCUMENTATION DATA PRE-PROCESSING000	0
QUANTITIES DATA PRE-PROCESSING037	266
ARRAY DATA PRE-PROCESSING000	0
SURFACE DATA PRE-PROCESSING (PASS 1) ...	1.416	64
SURFACE DATA PRE-PROCESSING (PASS 2)612	1141
BCS DATA PRE-PROCESSING214	186
FORM FACTOR DATA PRE-PROCESSING827	1169
SHADOW DATA PRE-PROCESSING000	0
FLUX DATA PRE-PROCESSING000	0
CORRESPONDENCE DATA PRE-PROCESSING223	101
OPERATIONS DATA PRE-PROCESSING	1.736	872
SUBROUTINE DATA PRE-PROCESSING209	0
SEQUENTIAL TAPE INITIALIZATION022	0
TOTAL CP TIME FOR PRE-PROCESSOR 7.088 DECIMAL SECONDS OR 000010 OCTAL SECONDS		
MINIMUM DYNAMIC STORAGE NEEDED BY PRE-PROCESSOR .. 1169 DECIMAL WORDS		
DYNAMIC STORAGE AVAILABLE TO PRE-PROCESSOR 10000 DECIMAL WORDS		

NORMAL TERMINATION BY PRE-PROCESSOR

@PHD,BLEP

@ASG,T/S RSO.,BC,RSO,92,RSO APPENDIX H, CASE 1.

@TEST TNE/1/S3

@JUMP L3
 INTERVENING STATEMENTS SKIPPED

@L3:FREE DATA1.

H-27
 @FREE 14

0FREE R105.

0FREE R102

0FREE CHERO

0FREE ENERO

0FREE INFO

0FOR.S1 TPF\$.TRASYS
FOR S0E3-06/22/78-20:27:01 (.0)

MAIN PROGRAM

STORAGE USED: CODE(1) 000123; DATA(0) 000001; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003	CCONST	000205
0004	TAPE	000042
0005	RSTRT	000017
0006	TITLE	000037
0007	PLOT	000234
0010	BLKDIR	000040
0011	BCSN	000010
0012	INDX	000001
0013	NMODIR	000050
0014	INDXS	000023
0015	INDXN	000023
0016	DIMS	000157
0017	OSTR	000271
0020	IFS	000045
0021	IKS	000045
0022	PR	000112
0023	PSH	000224
0024	TSTR	000515
0025	ALPH	000023
0026	AREA	000023
0027	EMISS	000023
0030	SRIR	000023
0031	SRSO	000023
0032	TRIR	000023
0033	TRSO	000023
0034	NODE	000023
0035	ODTEMP	000144
0036	ORBIT	000121
0037	OSTORE	000044
0040	1STPDR	000001
0041	NSPEC	000001
0042	ISPEC	000001
0043	SREFL1	000001
0044	SREFLS	000001
0045	PLOTTR	000051
0046	LNGSEG	000027

EXTERNAL REFERENCES (BLOCK, NAME)

0047	RDPROG
0050	ODPROG
0051	PRDUMP
0052	FFPROG
0053	RBPROG
0054	CMPROG
0055	SFPROG
0056	NPPROG

0057 .OPPROG
 0060 DIPROG
 0061 DRPROG
 0062 GBPROG
 0063 RCPROG
 0064 AQPROG
 0065 QOPROG
 0066 PLPROG
 0067 MFPROG
 0070 HRPUP
 0071 EXIT
 0072 NINTR\$
 0073 NERR\$
 0074 NSTOPS

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000004	100L	0001	000040	1300L	0001	000043	1325L	0001	000046	1350L	0001	000051	1400L
0001	000054	1500L	0001	000057	1600L	0001	000062	1700L	0001	000065	1750L	0001	000070	1800L
0001	000073	1900L	0001	000076	2000L	0001	000101	2100L	0001	000104	2200L	0001	000107	2300L
0001	000112	2400L	0001	000115	3000L	0036	000000	ALAN	0025	000000	ALPH	0036	000016	APER
0003	000202	AQPRNT	0003	000172	ARAD	0026	000000	AREA	0036	000001	ASUM	0036	000114	ATHT
0036	000037	BETA	0036	000015	BETAS	0011	000003	BOXINL	0011	000004	BOXINR	0011	000005	BOXOUT
0036	000036	CIGMA	0036	000014	CIGMAS	0036	000065	CLOCK	0036	000066	CONE	0036	000112	DAWN
0003	000146	DELCT	0003	000014	DIACC	0003	000015	DIACCS	0016	000000	DIMS	0003	000016	GINOSH
0003	000017	DIPNCH	0003	000143	DLTLNE	0036	000113	DOY	0017	000000	DSTR	0006	000027	DTE
0003	000000	DTR	0036	000111	DUSK	0036	000003	DWP	0036	000004	ECC	0003	000168	ELPBEA
0027	000000	EMISS	0003	000020	FFACC	0003	000021	FFACCS	0003	000125	FFCMB	0003	000133	FFDISF
0003	000022	FFHIN	0003	000175	FFNAC	0003	000024	FFNOSH	0003	000025	FFPNCH	0003	000026	FFPRNT
0003	000023	FFRATL	0003	000171	FFZERO	0003	000147	FOG	0003	000203	GAUSS	0003	000030	GBWAND
0036	000026	GRAV	0036	000030	HA	0036	000031	HP	0003	000115	IAI	0003	000113	IALBFL
0003	000060	IAQOBI	0003	000081	IAQODS	0003	000063	IAQSDA	0003	000064	IAQSDP	0003	000062	IAQSDS
0003	000116	IAS	0003	000027	IAUTOC	0036	000063	ICALFL	0003	000130	ICMBL	0037	000000	IDSTR
0003	000124	IEQFF	0003	000123	IFFSHO	0020	000000	IFS	0006	000033	IHSTEP	0021	000000	IKS
0003	000164	ILLUMN	0003	000105	IMESS	0003	000131	INCORE	0015	000000	INDXN	0014	000000	INDXS
0036	000101	INSHAD	0003	000163	INTMF	0007	000077	IOPNPNP	0007	000201	IOPNV	0007	000113	IOPNVU
0007	000105	IOPYIT	0036	000006	IORBIT	0036	000005	IORNT	0003	000010	IOVL	0006	000031	IPAGE
0003	000114	IPLAFL	0045	000004	IPLNA	0045	000005	IPLSN	0045	000000	IPLUNT	0003	000034	IPROMP
0003	000065	IQOARY	0003	000066	IQOCOR	0003	000074	IQOTAB	0003	000077	IQOTHE	0003	000032	IRKCN
0003	000035	IRKNSP	0036	000073	IROTXY	0036	000074	IROTY	0036	000075	IROTZ	0003	000140	IRSI
0003	000141	IRTI	0003	000174	ISFAC	0036	000077	ISFT	0007	000233	ISHO	0003	000137	ISKIP
0036	000025	ISKPSO	0003	000112	ISOLFL	0042	000000	ISPEC	0003	000106	ISPND	0040	000000	ISTPOR
0003	000150	ISTR	0003	000057	ITRALL	0003	000053	ITRCA0	0003	000054	ITRCB0	0003	000055	ITRCC0
0003	000056	ITRCDO	0003	000042	ITRC10	0003	000043	ITRC20	0003	000044	ITRC30	0003	000045	ITRC40
0003	000046	ITRC50	0003	000047	ITRC60	0003	000050	ITRC70	0003	000051	ITRC80	0003	000052	ITRC90
0045	000047	IIPLOT	0004	000033	KBCDOU	0004	000035	KRSI	0004	000038	KRSO	0004	000037	KRTI
0004	000040	KRTO	0004	000034	KTRAJ	0046	000011	LAQSEG	0046	000023	LCHCOM	0046	000022	LCHSEG
0046	000006	LDISEG	0046	000021	LORSEG	0046	000002	LFFSEG	0046	000010	LGBCOM	0046	000007	LGBCSEG
0011	000006	LIDINR	0011	000007	LIDOUT	0011	000000	LIDSP	0006	000032	LINE	0046	000025	LKFSEG
0046	000004	LNPSEG	0046	000000	LQDSEG	0046	000005	LQPSEG	0046	000016	LPLCOM	0046	000015	LPLSEG
0046	000013	LQOCOM	0046	000012	LQOSEG	0046	000014	LQOSEG	0046	000020	LRCCOM	0046	000017	LRCSEG
0046	000001	LROSEG	0046	000003	LSFSEG	0003	000003	MAXBC	0046	000024	MAXFL	0003	000151	MB
0011	000001	MESSL	0011	000002	MESSR	0003	000153	MFCO	0003	000154	MFLUK	0003	000152	MG
0003	000142	MITSIN	0006	000035	MLINE	0003	000200	MNND	0006	000026	MODELN	0003	000135	MRSRC
0003	000155	MSRF	0007	000232	NACT	0004	000023	NBCDOU	0003	000100	NBCDSK	0010	000000	NBLKDR
0003	000013	NBLKLN	0003	000156	NCONT	0046	000026	NCURFL	0004	000000	NDI	0004	000001	NOIR

0003	000157	NELN	0003	000107	NERN	0004	000002	NFF	0004	000003	NFFR	0003	000201	NFFYTP
0003	000144	NFIGCO	0003	000162	NFIGFF	0003	000178	NFIGGB	0045	000048	NFRNC	0004	000004	NGBIR
0004	000005	NGBIRR	0004	000008	NGBSO	0003	000165	NIBBLE	0008	000034	NJOB	0012	000000	NLRIO
0003	000110	NMESS	0003	000160	NHIR	0006	000038	NHODOL	0013	000008	NHODIR	0003	000132	NHODLS
0003	000004	NN	0003	000006	NNOD	0003	000128	NNODC	0003	000127	NNODU	0034	000000	NODE
0004	000010	NOUT	0004	000017	NPLS	0004	000020	NPLSR	0007	000000	NPNNP	0007	000008	NPTIT
0004	000022	NPUN	0007	000017	NPVU	0004	000011	NRAN	0004	000007	NRARR	0003	000177	NRMOD
0004	000025	NRSI	0004	000026	NRSO	0003	000138	NRSR	0005	000008	NRSRCB	0005	000011	NRSRCE
0005	000003	NRSRCI	0005	000000	NRSRCO	0005	000014	NRSRCT	0004	000027	NRTI	0004	000030	NRTO
0003	000005	NS	0004	000041	NSCRR	0004	000012	NSCRI	0004	000013	NSCR2	0004	000014	NSCR3
0041	000000	NSPEC	0036	000064	NSPFF	0003	000111	NSPND	0004	000021	NSQNTL	0003	000012	NSSTEP
0003	000011	NSTEP	0003	000145	NSTPOI	0003	000122	NSTPL	0003	000121	NSTSOL	0003	000007	NSURF
0006	000013	NTITLE	0004	000015	NTQ	0004	000018	NTQR	0004	000024	NTRAJ	0004	000031	NUSERI
0004	000032	NUSER2	0035	000000	ODTEMP	0036	000027	OTNC	0007	000121	OPROT	0007	000202	OPRPLN
0007	000165	OPSCL	0007	000173	OPSLR	0007	000216	OPTIMP	0007	000224	OPTIMS	0007	000210	OPTRUE
0036	000041	ORNT	0036	000011	PALB	0036	000007	PERIOD	0003	000002	PI	0036	000108	PLCL
0045	000050	PLCMB	0036	000107	PLCO	0045	000001	PLCRVF	0045	000008	PLLABX	0045	000013	PLLABY
0045	000020	PLTITI	0045	000032	PLTIT2	0036	000100	PLTYPE	0045	000002	PLXMPF	0045	000003	PLYMPF
0036	000076	PNAME	0022	000000	PR	0036	000012	PRAD	0036	000002	PSD	0023	000000	PSH
0003	000067	QOAMPF	0003	000070	QOFMPF	0003	000076	QOPNCH	0003	000072	QORMPF	0003	000075	QOTAPE
0003	000071	QOTMPF	0003	000073	QOTYPE	0003	000102	RALB	0036	000067	RATE	0003	000104	RFRAC
0003	000031	RKAMPF	0003	000033	RKMIN	0003	000038	RKPNCH	0003	000037	RKSP	0003	000040	RKTAPE
0036	000070	ROTX	0036	000071	ROTY	0036	000072	ROTZ	0003	000103	RPLAN	0003	000101	RSOLAR
0036	000013	RSUN	0003	000001	RTD	0036	000040	RTMET	0003	000204	RTOL	0003	000161	SAOS
0003	000134	SFPRNT	0036	000102	SHADIN	0036	000103	SHAOUT	0003	000041	SIGMA	0036	000024	SOL
0036	000115	SOLO	0036	000052	SPINT	0043	000000	SREFLI	0044	000000	SREFLS	0030	000000	SRIR
0031	000000	SRSO	0003	000173	STRACK	0036	000034	STRDEC	0036	000033	STRRA	0036	000104	SUNCL
0036	000105	SUNCO	0036	000035	SUNDEC	0036	000118	SUNPYO	0036	000032	SUNRA	0003	000167	TDIAM
0003	000170	THGHT	0036	000022	TIMEPR	0036	000021	TIMEST	0036	000110	TIMSP	0008	000000	TITLE
0006	000030	TME	0032	000000	TRIR	0033	000000	TRSO	0003	000117	TRUANF	0003	000120	TRUANI
0036	000023	TRUEAN	0024	000000	TSTR	0036	000017	WDS	0036	000010	WSS	0036	000020	WSUN
0007	000025	ZNPROT	0007	000071	ZNPSCl									

00101	1*	COMMON /CONST/	DTR	RTD	PI	MAXBC	NN	000000
00101	2*	NS	NNOD	NSURF	IOVL	NSTEP	NSSTEP	000000
00101	3*	NBLKLN	DIACC	DIACCS	DINOSH	DIPNCH	FFACC	000000
00101	4*	FFACCS	FFMIN	FFRATL	FFNOSH	FFPNCH	FFPRNT	000000
00101	5*	IAUTOC	GBWENO	RKAMPF	IRKCN	RKMIN	IPRODP	000000
00101	6*	IRKNSP	RKPNCH	RKSP	RKTAPE	SIGMA	ITRCIO	000000
00101	7*	ITRC20	ITRC30	ITRC40	ITRC50	ITRC60	ITRC70	000000
00101	8*	ITRC80	ITRC90	ITRCA0	ITRCB0	ITRCD0	ITRCD0	000000
00101	9*	ITRALL	IAQGBI	IAQGBS	IAQSDS	IAQSDA	IAQSDP	000000
00101	10*	IQOARY	IQOCOR	QOAMPF	QOFMPF	QOTMPF	QORMPF	000000
00101	11*	QOTYPE	IQOTAB	QOTAPE	QOPNCH	IQOTHE	NBCDSK	000000
00101	12*	RSOLAR	RALB	RPLAN	RFRAC	INESS	ISPND	000000
00101	13*	NERN	NMESS	NSPND	ISOLFL	IALBFL	IPLAFL	000000
00101	14*	IAI	IAS	TRUANF	TRUANI	NSTSOL	NSTPL	000000
00101	15*	IFFSHO	IEQFF	FFCMB	NNODC	NNODU	ICMBL	000000
00101	16*	INCORE	NMODLS	FFDISF	SFPRNT	NRSRC	NRSR	000000
00101	17*	ISKIP	IRSI	IRTI	HITSIN	DLTLE		000000
00103	18*	COMMON /CONST/	NFIGCO	NSTPDI	DELCT	FOO	ISTRIT	000001
00103	19*	MB	MG	MFCO	MFLUK	MSRF	NCONT	000001
00103	20*	NELN	NHIR	SAOS	NFIGFF	INTMF	ILLUMN	000001
00103	21*	NIBBLE	ELPBEA	TDIAM	THGHT	FFZERO	ARAD	000001

00103	22°	.	. STRACK	. ISFAC	. FFNAC	. NFICGB	. NRHOD	. MNND	000001
00103	23°	.	. NFFYP	. AQPRNT	. GAUSS	. RTOL			000001
00104	24°	1	COMMON /TAPE /	. NDI	. NDIR	. NFF	. NFFR		000001
00104	25°	1		. NGBIR	. NGBIRR	. NGBSO	. NRARR		000001
00104	26°	2		. NOUT	. NRAM	. NSCR1	. NSCR2		000001
00104	27°	3		. NSCR3	. NTQ	. NTQR	. NPLS		000001
00104	28°	4		. NPLSR	. NSQNTL	. NPUN	. NBCDOU		000001
00104	29°	5		. NTRAJ	. NRSI	. NRSO	. NRTI		000001
00104	30°	6		. NRTD	. NUSER1	. NUSER2			000001
00104	31°	7		. KBCDOU	. KTRAJ	. KRSI	. KRSO		000001
00104	32°	8		. KRTI	. KRTD	. NSCR			000001
00105	33°		COMMON /RSTRT /	. NRSRC(3)		. NRSRC1(3)			000001
00105	34°	1		. NRSRCB(3)		. NRSRCE(3)			000001
00105	35°	2		. NRSRCT(3)					000001
00106	36°		COMMON /TITLE /	. TITLE(11)		. NTITLE(11)			000001
00106	37°	1		. MODELN	. DTE	. THE	. IPAGE		000001
00106	38°	2		. LINE	. INSTEP	. NJOB	. MLINE		000001
00106	39°	3		. NHODEL					000001
00107	40°		COMMON /PLOT /	. NPNNP(8)		. NPTIT(9)			000001
00107	41°	1		. NPVU(8)		. ZNPROT(8,8)			000001
00107	42°	2		. ZNPSC(8)		. IOPNNP(8)			000001
00107	43°	3		. IOPTIT(8)		. IOPNVU(8)			000001
00107	44°	4		. OPROT(8,8)		. OPSCL(8)			000001
00107	45°	5		. OPSCLR(8)		. IOPNV			000001
00107	46°	6		. OPRPLN(8)		. OPTTRUE(8)			000001
00107	47°	7		. OPTIMP(8)		. OPTIMS(8)			000001
00107	48°	8		. NACT		. ISHO			000001
00110	49°		COMMON /BLKDIR/	. NBLKDR(4, 8)					000001
00111	50°		COMMON /BCSN /	. LIDSP	. MESSL	. MESSR	. BOXIML	. BOXINR	000001
00111	51°	.	. BOXOUT	. LIDINR	. LIDOUT				000001
00112	52°		COMMON /INDX /	. MLRIO					000001
00113	53°		COMMON /NHODIR/	. NHODIR(2, 20)					000001
00114	54°		COMMON /INDXS /	. INDXS (19)					000001
00115	55°		COMMON /INDXM /	. INDXM (19)					000001
00116	56°		COMMON /DIMS /	. DIMS(3, 37)					000001
00117	57°		COMMON /DSTR /	. DSTR (5, 37)					000001
00120	58°		COMMON /IFS /	. IFS (37)					000001
00121	59°		COMMON /IKS /	. IKS (37)					000001
00122	60°		COMMON /PR /	. PR (2, 37)					000001
00123	61°		COMMON /PSH /	. PSH (4, 37)					000001
00124	62°		COMMON /TSTR /	. TSTR (3,3, 37)					000001
00125	63°		COMMON /ALPH /	. ALPH (19)					000001
00126	64°		COMMON /AREA /	. AREA (19)					000001
00127	65°		COMMON /EMISS /	. EMISS (19)					000001
00130	66°		COMMON /SRIR /	. SRIR (19)					000001
00131	67°		COMMON /SRSO /	. SRSO (19)					000001
00132	68°		COMMON /TRIR /	. TRIR (19)					000001
00133	69°		COMMON /TRSO /	. TRSO (19)					000001
00134	70°		COMMON /NODE /	. NODE (19)					000001
00135	71°		COMMON /ODTEMP/	. ODTEMP(100)					000001
00136	72°		COMMON /ORBIT /	. ALAN	. ASUN	. PSD	. DWP		000001
00136	73°	1		. ECC	. IORNT	. IORBIT	. PERIOD		000001
00136	74°	2		. HSS	. PALB	. PRAD	. RSUN		000001
00136	75°	3		. CIGMAS	. BETAS	. APER	. WDS		000001
00136	76°	4		. HSUN	. TIMEST	. TIMEPR	. TRUEAN		000001
00136	77°	5		. SOL	. ISKPSO	. GRAY	. OINC		000001
00136	78°	6		. HA	. HP	. SUNRA	. STRRA		000001

00136	79°	7	. STRDEC	. SUNDEC	. CIGMA	. BETA	000001
00136	80°	8	. RTHET	. ORNT(3.3)		. SPINT(3.3)	000001
00136	81°	9	. ICALFL	. NSPFF	. CLOCK	. CONE	000001
00136	82°	0	. RATE	. ROTX	. ROTY	. ROTZ	000001
00136	83°	1	. IROTX	. IROTY	. IROTZ	. PHASE	000001
00136	84°	2	. ISFT	. FLTYPE	. INSHAD	. SHADIN	000001
00136	85°	3	. SHAOUT	. SUNCL	. SUNCO	. FLCL	000001
00136	86°	4	. PLCO	. TIMSP	. DUSK	. DAMN	000001
00136	87°	5	. DOY	. ATMT	. SOLO	. SUNPVO(3)	000001
00137	88°		COMMON /DSTORE/	IDSTR (12,3)			000001
00140	89°		COMMON /ISTPOR/	ISTPOR(1)			000001
00141	90°		COMMON /NSPEC /	NSPEC			000001
00142	91°		COMMON /ISPEC /	ISPEC (1)			000001
00143	92°		COMMON /SREFLI/	SREFLI(1)			000001
00144	93°		COMMON /SREFLS/	SREFLS(1)			000001
00145	94°		COMMON /PLOTTR/	IPLUNT . PLCRVF	. PLXMPF	. PLYMPF	000001
00145	95°	1		. IPLNA . IPLSN	. PLLABX(5)		000001
00145	96°	2		. PLLABY(5)	. PLTITI(10)		000001
00145	97°	3		. PLTIT2(12)	. NFRMC	. 11PLOT	000001
00145	98°	4		. PLCHB			000001
00146	99°		COMMON /LNGSEG/	LDDSEG . LRDSEG	. LFFSEG	. LSFSEG	000001
00146	100°	1		. LNPSEG . LOPSEG	. LDISEG	. LGBSEG	000001
00146	101°	2		. LGBCOM . LAQSEG	. LQOSEG	. LQOCOM	000001
00146	102°	3		. LRBSEG . LPLSEG	. LPLCOM	. LRCSEG	000001
00146	103°	4		. LRCCOM . LORSEG	. LCHSEG	. LCMCOM	000001
00146	104°	5		. MAXFL . LHFSEG	. NCURFL		000001
00147	105°		CALL ROPROG				000001
00150	106°	100	CONTINUE				000004
00151	107°		CALL OOPROG				000004
00152	108°		IF(IPROMP.NE.0)	CALL PROUMP (IPROMP)			000005
00154	109°		GO TO (1300,1400,1500,1600,1700,1800,1900,2000,				000012
00154	110°	1	2100,1325,2200,2300,1750,1350,2400,3000				000012
00154	111°	2), 10VL				000012
00155	112°	1300	CONTINUE				000040
00156	113°		CALL FFPROG				000040
00157	114°		GO TO 100				000041
00160	115°	1325	CONTINUE				000043
00161	116°		CALL RBPROG				000043
00162	117°		GO TO 100				000044
00163	118°	1350	CONTINUE				000046
00164	119°		CALL CMPROG				000046
00165	120°		GO TO 100				000047
00166	121°	1400	CONTINUE				000051
00167	122°		CALL SFPROG				000051
00170	123°		GO TO 100				000052
00171	124°	1500	CONTINUE				000054
00172	125°		CALL NPPROG				000054
00173	126°		GO TO 100				000055
00174	127°	1600	CONTINUE				000057
00175	128°		CALL OPPROG				000057
00176	129°		GO TO 100				000060
00177	130°	1700	CONTINUE				000062
00200	131°		CALL DIPROG				000062
00201	132°		GO TO 100				000063
00202	133°	1750	CONTINUE				000065
00203	134°		CALL DRPROG				000065
00204	135°		GO TO 100				000066

00205	136°	1900	CONTINUE
00206	137°		CALL GBPROG
00207	138°		GO TO 100
00210	139°	1900	CONTINUE
00211	140°		CALL RCPRG
00212	141°		GO TO 100
00213	142°	2000	CONTINUE
00214	143°		CALL AQPRG
00215	144°		GO TO 100
00216	145°	2100	CONTINUE
00217	146°		CALL QOPRG
00220	147°		GO TO 100
00221	148°	2200	CONTINUE
00222	149°		CALL PLPRG
00223	150°		GO TO 100
00224	151°	2300	CONTINUE
00225	152°		CALL RCPRG
00226	153°		GO TO 100
00227	154°	2400	CONTINUE
00230	155°		CALL MFPRG
00231	156°		GO TO 100
00232	157°	3000	CONTINUE
00233	158°		CALL WRAPUP
00234	159°		CALL EXIT
00235	160°		END

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 000122

END OF COMPILATION: NO DIAGNOSTICS.

OFOR.SI TFFS.ODPROG
FOR S0E3-06/22/78-20:27:12 (.0)

SUBROUTINE ODPROG ENTRY POINT 000170

STORAGE USED: CODE(1) 000172; DATA(0) 000053; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003	CCONST	000205
0004	TAPE	000042
0005	RSTR	000017
0006	TITLE	000037
0007	PLOT	000234
0010	BLKDIR	000040
0011	BCSN	000010
0012	INDX	000001
0013	NMODIR	000050
0014	INDXS	000023
0015	INDXN	000023
0016	QIMS	000157
0017	DSTR	000271
0020	IFS	000045
0021	IKS	000045
0022	PR	000112
0023	PSH	000224
0024	TSTR	000515
0025	ALPH	000023
0026	AREA	000023
0027	EMISS	000023
0030	SRIR	000023
0031	SRSO	000023
0032	TRIR	000023
0033	TRSO	000023
0034	NODE	000023
0035	ODTEMP	000144
0036	ORBIT	000121
0037	DSTORE	000044
0040	ISTPOR	000001
0041	NSPEC	000001
0042	ISPEC	000001
0043	SREFLI	000001
0044	SREFLS	000001
0045	PLOTTR	000051
0046	LNGSEG	000027
0047	DIRECT	000034

EXTERNAL REFERENCES (BLOCK, NAME)

0050	INTOD
0051	BUILDCC
0052	ADD
0053	NOATAS
0054	GBDATA

0055 RKDATA
0056 NERR25
0057 NERR35

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000020	10100L	0001	000033	10101L	0001	000073	10102L	0001	000104	10103L	0001	000114	10104L		
0001	000132	10105L	0001	000157	10106L	0038	000000	ALAN	0000	R	000027	ALL	0025	000000	ALPH	
0036	000016	APER	0003	000202	AQPRNT	0003	000172	ARAD	0028	000000	AREA	0036	000001	ASUN		
0036	000114	ATMT	0000	R	000033	AUTO	0000	R	000036	AV	0000	R	000040	BCDOU		
0038	000015	BETAS	0000	R	000023	BOTH	0011	R	000003	BOXINL	0011	R	000004	BOXINR		
0036	000036	CIGMA	0036	000014	CIGMAS	0036	000065	CLOCK	0000	R	000005	CM	0036	000066	CONE	
0000	R	000034	CORR	0036	000112	DAWN	0003	000146	DELCT	0003	000014	DIACC	0003	000015	DIACCS	
0016	000000	DIMS	0003	000016	DINOSH	0003	000017	DIPNCH	0047	000000	DIRECT	0003	000143	DLTLE		
0036	000113	DOY	0017	000000	DSTR	0006	000027	DTE	0003	000000	DTR	0036	000111	DUSK		
0036	000003	DWP	0000	R	000011	EAR	0036	000004	ECC	0003	000168	ELPBEA	0027	000000	EMISS	
0000	R	000004	FF	0003	000020	FFACC	0003	000021	FFACCS	0003	000125	FFCMB	0003	000133	FFDISF	
0003	000022	FFMIN	0003	000175	FFNAC	0003	000024	FFNOSH	0003	000025	FFPNCH	0003	000026	FFPRNT		
0003	000023	FFRATL	0003	000171	FFZERO	0003	000147	FOO	0003	000203	GAUSS	0003	000030	GBWBD		
0036	000026	GRAV	0036	000030	HA	0036	000031	HP	0003	000115	IAI	0003	000113	IABFL		
0003	000060	IAQGBI	0003	000061	IAQGBS	0003	000063	IAQSDA	0003	000064	IAQSDP	0003	000062	IAQSDS		
0003	000116	IAS	0003	000027	IATOC	0036	000063	ICALFL	0003	000130	ICMBL	0037	000000	IOSTR		
0003	000124	IEOFF	0003	000123	IFFSHO	0020	000000	IFS	0008	000033	IHSTEP	0021	000000	IKS		
0003	000164	ILLUMN	0003	000105	IHESS	0003	000131	INCORE	0015	000000	INDXN	0014	000000	INDXS		
0000	000047	INJPS	0036	000101	INSHAD	0003	000163	INTMF	0007	000077	IOPNPN	0007	000201	IOPNV		
0007	000113	IOPNVU	0007	000105	IOPNIT	0036	000008	IORBIT	0036	000005	IORNT	0003	I	000010	IOVL	
0006	000031	IPAGE	0003	000114	IPLAFL	0045	000004	IPLNA	0045	000005	IPLSN	0045	000000	IPLUNT		
0003	000034	IPRDHP	0003	000065	IQARY	0003	000066	IQCOR	0003	000074	IQOTAB	0003	000077	IQOTHE		
0000	I	000025	IR	0003	000032	IRKCN	0003	000035	IRKNSP	0036	000073	IROTX	0036	000074	IROTY	
0036	000075	IROTZ	0003	000140	IRSI	0003	000141	IRTI	0003	000174	ISFAC	0036	000077	ISFT		
0007	000233	ISHO	0003	000137	ISKIP	0036	000025	ISKPSO	0003	000112	ISOLFL	0042	000000	ISPEC		
0003	000106	ISPND	0040	000000	ISTPOR	0003	000150	ISTRT	0003	000057	ISTRALL	0003	000053	ITRCAO		
0003	000054	ITRCBO	0003	000055	ITRCCO	0003	000056	ITRCDO	0000	I	000032	ITRCON	0003	000042	ITRCIO	
0003	000043	ITRC20	0003	000044	ITRC30	0003	000045	ITRC40	0003	000046	ITRC50	0003	000047	ITRC60		
0003	000050	ITRC70	0003	000051	ITRC80	0003	000052	ITRC90	0045	000047	IIPLOT	0000	I	000014	JUP	
0004	000033	KBCDOU	0004	000035	KRSI	0004	000036	KRSO	0004	000037	KRTI	0004	000040	KRTO		
0000	I	000042	KSTEP	0004	000034	KTRAJ	0046	000011	LAQSEG	0046	000023	LCMCON	0046	000022	LCHSEG	
0046	000006	LDISEG	0046	000021	LDRSEG	0046	000002	LFFSEG	0046	000010	LGBCON	0046	000007	LGBSEG		
0011	I	000006	LIDINR	0011	I	000007	LIDOUT	0011	000000	LIDSP	0006	000072	LINE	0046	000025	LKFSEG
0046	000004	LNPSEG	0046	000000	LQDSEG	0046	000005	LQDSEG	0046	000011	LPLCON	0046	000015	LFLSEG		
0046	000013	LQDCOM	0046	000012	LQDSEG	0046	000014	LRBSEG	0046	000014	LRCCON	0046	000017	LRCSEG		
0046	000001	LRDSEG	0046	000003	LSFSEG	0000	I	000013	MAR	0003	000003	MAXBC	0046	000024	MAXFL	
0003	000151	MB	0000	I	000007	MER	0011	000001	MESSL	0011	000002	MESSR	0003	000153	MFCO	
0003	000154	MFLUK	0003	000152	MO	0003	000142	MITSIN	0006	000035	MLINE	0003	000200	MNIO		
0006	000026	MODELN	0000	I	000012	MOO	0003	000135	MRSRC	0003	000155	MRRF	0007	000232	NACT	
0004	000023	NBCDOU	0003	000100	NBCDSK	0010	000000	NBLKDR	0003	000013	NBLKLN	0003	000156	NCONT		
0046	000026	NCURFL	0004	000000	NOI	0004	000001	NOIR	0003	000157	NELN	0000	I	000016	NEP	
0003	000107	NERN	0004	000002	NFF	0004	000003	NFFR	0003	000201	NFFTP	0003	000144	NFIGCO		
0003	000162	NFIGFF	0003	000176	NFIGGB	0045	000046	NFRMC	0004	000004	NGBR	0004	000005	NGBRIR		
0004	000006	NGBSO	0003	000165	NIOBLE	0006	000034	NJOB	0012	000006	NLRIO	0003	000110	NHESS		
0003	000160	NMIR	0006	000036	NMODEL	0013	000000	NMODIR	0003	000132	NMODLS	0003	000004	NN		
0003	000006	NNOD	0003	000126	NNODC	0003	000127	NNODU	0000	I	000000	NO	0034	000000	NODE	
0000	I	000003	NOSH	0004	000010	NOUT	0004	000017	NPLS	0004	000020	NPLSR	0007	000000	NPPNP	
0007	000006	NPTIT	0004	000022	NPUN	0007	000017	NPVU	0004	000011	NRAN	0004	000007	NRARR		
0003	000177	NRMOD	0004	000025	NRSI	0004	000026	NRSO	0003	000136	NRSR	0005	000006	NRSRCB		
0005	000011	NRSRCE	0005	000003	NRSRCI	0005	000000	NRSRCO	0005	000014	NRSRCT	0004	000027	NRTI		

0004	000030	NRT0	0003	000005	NS	0004	000041	NSCRR	0004	000012	NSCR1	0004	000013	NSCR2
0004	000014	NSCR3	0041	000000	NSPEC	0036	000064	NSPFF	0003	000111	NSPND	0004	000021	NSQNTL
0003	000012	NSSTEP	0003	000011	NSTEP	0003	000145	NSTPDI	0003	000122	NSTPL	0003	000121	NSTSQL
0003	000007	NSURF	0008	000013	NTITLE	0004	000015	NTQ	0004	000016	NTQR	0004	000024	NTRAJ
0004	000031	NUSER1	0004	000032	NUSER2	0035	000000	ODTEHP	0036	000027	OINC	0007	000121	OPROT
0007	000202	OPRPLN	0007	000165	OPSC1	0007	000173	OPSC1R	0007	000216	OPTIMP	0007	000224	OPTIMS
0007	000210	OPTRUE	0036	000041	ORNT	0036	000011	PALB	0000	R 000041	PALL	0036	000007	PERIOD
0003	000002	PI	0036	000106	PLCL	0045	000050	PLCHB	0036	000107	PLCO	0045	000001	PLCRVF
0045	000006	PLLABX	0045	000013	PLLABY	0045	000020	PLTITI	0045	000032	PLTIT2	0036	000100	PLTYPE
0045	000002	PLXMPF	0045	000003	PLYMPF	0036	000076	PNAME	0022	000000	PR	0036	000012	PRAD
0036	000002	PSD	0023	000000	PSH	0000	R 000031	PUN	0003	000067	QOAMPF	0003	000070	QOFMPF
0003	000076	QOPNCH	0003	000072	QORMPF	0003	000075	QOTAPE	0003	000071	QOTHPF	0003	000073	QOTYPE
0003	000102	RALB	0036	000067	RATE	0000	R 000006	RB	0000	R 000022	READ	0003	000104	RFRAC
0003	000031	RKAMPF	0003	000033	RKMIN	0003	000036	RKPNCH	0003	000037	RKSP	0003	000040	RKTAPE
0036	000070	ROTX	0036	000071	ROTY	0036	000072	ROTZ	0003	000103	RPLAN	0003	000101	RSOLAR
0036	000013	RSUN	0003	000001	RTD	0036	000040	RTMET	0003	000204	RTOL	0003	000161	SAOS
0000	R 000015	SAT	0000	R 000021	SAVE	0003	000134	SFPRNT	0000	R 000002	SHAD	0036	000102	SHADIN
0036	000103	SHAOUT	0003	000041	SIGMA	0036	000024	SOL	0000	R 000024	SOLAR	0036	000115	SOLO
0000	R 000030	SPACE	0036	000052	SPINT	0043	000000	SREFLI	0044	000000	SREFLS	0030	000000	SRIR
0031	000000	SRSO	0003	000173	STRACK	0036	000034	STRDEC	0038	000033	STRRA	0000	R 000020	SUN
0036	000104	SUNCL	0036	000105	SUNCO	0036	000035	SUNDEC	0036	000116	SUNPVO	0036	000032	SUNRA
0000	R 000026	TAPE	0003	000167	TDIAM	0003	000170	THGHT	0036	000022	TIMEPR	0036	000021	TIMEST
0036	000110	TIKSP	0006	000000	TITLE	0006	000030	TME	0032	000000	TRIR	0033	000000	TRSO
0003	000117	TRUANF	0003	000120	TRUANI	0036	000023	TRUEAN	0024	000000	TSTR	0000	R 000017	URA
0000	R 000037	USER1	0000	R 000010	VEN	0036	000017	WDS	0036	000010	WSS	0036	000020	WSUN
0000	R 000001	YES	0000	R 000035	ZERO	0007	000025	ZNPROT	0007	000071	ZNPSCL			

00101	1*	SUBROUTINE ODPROQ										000000
00103	2*	COMMON /CONST/										000000
00103	3*	000000	
00103	4*	000000	
00103	5*	000000	
00103	6*	000000	
00103	7*	000000	
00103	8*	000000	
00103	9*	000000	
00103	10*	000000	
00103	11*	000000	
00103	12*	000000	
00103	13*	000000	
00103	14*	000000	
00103	15*	000000	
00103	16*	000000	
00103	17*	000000	
00103	18*	000000	
00104	19*	COMMON /CONST/										000000
00104	20*	000000	
00104	21*	000000	
00104	22*	000000	
00104	23*	000000	
00104	24*	000000	
00105	25*	COMMON /TAPE /										000000
00105	26*	1	000000	
00105	27*	2	000000	

00105	28°	3	. NSCR3	. NTQ	. NTQR	. NPLS	000000		
00105	29°	4	. NPLSR	. NSQNTL	. NPUN	. NBCDOW	000000		
00105	30°	5	. NTRAJ	. NRSI	. NRSO	. NRTI	000000		
00105	31°	6	. NRTQ	. NUSER1	. NUSER2		000000		
00105	32°	7	. KBCDOU	. KTRAJ	. KRSI	. KRSO	000000		
00105	33°	8	. KRTI	. KRTQ	. NSCR		000000		
00106	34°		COMMON /RSTRY /	. NRSRC(3)	. NRSRC1(3)		000000		
00106	35°	1		. NRSRCB(3)	. NRSRC(3)		000000		
00106	36°	2		. NRSRCT(3)			000000		
00107	37°		COMMON /TITLE /	. TITLE(11)	. NTITLE(11)		000000		
00107	38°	1		. MODELN	. DTE	. THE	. IPAGE	000000	
00107	39°	2		. LINE	. IHSTEP	. NJOB	. MLINE	000000	
00107	40°	3		. NMODEL				000000	
00110	41°		COMMON /PLOT /	. NPNNP(6)	. NPTIT(9)			000000	
00110	42°	1		. NPVU(6)	. ZNPROT(6,6)			000000	
00110	43°	2		. ZNPSC(6)	. IOPNNP(6)			000000	
00110	44°	3		. IOPTIT(6)	. IOPNVU(6)			000000	
00110	45°	4		. OPROT(6,6)	. OPSCL(6)			000000	
00110	46°	5		. OPSCLR(6)	. IOPNV			000000	
00110	47°	6		. OPRPLN(6)	. OPTTRUE(6)			000000	
00110	48°	7		. OPTIMP(6)	. OPTIMS(6)			000000	
00110	49°	8		. NACT	. ISHO			000000	
00111	50°		COMMON /BLKDIR/	. NBLKDR(4, 8)				000000	
00112	51°		COMMON /BCSN /	. LIDSP	. HESSL	. HESSR	. BOXINL	. BOXINR	000000
00112	52°		. BOXOUT	. LIDINR	. LIDOUT				000000
00113	53°		COMMON /INDX /	. MLRIO					000000
00114	54°		COMMON /NMODIR/	. NMODIR(2, 20)					000000
00115	55°		COMMON /INDXS /	. INDXS (19)					000000
00116	56°		COMMON /INDXN /	. INDXN (19)					000000
00117	57°		COMMON /DIHS /	. DIHS(3, 37)					000000
00120	58°		COMMON /DSTR /	. DSTR (5, 37)					000000
00121	59°		COMMON /IFS /	. IFS (37)					000000
00122	60°		COMMON /IKS /	. IKS (37)					000000
00123	61°		COMMON /PR /	. PR (2, 37)					000000
00124	62°		COMMON /PSH /	. PSH (4, 37)					000000
00125	63°		COMMON /TSTR /	. TSTR (3,3, 37)					000000
00126	64°		COMMON /ALPH /	. ALPH (19)					000000
00127	65°		COMMON /AREA /	. AREA (19)					000000
00130	66°		COMMON /EMISS /	. EMISS (19)					000000
00131	67°		COMMON /SRIR /	. SRIR (19)					000000
00132	68°		COMMON /SRSO /	. SRSO (19)					000000
00133	69°		COMMON /TRIR /	. TRIR (19)					000000
00134	70°		COMMON /TRSO /	. TRSO (19)					000000
00135	71°		COMMON /NODE /	. NODE (19)					000000
00138	72°		COMMON /ODTEMP/	. ODTEMP(100)					000000
00137	73°		COMMON /ORBIT /	. ALAN	. ASUN	. PSD	. DMP		000000
00137	74°	1		. ECC	. IORNT	. IORBIT	. PERIOD		000000
00137	75°	2		. WSS	. PALB	. PRAD	. RSUN		000000
00137	76°	3		. CIGHAS	. BETAS	. APER	. NDS		000000
00137	77°	4		. WSUH	. TIMEST	. TIMEPR	. TRUEAN		000000
00137	78°	5		. SOL	. ISKPSO	. GRAV	. OINC		000000
00137	79°	6		. HA	. HP	. SUNRA	. STRRA		000000
00137	80°	7		. STRDEC	. SUNDEC	. CIGHA	. BETA		000000
00137	81°	8		. RTHET	. ORNT(3,3)		. SPINT(3,3)		000000
00137	82°	9		. ICALFL	. NSPFF	. CLOCK	. CONE		000000
00137	83°	0		. RATE	. ROTX	. ROTY	. ROTZ		000000
00137	84°	1		. IROTX	. IROTY	. IROTZ	. PNAME		000000

00137	88°	2	. ISFT	. PLTYPE	. INSHAD	. SHADIN	000000
00137	86°	3	. SNAOUT	. SUNCL	. SUNCO	. PLCL	000000
00137	87°	4	. PLCO	. TIMSP	. DUSK	. DAWN	000000
00137	88°	5	. DOY	. ATHT	. SOLO	. SUNPVO(3)	000000
00140	89°		COMMON /DSTORE/	IDSTR (12,3)			000000
00141	90°		COMMON /ISTPDR/	ISTPDR (1)			000000
00142	91°		COMMON /NSPEC /	NSPEC			000000
00143	92°		COMMON /ISPEC /	ISPEC (1)			000000
00144	93°		COMMON /SREFLI/	SREFLI (1)			000000
00145	94°		COMMON /SREFLS/	SREFLS (1)			000000
00146	95°		COMMON /PLOTTR/	1PLUNT	. PLCRVF	. PLXHPF	000000
00146	96°	1		. IPLNA	. IPLSN	. PLLABX(5)	000000
00146	97°	2		. PLLABY(5)		. PLTITI(10)	000000
00146	98°	3		. PLTIT2(12)		. NFRMC	000000
00146	99°	4		. PLCHB		. IIPLOT	000000
00147	100°		COMMON /LNQSEG/	LODSEG	. LRQSEG	. LFFSEG	000000
00147	101°	1		. LNPSEG	. LOPSEG	. LDISEG	000000
00147	102°	2		. LOBCOM	. LAQSEG	. LQOSEG	000000
00147	103°	3		. LRQSEG	. LPLSEG	. LPLCOM	000000
00147	104°	4		. LRCCOM	. LDRSEG	. LCMSEG	000000
00147	105°	5		. MAXFL	. LMFSEG	. NCURFL	000000
00150	106°		COMMON /DIRCT /	DIRCT (28)			000000
00151	107°		DATA NO	/2HNO	/		000000
00153	108°		DATA YES	/3HYES	/		000000
00155	109°		DATA SHAD	/4HSHAD	/		000000
00157	110°		DATA NOSH	/4HNOSH	/		000000
00161	111°		DATA FF	/2HFF	/		000000
00163	112°		DATA CH	/2HCM	/		000000
00165	113°		DATA RB	/2HRB	/		000000
00167	114°		DATA MER	/3HMER	/		000000
00171	115°		DATA VEN	/3HVEN	/		000000
00173	116°		DATA EAR	/3HEAR	/		000000
00175	117°		DATA MOO	/3HMOO	/		000000
00177	118°		DATA MAR	/3HMAR	/		000000
00201	119°		DATA JUP	/3HJUP	/		000000
00203	120°		DATA SAT	/3HSAT	/		000000
00205	121°		DATA NEP	/3HNEP	/		000000
00207	122°		DATA URA	/3HURA	/		000000
00211	123°		DATA SUN	/3HSUN	/		000000
00213	124°		DATA SAVE	/4HSAVE	/		000000
00215	125°		DATA READ	/4HREAD	/		000000
00217	126°		DATA BOTH	/4HBOTH	/		000000
00221	127°		DATA SOLAR	/3HSOL	/		000000
00223	128°		DATA IR	/2HIR	/		000000
00225	129°		DATA TAPE	/4HTAPE	/		000000
00227	130°		DATA ALL	/3HALL	/		000000
00231	131°		DATA SPACE	/5HSPACE	/		000000
00233	132°		DATA PUN	/3HPUN	/		000000
00235	133°		DATA ITRCON	/2HON	/		000000
00237	134°		DATA AUTO	/4HAUTO	/		000000
00241	135°		DATA CORR	/4HCORR	/		000000
00243	136°		DATA ZERO	/4HZERO	/		000000
00245	137°		DATA AV	/2HAV	/		000000
00247	138°		DATA USER1	/5HUSER1	/		000000
00251	139°		DATA BCDU	/5HBCDU	/		000000
00253	140°		DATA PALL/4HPALL/				000000
00253	141°						000000

C

00253	142°	C-----BUILD THE CASE 1 CONFIGURATION	193	-000000
00253	143°	C	193	000000
00255	144°	CALL INTOD		000000
00256	145°	KSTEP = NSTEP		000001
00257	146°	IF(KSTEP.GT.100) KSTEP = 100		000003
00261	147°	GO TO (10100		000011
00261	148°), KSTEP		000011
00261	149°	C		000011
00261	150°	C-----		000011
00261	151°	C		000011
00261	152°	CSTEP -1	0	000011
00261	153°	C		000011
00262	154°	10100 CONTINUE		000020
00263	155°	GO TO (10101 , 10102 , 10103 , 10104 , 10105 , 10106		000020
00263	156°), NSSTEP		000020
00264	157°	10101 CONTINUE		000033
00264	158°	CBUILD CASE1,BOXINR,BOXINL,LIDINR,BOXOUT,LIDOUT	197	000033
00265	159°	CALL BUILD (BOXINR,6HCASE1)	0	000033
00266	160°	CALL ADD (BOXINL)	0	000038
00267	161°	CALL ADD (LIDINR)	0	000041
00270	162°	CALL ADD (BOXOUT)	0	000044
00271	163°	CALL ADD (LIDOUT)	0	000047
00271	164°	C	198	000047
00271	165°	C-----PLOT THE CASE 1 CONFIGURATION INDICATING THE ACTIVE	199	000047
00271	166°	C-----SIDES OF THE NODES.	200	000047
00271	167°	C	201	000047
00272	168°	CALL NDATA(0.0,0.YES,0)	202	000052
00272	169°	C		000052
00272	170°	CL NPLOT	203	000052
00272	171°	C		000052
00273	172°	IOVL = 3		000061
00274	173°	NSSTEP = 1		000063
00275	174°	NSSTEP = 2		000065
00276	175°	RETURN		000067
00277	176°	10102 CONTINUE		000073
00277	177°	C	204	000073
00277	178°	C-----CALCULATE SHADOW FACTOR TABLES FOR SUBSEQUENT USE	205	000073
00277	179°	C-----SAMPLE CASE 2 IN THE CALCULATION OF DIRECT FLUXES.	206	000073
00277	180°	C	207	000073
00277	181°	C		000073
00277	182°	CL SFCAL	208	000073
00277	183°	C		000073
00300	184°	IOVL = 2		000073
00301	185°	NSSTEP = 1		000074
00302	186°	NSSTEP = 3		000075
00303	187°	RETURN		000100
00304	188°	10103 CONTINUE		000104
00304	189°	C	209	000104
00304	190°	C-----CALCULATE THE FORM FACTOR MATRIX.	210	000104
00304	191°	C	211	000104
00304	192°	C		000104
00304	193°	CL FFCAL	212	000104
00304	194°	C		000104
00305	195°	IOVL = 1		000104
00306	196°	NSSTEP = 1		000105
00307	197°	NSSTEP = 4		000106
00310	198°	RETURN		000110

00311	199°	10104	CONTINUE		000114
00311	200°	C		213	000114
00311	201°	C-----CALCULATE THE GRAY BODY MATRIX.		214	000114
00311	202°	C		215	000114
00312	203°	CALL GBDATA(BOTH,0,FF)		216	000114
00312	204°	C			000114
00312	205°	CL GBCAL		217	000114
00312	206°	C			000114
00313	207°		IOVL = 6		000120
00314	208°		NSTEP = 1		000122
00315	209°		NSSTEP = 5		000124
00316	210°		RETURN		000126
00317	211°	10105	CONTINUE		000132
00317	212°	C		218	000132
00317	213°	C-----CALCULATE AND PUNCH RADIATION CONDUCTORS.		219	000132
00317	214°	C		220	000132
00320	215°	CALL RKDATA(0.0,0.0,SPACE,999,0.0,0.0,0)		221	000132
00320	216°	C			000132
00320	217°	CL RKCAL		222	000132
00320	218°	C			000132
00321	219°		IOVL = 12		000145
00322	220°		NSTEP = 1		000147
00323	221°		NSSTEP = 6		000151
00324	222°		RETURN		000153
00325	223°	10106	CONTINUE		000157
00326	224°		IOVL = 16		000157
00327	225°		RETURN		000160
00330	226°		END		000171

END OF COMPILATION: NO DIAGNOSTICS.

OFOR.S1 TPFS.RDPROG
FOR SOE3-05/22/78-20:27:20 (.0)

SUBROUTINE RDPROG ENTRY POINT 000011

STORAGE USED: CODE(1) 000013; DATA(0) 000004; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK. NAME)

0003 RDMAIN
0004 MERR3\$

STORAGE ASSIGNMENT (BLOCK. TYPE. RELATIVE LOCATION. NAME)

0000 000000 INJP\$

00101	1*	SUBROUTINE RDPROG
00103	2*	CALL RDMAIN
00104	3*	RETURN
00105	4*	END

000000
000000
000001
000012

END OF COMPILATION: NO DIAGNOSTICS.

OFOR.SI TPFS.FFPROG
FOR SOE3-06/22/78-20:27:32 (.0)

SUBROUTINE FFPROG ENTRY POINT 000011

STORAGE USED: CODE(1) 000013; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 FFVALI 000023
0004 FFVALS 000023
0005 BFE 000023
0006 BFA 000023
0007 FFRS11 000001
0010 FFRS12 000001
0011 FFRS13 000001
0012 FFRS14 000001
0013 FFRS15 000001
0014 FFSHDC 000023
0015 FFSUMC 000023
0016 FFEQ 000023

EXTERNAL REFERENCES (BLOCK, NAME)

0017 FFMAIN
0020 NERR3S

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0006	000000	BFA	0005	000000	BFE	0013	000000	FFRS1A	0012	000000	FFRS1E	0010	000000	FFRS1I
0011	000000	FFRS1S	0003	000000	FFVALI	0004	000000	FFVALS	0016	000000	INDXF	0000	000000	INJPS
0014	000000	ISHAD	0007	000000	NODERI	0015	000000	SUM						

00101	1*	SUBROUTINE FFPROG		000000
00103	2*	COMMON /FFVALI/	FFVALI(19)	000000
00104	3*	COMMON /FFVALS/	FFVALS(19)	000000
00105	4*	COMMON /BFE /	BFE(19)	000000
00106	5*	COMMON /BFA /	BFA(19)	000000
00107	6*	COMMON /FFRS11/	NODERI(1)	000000
00110	7*	COMMON /FFRS12/	FFRS1I(1)	000000
00111	8*	COMMON /FFRS13/	FFRS1S(1)	000000
00112	9*	COMMON /FFRS14/	FFRS1E(1)	000000
00113	10*	COMMON /FFRS15/	FFRS1A(1)	000000
00114	11*	COMMON /FFSHDC/	ISHAD(19)	000000
00115	12*	COMMON /FFSUMC/	SUM(19)	000000
00116	13*	COMMON /FFEQ/	INDXF(19)	000000
00117	14*	CALL FFMAIN		000000
00120	15*	RETURN		000001
00121	16*	END		000012

END OF COMPILATION: NO DIAGNOSTICS.

8FOR.S1 TPFS.SFPROG
 FOR SOE3-06/22/78-20:27:37 (,0)

SUBROUTINE SFPROG ENTRY POINT 000011

STORAGE USED: CODE(1) 000013; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 SFSDHC 000023
 0004 SFQDP 000023
 0005 SFQDR 000023
 0006 SFQDS 000023

EXTERNAL REFERENCES (BLOCK, NAME)

0007 SFMAIN
 0010 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000000 INJP\$ 0003 000000 ISHAD 0004 000000 QDP 0005 000000 QDR 0006 000000 QDS

00101	1*	SUBROUTINE SFPROG		000000
00103	2*	COMMON /SFSDHC/	ISHAD(19)	000000
00104	3*	COMMON /SFQDP /	QDP(19)	000000
00105	4*	COMMON /SFQDR /	QDR(19)	000000
00106	5*	COMMON /SFQDS /	QDS(19)	000000
00107	6*	CALL SFMAIN		000000
00110	7*	RETURN		000001
00111	8*	END		000012

END OF COMPILATION: NO DIAGNOSTICS.

0FOR,SI TPF\$.NPPROG
FOR 50E3-06/22/78-20:27:41 (1.0)

SUBROUTINE NPPROG ENTRY POINT 000011

STORAGE USED: CODE(1) 000013; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 MNP 000023

EXTERNAL REFERENCES (BLOCK, NAME)

0004 NPMAN
0005 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0000 000000 INJP\$ 0003 000000 MNP

00101	1*	SUBROUTINE NPPROG	000000
00103	2*	COMMON /MNP / MNP(19)	000000
00104	3*	CALL NPMAN	000000
00105	4*	RETURN	000001
00106	5*	END	000012

END OF COMPILATION: NO DIAGNOSTICS.

0FOR.S1 TPF\$.GBPROG
FOR SOE3-06/22/78-20:27:45 (.0)

SUBROUTINE GBPROG ENTRY POINT 000011

STORAGE USED: CODE(1) 000013; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 FA 000023
0004 SPACE 000023
0005 XSPACE 000023
0006 BLKGB 000278

EXTERNAL REFERENCES (BLOCK, NAME)

0007 GBMAIN
0010 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0003 000000 FA 0000 000000 INJP\$ 0006 000000 IX 0004 000000 SPACE 0005 000000 XSPACE

00101	1*	SUBROUTINE GBPROG		000000
00103	2*	COMMON /FA / FA (19)		000000
00104	3*	COMMON /SPACE / SPACE (19)		000000
00105	4*	COMMON /XSPACE/ XSPACE(19)		000000
00106	5*	COMMON /BLKGB / IX(190)		000000
00107	6*	CALL GBMAIN		000000
00110	7*	RETURN		000001
00111	8*	END		000012

END OF COMPILATION: NO DIAGNOSTICS.

8FOR.SI TPFS.RCPROG
FOR S0E3-06/22/78-20:27:48 (.0)

SUBROUTINE RCPROG ENTRY POINT 000011

STORAGE USED: CODE(1) 000013; DATA(0) 000004; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 ISPN 000144
0004 MSND 000144
0005 NDS 000024
0006 SFS 000024
0007 SPCNO 000024
0010 RCEMIT 000024
0011 RCARET 000024
0012 RCSUM1 000023
0013 RCSUM2 000023
0014 BLKRC 000574

EXTERNAL REFERENCES (BLOCK, NAME)

0015 RCHAIN
0016 NERR3\$

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0011	000000	AREAT	0010	000000	EMIT	0000	000000	INJPS	0003	000000	ISPN	0014	000000	IX
0004	000000	MSND	0005	000000	NDS	0006	000000	SF	0007	000000	SPACNO	0012	000000	SUM1
0013	000000	SUM2												

00101	1*	SUBROUTINE RCPROG												000000
00103	2*	COMMON /ISPN /	ISPN	(100)									000000
00104	3*	COMMON /MSND /	MSND	(100)									000000
00105	4*	COMMON /NDS /	NDS	(20)									000000
00106	5*	COMMON /SFS /	SF	(20)									000000
00107	6*	COMMON /SPCNO /	SPACNO	(20)									000000
00110	7*	COMMON /RCEMIT/	EMIT	(20)									000000
00111	8*	COMMON /RCARET/	AREAT	(20)									000000
00112	9*	COMMON /RCSUM1/	SUM1	(19)									000000
00113	10*	COMMON /RCSUM2/	SUM2	(19)									000000
00114	11*	COMMON /BLKRC /	IX	(380)									000000
00115	12*	CALL RCHAIN												000000
00116	13*	RETURN												000001
00117	14*	END												000012

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END OF COMPILATION: NO DIAGNOSTICS.

0FREE CNPL.

0COPY.1 MAP..HAPP
FURPUR 27R1 RL72-0 06/22/70 20:27:54

0FREE MAP

0PREP TPFS
FURPUR 27R1 RL72-0 06/22/70 20:27:54
END PREP.

SHAP,S HAPF,TRASYS
 MAP20R2 RL71-3 06/22/78 20:27:56 (0,)
 SIR: S1 ELEMENT IS NON-SIR TYPE SDF *IF000000000

1. LIB TPF\$
2. LIB ES3-TRASYS*LIBRYN
3. LIB MSC*PLTLIB
4. LIB MSC*LOCALIB
5. SEG TR
6. IN TPF\$.TRASYS
7. IN NTRANS/JSC
8. SEG RD*,(TR)
9. IN TPF\$.RDPROG
10. SEG OD*,(TR)
11. IN TPF\$.ODPROG
12. SEG FF*,(TR)
13. IN TPF\$.FFPROG
14. SEG SF*,(TR)
15. IN TPF\$.SFPROG
16. SEG NP*,(TR)
17. IN TPF\$.NPPROG
18. SEG GB*,(TR)
19. IN TPF\$.GBPROG
20. SEG RC*,(TR)
21. IN TPF\$.RCPROG
22. END

ADDRESS LIMITS 001000 064120 26193 10ANK WORDS DECIMAL
 065000 123007 15368 00ANK WORDS DECIMAL
 SEGMENT LOAD TABLE 065000 065037
 INDIRECT LOAD TABLE 065040 065752
 STARTING ADDRESS 027243

SEGMENT TR		001000 030660	065753 104534
DEPTH(COMMONBLOCK)			
FPACK\$/MSC8	\$(013)	DEPTH	\$(0) 065753 065760
NBF00\$			\$(2) 065761 065107
NCNVT\$/FOR68	\$(1)	001000 001221	\$(2) 066110 070335
NINPT\$/FOR3-CORR	\$(1)	001222 002616	\$(2) 070336 070432
NFINO\$/FOR-E3	\$(1)	002617 003036	\$(2) 070433 070468
NFTCH\$/FOR-E2	\$(1)	003037 003321	\$(2) 070467 070537
NOTIN\$/FOR-E3	\$(1)	003322 003616	\$(2) 070540 070553
NCLOS\$/FOR-E3	\$(1)	003617 004054	\$(2) 070554 070557
NRBLK\$/FOR-E2	\$(1)	004055 004077	\$(2) 070560 070605
NSWTC\$/FOR69	\$(1)	004078 004124	
NBSOL\$/FOR-E3	\$(1)	004125 004161	
NUPDA\$/FOR68	\$(1)	004162 004215	
NHBLI\$/FOR68	\$(1)	004216 004327	
NFCHK\$/FOR-E3	\$(1)	004330 005321	\$(2) 070606 070756
	\$(3)	005322 005322	\$(4) 070757 071030
NFTV\$/FOR-E2	\$(1)	005323 005345	
NBDCV\$/FOR-E3	\$(1)	005346 005476	\$(2) 071031 071106

NIOERS/FOR-E3	\$ (1)	005477 005716	\$ (2)	071107 071258
NFMTS/FOR-E3	\$ (1)	005717 006601	\$ (2)	071257 071333
CLOSESF/FOR-TE3	\$ (1)	006602 006602		
NEXP6\$/FOR-E3	\$ (1)	006603 007000	\$ (2)	071334 071405
TANCOTANS/FOR59	\$ (1)	007001 007176	\$ (2)	071406 071426
ATANS/FOR59	\$ (1)	007177 007402	\$ (2)	071427 071460
NWDAS/FOR-E3	\$ (1)	007403 010150	\$ (2)	071461 071464
NRDAS/FOR-E3	\$ (1)	010151 010600	\$ (2)	071465 071477
SQRT\$/FOR59	\$ (1)	010601 010641	\$ (2)	071500 071511
SINCOS\$/FOR-E3	\$ (1)	010642 010776	\$ (2)	071512 071534
NDEFS/FOR-E3	\$ (1)	010777 011571	\$ (2)	071535 071636
NFINPS/FOR-E3	\$ (1)	011572 012217	\$ (2)	071637 071722
NRWNS/FOR-E3	\$ (1)	012220 012303	\$ (2)	071723 071734
NOBUF\$/FOR68	\$ (1)	012304 012344		
NBKSP\$/FOR-E3	\$ (1)	012345 013100	\$ (2)	071735 071762
NHEF\$/FOR-E2	\$ (1)	013101 013306	\$ (2)	071763 072002
NIERS/FOR-E3	\$ (1)	013307 013465	\$ (2)	072003 072122
NFOUS/FOR-E3	\$ (1)	013466 014105	\$ (2)	072123 072144
FORVCOMS/FOR-TE3			\$ (2)	072145 072154
NERCOMS/FOR-TE3	\$ (1)	014106 014165	\$ (2)	072155 072170
FORCOMS/FORFTN			\$ (2)	072171 072176
ERUS/SYS72-8				
NTABS/E3-JSC			\$ (2)	072177 072236
NSTOP\$/FORE3-JSC	\$ (1)	014166 014265	\$ (2)	072237 072310
NERRS/FOR-E3	\$ (1)	014266 014627	\$ (2)	072311 072470
EXITSF/FOR-TE3	\$ (1)	014630 014630		
IDLS/SYS64	\$ (1)	014631 014677		
NERTRANS/JSC-E3	\$ (1)	014700 015054	\$ (2)	072471 072600
	\$ (037)	INFO-010-LC		
SCCTAB/SMICHI			\$ (0)	072601 072704
PRINTV/SMICHI	\$ (1)	015055 015167	\$ (0)	072705 072713
PAC	\$ (1)	015170 015212		
UNPAC	\$ (1)	015213 015227		
BXLTR			\$ (0)	072714 073343
FNODES/LL1B11	\$ (1)	015230 015342	\$ (4)	073344 073344
	\$ (013)	DEPTH		
CNVRT	\$ (1)	015343 017077	\$ (0)	073345 073704
			\$ (2)	BLANK\$COMMON
PUT	\$ (1)	017100 017115		
SCTZ			\$ (0)	073705 074004
GET	\$ (1)	017116 017137	\$ (0)	074005 074006
IDF	\$ (1)	017140 017215	\$ (2)	IDINFO
PACKZZ	\$ (1)	017216 017360	\$ (0)	074007 074045
	\$ (3)	IDINFO	\$ (2)	BLANK\$COMMON
PLOTSS	\$ (1)	017361 017370	\$ (0)	074046 074051
BUFRZZ	\$ (1)	017371 017625	\$ (0)	074052 074143
			\$ (2)	074144 074413
NOUTS/JSC-E3	\$ (1)	017626 021341	\$ (2)	074414 074455
IDINFO(COMMONBLOCK)				074456 074463
IDENT	\$ (1)	021342 022506	\$ (0)	074464 075753
			\$ (2)	IDINFO
ERRZZ	\$ (1)	022507 022557	\$ (0)	075754 076012
			\$ (2)	BLANK\$COMMON
NOSYMS/JSC-E3	\$ (1)	022560 023024	\$ (2)	076013 076014
EXITG	\$ (1)	023025 023067	\$ (0)	076015 076057
			\$ (2)	BLANK\$COMMON
GETSMG	\$ (1)	023070 023170	\$ (0)	076060 076071

NINTRS/JSC-E3	\$ (1)	023171 023531	\$ (2)	BLANK\$COMMON
KLEAR	\$ (1)	023532 023534	\$ (2)	076072 076141
TPERR	\$ (1)	023535 023584	\$ (0)	076142 076173
	\$ (3)	TAPE	\$ (2)	BLANK\$COMMON
SKFILE	\$ (1)	023565 023640	\$ (0)	076174 076205
			\$ (2)	BLANK\$COMMON
RSRCK	\$ (1)	023641 024075	\$ (0)	076206 076366
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	TAPE	\$ (4)	RSTRT
READHD	\$ (1)	024076 024416	\$ (0)	076367 076575
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	TITLE	\$ (4)	TAPE
	\$ (7)	ISTPDR	\$ (6)	RSTRT
			\$ (010)	ACCESS
STORE	\$ (1)	024417 024553	\$ (0)	076576 076653
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	DSTORE	\$ (4)	TAPE
PDUMP	\$ (1)	024554 025014	\$ (0)	076654 076722
			\$ (2)	BLANK\$COMMON
FINDST	\$ (1)	025015 025303	\$ (0)	076723 077061
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	DSTORE	\$ (4)	TAPE
	\$ (7)	ACCESS	\$ (6)	ISTPDR
SETFLO	\$ (1)	025304 025401	\$ (0)	077062 077102
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	NMODIR	\$ (4)	TITLE
SECOND	\$ (1)	025402 025412	\$ (0)	077103 077104
			\$ (2)	077105 077105
SHIFT	\$ (1)	025413 025422		077106 077107
.LR10DM(COMMONBLOCK)				077110 077123
RIOPAC	\$ (1)	025423 025546	\$ (0)	077110 077123
	\$ (3)	LR10DM	\$ (2)	BLANK\$COMMON
ABT	\$ (1)	025547 025564	\$ (0)	077124 077131
			\$ (2)	BLANK\$COMMON
PAGE	\$ (1)	025565 025714	\$ (0)	077132 077202
	\$ (3)	TAPE	\$ (2)	BLANK\$COMMON
			\$ (4)	TITLE
RETRVE	\$ (1)	025715 026151	\$ (0)	077203 077241
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	TAPE	\$ (4)	TITLE
	\$ (7)	AREA	\$ (6)	NODE
	\$ (011)	ALPH	\$ (010)	EMISS
	\$ (013)	TRSO	\$ (012)	TRIR
	\$ (015)	SRSO	\$ (014)	SRIR
	\$ (017)	ODTEMP	\$ (016)	NMODIR
WRITHD	\$ (1)	026152 026317	\$ (0)	077242 077263
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	RSTRT	\$ (4)	TITLE
	\$ (7)	ACCESS	\$ (6)	ISTPDR
ARRAYS(COMMONBLOCK)				077264 077264
IGS(COMMONBLOCK)				077265 077574
WRAPUP	\$ (1)	026320 026374	\$ (0)	077575 077624
	\$ (3)	TAPE	\$ (2)	BLANK\$COMMON
	\$ (5)	IGS	\$ (4)	PLOTTR
MFPROG	\$ (1)	026375 026404	\$ (0)	077625 077630
			\$ (2)	BLANK\$COMMON

FLPROG	\$ (1)	026405 026414	\$ (0)	077631 077634
QSPROG	\$ (1)	026415 026424	\$ (2)	BLANKSCOMMON
ACPROG	\$ (1)	026425 026434	\$ (0)	077635 077640
DRPROG	\$ (1)	026435 026444	\$ (2)	BLANKSCOMMON
DIPROG	\$ (1)	026445 026454	\$ (0)	077641 077644
OPPROG	\$ (1)	026455 026464	\$ (2)	BLANKSCOMMON
CMPPROG	\$ (1)	026465 026474	\$ (0)	077645 077650
RBPROG	\$ (1)	026475 026504	\$ (2)	BLANKSCOMMON
ACCESS (COMMONBLOCK)	\$ (1)	026505 027242	\$ (0)	077651 077654
PRDUMP	\$ (3)	ALPH	\$ (2)	BLANKSCOMMON
	\$ (5)	CCONST	\$ (4)	AREA
	\$ (7)	NODE	\$ (6)	EMISS
	\$ (011)	TITLE	\$ (010)	TAPE
	\$ (013)	ACCESS	\$ (012)	RSTRT
	\$ (015)	SRIR	\$ (014)	ODTEMP
	\$ (017)	TRIR	\$ (016)	SRSO
			\$ (020)	TRSO
LNGSEG (COMMONBLOCK)				100056 100104
PLOTTR (COMMONBLOCK)				100105 100155
SREFLS (COMMONBLOCK)				100156 100158
SREFLI (COMMONBLOCK)				100157 100157
ISPEC (COMMONBLOCK)				100160 100160
NSPEC (COMMONBLOCK)				100161 100161
ISTPOR (COMMONBLOCK)				100162 100162
DSTORE (COMMONBLOCK)				100163 100226
ORBIT (COMMONBLOCK)				100227 100347
ODTEMP (COMMONBLOCK)				100350 100513
NODE (COMMONBLOCK)				100514 100536
TRSO (COMMONBLOCK)				100537 100561
TRIR (COMMONBLOCK)				100562 100604
SRSO (COMMONBLOCK)				100605 100627
SRIR (COMMONBLOCK)				100630 100652
EMISS (COMMONBLOCK)				100653 100675
AREA (COMMONBLOCK)				100676 100720
ALPH (COMMONBLOCK)				100721 100743
TSTR (COMMONBLOCK)				100744 101460
PSH (COMMONBLOCK)				101461 101704
PR (COMMONBLOCK)				101705 102016
IKS (COMMONBLOCK)				102017 102063
IFS (COMMONBLOCK)				102064 102130
DSTR (COMMONBLOCK)				102131 102421
DIMS (COMMONBLOCK)				102422 102600
INDXN (COMMONBLOCK)				102601 102623
INDXS (COMMONBLOCK)				102624 102646
NMODIR (COMMONBLOCK)				102647 102716
INDX (COMMONBLOCK)				102717 102717
BCSN (COMMONBLOCK)				102720 102727
BLKDIR (COMMONBLOCK)				102730 102767

PLOT(COMMONBLOCK)			102770 103223
TITLE(COMMONBLOCK)			103224 103262
RSTRT(COMMONBLOCK)			103263 103301
TAPE(COMMONBLOCK)			103302 103343
CCONST(COMMONBLOCK)			103344 103550
BLANK\$COMMON(COMMONBLOCK)			

TRASYS	\$ (1)	027243 027365	\$ (0)	103551 103551
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	RSTRT	\$ (4)	TAPE
	\$ (7)	PLOT	\$ (6)	TITLE
	\$ (011)	BCSN	\$ (010)	BLKDIR
	\$ (013)	NMODIR	\$ (012)	INDX
	\$ (015)	INDXM	\$ (014)	INDXS
	\$ (017)	DSTR	\$ (016)	OIMS
	\$ (021)	IKS	\$ (020)	IFS
	\$ (023)	PSH	\$ (022)	PR
	\$ (025)	ALPH	\$ (024)	TSTR
	\$ (027)	EMISS	\$ (026)	AREA
	\$ (031)	SRSO	\$ (030)	SRIR
	\$ (033)	TRSO	\$ (032)	TRIR
	\$ (035)	ODTEMP	\$ (034)	NOOE
	\$ (037)	DSTORE	\$ (036)	ORBIT
	\$ (041)	NSPEC	\$ (040)	ISTPOR
	\$ (043)	SREFLI	\$ (042)	ISPEC
	\$ (045)	PLOTTR	\$ (044)	SREFLS
			\$ (046)	LNGSEQ
NTRANS/JSC	\$ (1)	027366 030660	\$ (2)	103552 104534
	\$ (037)	INFO-010-LC		

SEGMENT RD* 030661 032341 104535 105471
FOLLOWS SEGMENT TR

GETPSR	\$ (1)	030661 031102	\$ (0)	104535 104616
AAAAAA	\$ (1)	031103 031122	\$ (0)	104617 104624
BANNLB	\$ (1)	031123 031217	\$ (2)	BLANK\$COMMON
	\$ (3)	TAPE	\$ (0)	104625 105263
			\$ (2)	BLANK\$COMMON
			\$ (4)	TITLE
UCONST(COMMONBLOCK)				105264 105264
RDMAIN	\$ (1)	031220 032326	\$ (0)	105265 105465
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	ISTPOR	\$ (4)	TAPE
	\$ (7)	PLOTTR	\$ (6)	PLOT
	\$ (011)	LNGSEQ	\$ (010)	TITLE
	\$ (013)	UCONST	\$ (012)	RSTRT
	\$ (015)	BCSN	\$ (014)	ARRAYS
	\$ (017)	INDX	\$ (016)	BLKDIR
	\$ (021)	LRTODM	\$ (020)	DSTORE
			\$ (022)	ODTEMP
RDPROG	\$ (1)	032327 032341	\$ (0)	105466 105471
			\$ (2)	BLANK\$COMMON

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SEGMENT OD* 030661 034523 104535 105730
FOLLOWS SEGMENT TR

I ACT	\$ (1)	030661 030715	\$ (0)	104535 104544
			\$ (2)	BLANK\$COMMON
SORTS	\$ (1)	030716 031224	\$ (0)	104545 104627
			\$ (2)	BLANK\$COMMON
TRS3	\$ (1)	031225 031305	\$ (0)	104630 104638
			\$ (2)	BLANK\$COMMON
RCDATA	\$ (1)	031306 031540	\$ (0)	104637 104673
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	ISTPDR	\$ (4)	TITLE
			\$ (6)	ARRAYS
NDUPCK	\$ (1)	031541 031617	\$ (0)	104674 104712
	\$ (3)	TAPE	\$ (2)	BLANK\$COMMON
	\$ (5)	NODE	\$ (4)	CCONST
			\$ (6)	ODTEMP
NPRNT	\$ (1)	031620 031750	\$ (0)	104713 105022
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
			\$ (4)	TAPE
TRANSF	\$ (1)	031751 032134	\$ (0)	105023 105046
			\$ (2)	BLANK\$COMMON
DIRCOS	\$ (1)	032135 032415	\$ (0)	105047 105140
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
RKDATA	\$ (1)	032416 032473	\$ (0)	105141 105145
			\$ (2)	BLANK\$COMMON
GBDATA	\$ (1)	032474 032614	\$ (0)	105146 105233
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	TAPE	\$ (4)	ISTPDR
			\$ (6)	TITLE
NDA TA	\$ (1)	032615 033152	\$ (0)	105234 105270
	\$ (3)	ARRAYS	\$ (2)	BLANK\$COMMON
	\$ (5)	PLOT	\$ (4)	CCONST
			\$ (6)	TITLE
BUILD C	\$ (1)	033153 034154	\$ (0)	105271 105561
	\$ (3)	BLKDIR	\$ (2)	BLANK\$COMMON
	\$ (5)	TAPE	\$ (4)	DIRECT
	\$ (7)	ALPH	\$ (6)	AREA
	\$ (011)	SRSO	\$ (010)	SRI R
	\$ (013)	TRSO	\$ (012)	TRIR
	\$ (015)	NODE	\$ (014)	EMISS
	\$ (017)	NSPEC	\$ (016)	ISPEC
	\$ (021)	TITLE	\$ (020)	CCONST
	\$ (023)	INDXS	\$ (022)	NHODIR
			\$ (024)	INDXN
INTOD	\$ (1)	034155 034331	\$ (0)	105562 105621
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	LNGSEQ	\$ (4)	ISTPDR
			\$ (6)	TITLE
DIRECT (COMMONBLOCK)				105622 105655
ODPROG	\$ (1)	034332 034523	\$ (0)	105656 105730
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	RSTRT	\$ (4)	TAPE
	\$ (7)	PLOT	\$ (6)	TITLE
	\$ (011)	BCSH	\$ (010)	BLKDIR
	\$ (013)	NHODIR	\$ (012)	INDX
	\$ (015)	INDXN	\$ (014)	INDXS
	\$ (017)	DSTR	\$ (016)	DIMS
	\$ (021)	IKS	\$ (020)	IFS
	\$ (023)	PSH	\$ (022)	PR

\$(025)	ALPH	\$(024)	TSTR
\$(027)	ENISS	\$(026)	AREA
\$(031)	SR50	\$(030)	SRIR
\$(033)	TR50	\$(032)	TRIR
\$(035)	ODTEHP	\$(034)	NODE
\$(037)	DSTORE	\$(036)	ORBIT
\$(041)	NSPEC	\$(040)	ISTPDR
\$(043)	SREFLI	\$(042)	ISPEC
\$(045)	PLOTTR	\$(044)	SREFLS
\$(047)	DIRECT	\$(046)	LN05EO

SEGMENT FF* 030661 064120 104535 123007
FOLLOWS SEGMENT TR

FFGTST	\$(1)	030661 030725	\$(0)	104535 104545
FFVMT	\$(1)	030726 031377	\$(2)	BLANK\$COMMON
FFAREA	\$(3)	CCONST	\$(0)	104546 105640
FFRPSN	\$(1)	031400 031755	\$(2)	BLANK\$COMMON
FFCRSS	\$(3)	CCONST	\$(0)	105641 105674
FFTRS3	\$(1)	031756 033025	\$(2)	BLANK\$COMMON
FFPVH	\$(3)	CCONST	\$(0)	105675 105760
FFXPHI	\$(1)	033026 033062	\$(2)	BLANK\$COMMON
	\$(3)	033063 033143	\$(0)	105761 105765
	\$(5)	RMASS2	\$(2)	BLANK\$COMMON
FFUNTI	\$(1)	033144 033674	\$(0)	105766 105774
FFSHD	\$(3)	CCONST	\$(2)	BLANK\$COMMON
	\$(1)	033675 035630	\$(0)	105775 106103
	\$(3)	CCONST	\$(2)	BLANK\$COMMON
	\$(5)	RMASS2	\$(0)	106104 106431
	\$(6)	RMASS1	\$(2)	BLANK\$COMMON
	\$(1)	035631 036514	\$(4)	FFDAT1
	\$(3)	CCONST	\$(6)	RMASS1
	\$(5)	TAPE	\$(0)	106432 106610
	\$(1)	036515 042155	\$(2)	BLANK\$COMMON
	\$(3)	DIMS	\$(4)	RMASS1
	\$(5)	TSTR	\$(0)	106611 106726
	\$(7)	IKS	\$(2)	BLANK\$COMMON
	\$(011)	PSH	\$(4)	DSTR
	\$(013)	FFSHDC	\$(6)	IFS
	\$(015)	FFVALI	\$(010)	PR
	\$(017)	BFA	\$(012)	CCONST
	\$(021)	FF2RSI	\$(014)	FFVALS
	\$(023)	FF4RSI	\$(016)	BFE
	\$(025)	FFSUMC	\$(020)	FF1RSI
FFEXPN	\$(1)	042156 044111	\$(022)	FF3RSI
	\$(3)	CCONST	\$(024)	FF5RSI
	\$(5)	RMASS1	\$(0)	106727 107254
	\$(6)	RMASS2	\$(2)	BLANK\$COMMON
FFTHCK	\$(1)	044112 044121	\$(4)	FFDAT1
FFPSHD	\$(1)	044122 045066	\$(6)	RMASS2
	\$(3)	DIMS	\$(0)	107255 107260
	\$(5)	TSTR	\$(2)	BLANK\$COMMON
	\$(7)	IKS	\$(0)	107261 107411
			\$(2)	BLANK\$COMMON
			\$(4)	DSTR
			\$(6)	IFS

	\$ (011)	PSH		\$ (010)	PR
	\$ (013)	FFVALS		\$ (012)	FFSHDC
	\$ (015)	BFE		\$ (014)	FFVALI
	\$ (017)	FF1RSI		\$ (016)	BFA
	\$ (021)	FF3RSI		\$ (020)	FF2RSI
	\$ (023)	FF5RSI		\$ (022)	FF4RSI
				\$ (024)	FFSUNC
FFUNIT	\$ (1)	045067 045752		\$ (0)	107412 107570
	\$ (3)	CCONST		\$ (2)	BLANK\$COMMON
	\$ (5)	TAPE		\$ (4)	RMASS2
FFVIEW	\$ (1)	045753 046442		\$ (0)	107571 110663
	\$ (3)	CCONST		\$ (2)	BLANK\$COMMON
FFELEM	\$ (1)	046443 050554		\$ (0)	110664 111004
	\$ (3)	CCONST		\$ (2)	BLANK\$COMMON
FFELSL	\$ (1)	050555 051266		\$ (0)	111005 111045
	\$ (3)	CCONST		\$ (2)	BLANK\$COMMON
FFESUM	\$ (1)	051267 051365		\$ (0)	111046 111111
	\$ (3)	CCONST		\$ (2)	BLANK\$COMMON
	\$ (5)	NODE		\$ (4)	FFDAT1
	\$ (7)	FFSHDC		\$ (6)	TAPE
	\$ (011)	FFVALI		\$ (010)	FFVALS
	\$ (013)	BFA		\$ (012)	BFE
	\$ (015)	FF2RSI		\$ (014)	FF1RSI
	\$ (017)	FF4RSI		\$ (016)	FF3RSI
	\$ (021)	FFSUNC		\$ (020)	FF5RSI
FFPCL	\$ (1)	051366 052331		\$ (0)	111112 111247
	\$ (3)	AREA		\$ (2)	BLANK\$COMMON
	\$ (5)	FFDAT1		\$ (4)	CCONST
	\$ (7)	RMASS1		\$ (6)	NODE
	\$ (011)	DIMS		\$ (010)	RMASS2
	\$ (013)	TSTR		\$ (012)	DSTR
	\$ (015)	IKS		\$ (014)	IFS
	\$ (017)	PSH		\$ (016)	PR
	\$ (021)	FFSHDC		\$ (020)	TAPE
	\$ (023)	FFVALI		\$ (022)	FFVALS
	\$ (025)	BFA		\$ (024)	BFE
	\$ (027)	FF2RSI		\$ (026)	FF1RSI
	\$ (031)	FF4RSI		\$ (030)	FF3RSI
	\$ (033)	FFSUNC		\$ (032)	FF5RSI
	\$ (035)	ELEM		\$ (034)	FFELCH
FFCALI	\$ (1)	052332 053601		\$ (0)	111250 111421
	\$ (3)	AREA		\$ (2)	BLANK\$COMMON
	\$ (5)	FFDAT1		\$ (4)	CCONST
	\$ (7)	RMASS2		\$ (6)	NODE
	\$ (011)	DIMS		\$ (010)	RMASS1
	\$ (013)	TSTR		\$ (012)	DSTR
	\$ (015)	IKS		\$ (014)	IFS
	\$ (017)	PSH		\$ (016)	PR
	\$ (021)	FFSHDC		\$ (020)	TAPE
	\$ (023)	FFVALI		\$ (022)	FFVALS
	\$ (025)	BFA		\$ (024)	BFE
	\$ (027)	FF2RSI		\$ (026)	FF1RSI
	\$ (031)	FF4RSI		\$ (030)	FF3RSI
	\$ (033)	FFSUNC		\$ (032)	FF5RSI
	\$ (035)	ELEM		\$ (034)	FFELCH
FFELCH (COMMON\$LOCK)					111422 117311
FFCAL	\$ (1)	053602 055051		\$ (0)	117312 117463

FFMINR

\$(3) AREA
 \$(5) FFDATI
 \$(7) RMASS1
 \$(011) DIMS
 \$(013) TSTR
 \$(015) IKS
 \$(017) PSN
 \$(021) FFSHDC
 \$(023) FFVALI
 \$(025) BFA
 \$(027) FF2RSI
 \$(031) FF4RSI
 \$(033) FFSUMC
 \$(035) ELEM
 \$(1) 055052 055160
 \$(3) AREA
 \$(5) FFDATI
 \$(7) TAPE
 \$(011) FFVALS
 \$(013) BFE
 \$(015) FF1RSI
 \$(017) FF3RSI
 \$(021) FF5RSI

FFEQIV

\$(1) 055181 055316
 \$(3) CCONST
 \$(5) FFVALI
 \$(7) TAPE
 \$(011) ELEM

FFGEQ

\$(1) 055317 056167
 \$(3) CCONST
 \$(5) NODE
 \$(7) FFVALS
 \$(011) BFE
 \$(013) FF1RSI
 \$(015) FF3RSI
 \$(017) FF5RSI
 \$(021) FFDATI

FFRTR

\$(1) 056170 056427
 \$(3) CCONST
 \$(5) TAPE
 \$(7) FFVALI
 \$(011) BFE
 \$(013) NODE

FFRSMR

\$(1) 056430 056547
 \$(3) CCONST
 \$(5) NODE
 \$(7) TAPE
 \$(011) FFVALS
 \$(013) BFE
 \$(015) FF1RSI
 \$(017) FF3RSI
 \$(021) FF5RSI
 \$(023) AREA

\$(2) BLANK\$COMMON
 \$(4) CCONST
 \$(6) NODE
 \$(010) RMASS2
 \$(012) DSTR
 \$(014) IFS
 \$(016) PR
 \$(020) TAPE
 \$(022) FFVALS
 \$(024) BFE
 \$(026) FF1RSI
 \$(030) FF3RSI
 \$(032) FF5RSI
 \$(034) FFELCH
 \$(0) 117464 117500
 \$(2) BLANK\$COMMON
 \$(4) CCONST
 \$(6) NODE
 \$(010) FFSHDC
 \$(012) FFVALI
 \$(014) BFA
 \$(016) FF2RSI
 \$(020) FF4RSI
 \$(022) FFSUMC
 \$(0) 117501 117540
 \$(2) BLANK\$COMMON
 \$(4) FFDATI
 \$(6) FFVALS
 \$(010) NODE
 \$(0) 117541 117626
 \$(2) BLANK\$COMMON
 \$(4) TAPE
 \$(6) FFSHDC
 \$(010) FFVALI
 \$(012) BFA
 \$(014) FF2RSI
 \$(016) FF4RSI
 \$(020) FFSUMC
 \$(022) ODTEMP
 \$(0) 117627 117705
 \$(2) BLANK\$COMMON
 \$(4) FFDATI
 \$(6) RSTR
 \$(010) FFVALS
 \$(012) BFA
 \$(014) TITLE
 \$(0) 117706 120115
 \$(2) BLANK\$COMMON
 \$(4) FFDATI
 \$(6) RMASS1
 \$(010) FFSHDC
 \$(012) FFVALI
 \$(014) BFA
 \$(016) FF2RSI
 \$(020) FF4RSI
 \$(022) FFSUMC
 \$(024) FFSHO

ELEM(COMMONBLOCK)

FFPRT	\$ (1) 056550 057210	\$ (0) 120116 120117
	\$ (3) AREA	\$ (2) 120120 120346
	\$ (5) FFDAT1	\$ (4) BLANK\$COMMON
	\$ (7) TAPE	\$ (6) CCONST
	\$ (011) FFVALS	\$ (8) NODE
	\$ (013) BFE	\$ (010) FFSHDC
	\$ (015) FF1RSI	\$ (012) FFVALI
	\$ (017) FF3RSI	\$ (014) BFA
	\$ (021) FF5RSI	\$ (016) FF2RSI
	\$ (023) ELEM	\$ (020) FF4RSI
FFPCH	\$ (1) 057211 057506	\$ (022) FFSUMC
	\$ (3) CCONST	\$ (0) 120347 120430
	\$ (5) FFDAT1	\$ (2) BLANK\$COMMON
	\$ (7) FFSHDC	\$ (4) NODE
	\$ (011) FFVALI	\$ (6) TAPE
	\$ (013) BFA	\$ (010) FFVALS
	\$ (015) FF2RSI	\$ (012) BFE
	\$ (017) FF4RSI	\$ (014) FF1RSI
	\$ (021) FFSUMC	\$ (016) FF3RSI
FFRIN	\$ (023) TITLE	\$ (020) FF5RSI
	\$ (1) 057507 060404	\$ (022) 1STPDR
	\$ (3) CCONST	\$ (0) 120431 120566
	\$ (5) NODE	\$ (2) BLANK\$COMMON
	\$ (7) FFSHDC	\$ (4) FFDAT1
	\$ (011) FFVALI	\$ (6) TAPE
	\$ (013) BFA	\$ (010) FFVALS
	\$ (015) FF2RSI	\$ (012) BFE
	\$ (017) FF4RSI	\$ (014) FF1RSI
	\$ (021) FFSUMC	\$ (016) FF3RSI
FFEND	\$ (1) 060405 060425	\$ (020) FF5RSI
	\$ (3) CCONST	\$ (022) OTEMP
	\$ (5) FFSHDC	\$ (0) 120567 120572
	\$ (7) FFVALI	\$ (2) BLANK\$COMMON
	\$ (011) BFA	\$ (4) TAPE
	\$ (013) FF2RSI	\$ (6) FFVALS
	\$ (015) FF4RSI	\$ (010) BFE
	\$ (017) FFSUMC	\$ (012) FF1RSI
	\$ (021) AREA	\$ (014) FF3RSI
FFROW	\$ (1) 060426 060675	\$ (016) FF5RSI
	\$ (3) FFDAT1	\$ (020) NODE
	\$ (5) FFVALS	\$ (0) 120573 120771
	\$ (7) BFE	\$ (2) BLANK\$COMMON
	\$ (011) FF1RSI	\$ (4) FFSHDC
	\$ (013) FF3RSI	\$ (6) FFVALI
	\$ (015) FF5RSI	\$ (010) BFA
	\$ (017) NODE	\$ (012) FF2RSI
	\$ (021) CCONST	\$ (014) FF4RSI
	\$ (023) AREA	\$ (016) FFSUMC
	\$ (025) FFSHO	\$ (020) TITLE
FFRSUM	\$ (1) 060676 061010	\$ (022) RMASS1
	\$ (3) CCONST	\$ (024) TAPE
	\$ (5) NODE	\$ (026) RSTRT
	\$ (7) TAPE	\$ (0) 120772 121206
	\$ (011) FFSHO	\$ (2) BLANK\$COMMON
		\$ (4) FFDAT1
		\$ (6) RMASS1
		\$ (010) AREA

	\$ (013)	FFVALS		\$ (012)	FFSHDC
	\$ (015)	BFE		\$ (014)	FFVALI
	\$ (017)	FF1RSI		\$ (016)	BFA
	\$ (021)	FF3RSI		\$ (020)	FF2RSI
	\$ (023)	FF5RSI		\$ (022)	FF4RSI
FFSF	\$ (1)	061011 061043		\$ (024)	FFSUMC
	\$ (3)	FFDATI		\$ (0)	121207 121214
	\$ (5)	BFA		\$ (2)	BLANK\$COMMON
	\$ (7)	FFVALI		\$ (4)	BFE
				\$ (6)	AREA
FFPRE	\$ (1)	061044 061105		\$ (010)	FFVALS
	\$ (3)	CCONST		\$ (0)	121215 121223
	\$ (5)	FFSHDC		\$ (2)	BLANK\$COMMON
	\$ (7)	FFVALI		\$ (4)	FFDATI
	\$ (011)	BFA		\$ (6)	FFVALS
	\$ (013)	FF2RSI		\$ (010)	BFE
	\$ (015)	FF4RSI		\$ (012)	FF1RSI
	\$ (017)	FFSUMC		\$ (014)	FF3RSI
	\$ (021)	AREA		\$ (016)	FF5RSI
	\$ (023)	RMASS1		\$ (020)	NODE
FFOUT	\$ (1)	061106 061216		\$ (022)	TAPE
	\$ (3)	FFEQ		\$ (0)	121224 121242
	\$ (5)	CCONST		\$ (2)	BLANK\$COMMON
	\$ (7)	NODE		\$ (4)	AREA
	\$ (011)	RSTRT		\$ (6)	FFDATI
	\$ (013)	FFVALS		\$ (010)	TAPE
	\$ (015)	BFE		\$ (012)	FFSHDC
	\$ (017)	FF1RSI		\$ (014)	FFVALI
	\$ (021)	FF3RSI		\$ (016)	BFA
	\$ (023)	FF5RSI		\$ (020)	FF2RSI
				\$ (022)	FF4RSI
FFRDRQ	\$ (1)	061217 061707		\$ (024)	FFSUMC
	\$ (3)	AREA		\$ (0)	121243 121333
	\$ (5)	FFDATI		\$ (2)	BLANK\$COMMON
	\$ (7)	TAPE		\$ (4)	CCONST
	\$ (011)	FFVALS		\$ (6)	NODE
	\$ (013)	BFE		\$ (010)	FFSHDC
	\$ (015)	FF1RSI		\$ (012)	FFVALI
	\$ (017)	FF3RSI		\$ (014)	BFA
	\$ (021)	FF5RSI		\$ (016)	FF2RSI
	\$ (023)	RSTRT		\$ (020)	FF4RSI
FFRDIN	\$ (1)	061710 063242		\$ (022)	FFSUMC
	\$ (3)	ALPH		\$ (0)	121334 121625
	\$ (5)	CCONST		\$ (2)	BLANK\$COMMON
	\$ (7)	FFDATI		\$ (4)	AREA
	\$ (011)	INDXN		\$ (6)	EMISS
	\$ (013)	RMASS1		\$ (010)	INDXS
	\$ (015)	DIMS		\$ (012)	NODE
	\$ (017)	TSTR		\$ (014)	TAPE
	\$ (021)	IKS		\$ (016)	DSTR
	\$ (023)	PSH		\$ (020)	IFS
	\$ (025)	FFVALS		\$ (022)	PR
	\$ (027)	BFE		\$ (024)	FFSHDC
	\$ (031)	FF1RSI		\$ (026)	FFVALI
	\$ (033)	FF3RSI		\$ (030)	BFA
	\$ (035)	FF5RSI		\$ (032)	FF2RSI
				\$ (034)	FF4RSI

	\$ (037) ISTDOR	\$ (036) FFSUNC
	\$ (041) FFSHO	\$ (040) TITLE
FFHEAD	\$ (1) 063243 063341	\$ (042) RSTRT
	\$ (3) TAPE	\$ (0) 121626 122161
		\$ (2) BLANK\$COMMON
CHKACC	\$ (1) 063342 063502	\$ (4) CCONST
	\$ (3) CCONST	\$ (0) 122162 122277
	\$ (5) TITLE	\$ (2) BLANK\$COMMON
		\$ (4) TAPE
FFSHO (COMMONBLOCK)		\$ (6) NHODIR
FF5RS1 (COMMONBLOCK)		122300 122301
FF4RS1 (COMMONBLOCK)		122302 122302
FF3RS1 (COMMONBLOCK)		122303 122303
FF2RS1 (COMMONBLOCK)		122304 122304
FF1RS1 (COMMONBLOCK)		122305 122305
RMASS2 (COMMONBLOCK)		122306 122306
RMASS1 (COMMONBLOCK)		122307 122353
FFDAT1 (COMMONBLOCK)		122354 122420
FFMAIN		122421 122435
	\$ (1) 063503 064105	\$ (0) 122438 122571
	\$ (3) AREA	\$ (2) BLANK\$COMMON
	\$ (5) FFDAT1	\$ (4) CCONST
	\$ (7) INDXN	\$ (6) INDXS
	\$ (011) RMASS1	\$ (010) NODE
	\$ (013) DIMS	\$ (012) RMASS2
	\$ (015) TSTR	\$ (014) DSTR
	\$ (017) IKS	\$ (016) IFS
	\$ (021) PSH	\$ (020) PR
	\$ (023) FFSHDC	\$ (022) TAPE
	\$ (025) FFVAL1	\$ (024) FFVALS
	\$ (027) BFA	\$ (026) BFE
	\$ (031) FF2RS1	\$ (030) FF1RS1
	\$ (033) FF4RS1	\$ (032) FF3RS1
	\$ (035) FFSUNC	\$ (034) FF5RS1
	\$ (037) RSTRT	\$ (036) TITLE
	\$ (041) FFSHO	\$ (040) FFEQ
FFEQ (COMMONBLOCK)		122572 122614
FFSUNC (COMMONBLOCK)		122615 122637
FFSHDC (COMMONBLOCK)		122640 122662
FFRS15 (COMMONBLOCK)		122663 122663
FFRS14 (COMMONBLOCK)		122664 122664
FFRS13 (COMMONBLOCK)		122665 122665
FFRS12 (COMMONBLOCK)		122666 122666
FFRS11 (COMMONBLOCK)		122667 122667
BFA (COMMONBLOCK)		122670 122712
BFE (COMMONBLOCK)		122713 122735
FFVALS (COMMONBLOCK)		122736 122760
FFVAL1 (COMMONBLOCK)		122761 123003
FFPROG		123004 123007
	\$ (1) 064106 064120	\$ (0) BLANK\$COMMON
	\$ (3) FFVAL1	\$ (2) FFVALS
	\$ (5) BFE	\$ (4) BFA
	\$ (7) FFRS11	\$ (6) FFRS12
	\$ (011) FFRS13	\$ (010) FFRS14
	\$ (013) FFRS15	\$ (012) FFSHDC
	\$ (015) FFSUNC	\$ (014) FFEQ
		\$ (016)

SEGMENT SF°
FOLLOWS SEGMENT TR

030661 043643

104335 116121

SFOTST	\$ (1)	030661 030725	\$ (0)	104535 104545
			\$ (2)	BLANK\$COMMON
SFELSL	\$ (1)	030726 031505	\$ (0)	104546 104612
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
SFTR53	\$ (1)	031506 031566	\$ (0)	104613 104621
			\$ (2)	BLANK\$COMMON
SFSHAD	\$ (1)	031567 035141	\$ (0)	104622 104762
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	SFQDS	\$ (4)	SFSHDC
	\$ (7)	SFQDP	\$ (6)	SFQDR
	\$ (011)	DSTR	\$ (010)	DIMS
	\$ (013)	IFS	\$ (012)	TSTR
	\$ (015)	PR	\$ (014)	IKS
	\$ (017)	SFVECC	\$ (016)	PSH
SFSPHS	\$ (1)	035142 035511	\$ (0)	104763 105054
	\$ (3)	DIMS	\$ (2)	BLANK\$COMMON
	\$ (5)	TSTR	\$ (4)	DSTR
	\$ (7)	IKS	\$ (6)	IFS
	\$ (011)	PSH	\$ (010)	PR
	\$ (013)	SFQDS	\$ (012)	SFSHDC
	\$ (015)	SFQDP	\$ (014)	SFQDR
SFELEM	\$ (1)	035512 037628	\$ (0)	105055 105200
	\$ (3)	SFVECC	\$ (2)	BLANK\$COMMON
	\$ (5)	TAPE	\$ (4)	CCONST
SFELAV	\$ (1)	037627 040366	\$ (0)	105201 105257
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
			\$ (4)	SFVECC
SFELMT	\$ (1)	040367 040546	\$ (0)	105260 105276
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
			\$ (4)	SFSURI
SFRDRQ	\$ (1)	040547 040712	\$ (0)	105277 105603
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	ORBIT	\$ (4)	NODE
			\$ (6)	TAPE
SFPRTR	\$ (1)	040713 041124	\$ (0)	105604 105735
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	NODE	\$ (4)	TAPE
			\$ (6)	TITLE
SFRDIN	\$ (1)	041125 042370	\$ (0)	105736 106035
	\$ (3)	NODE	\$ (2)	BLANK\$COMMON
	\$ (5)	SFQDS	\$ (4)	SFSHDC
	\$ (7)	SFQDP	\$ (6)	SFQDR
	\$ (011)	INDXM	\$ (010)	INDXS
	\$ (013)	CCONST	\$ (012)	ORBIT
	\$ (015)	DIMS	\$ (014)	SFSURI
	\$ (017)	TSTR	\$ (016)	DSTR
	\$ (021)	IKS	\$ (020)	IFS
	\$ (023)	PSH	\$ (022)	PR
	\$ (025)	TITLE	\$ (024)	TAPE
	\$ (027)	RSTRT	\$ (026)	ISTPDR
SFVECC (COMMONBLOCK)				106036 113732
SFSURI (COMMONBLOCK)				113733 113777
SFMAIN	\$ (1)	042371 043630	\$ (0)	114000 116001

	\$ (3)	RSTRT		\$ (2)	BLANK\$COMMON
	\$ (5)	AREA		\$ (4)	ORBIT
	\$ (7)	INDXS		\$ (6)	CCONST
	\$ (011)	ISTPDR		\$ (010)	INDXM
	\$ (013)	SFSUR1		\$ (012)	MODE
	\$ (015)	TITLE		\$ (014)	TAPE
				\$ (016)	SFVECC
SFQDS (COMMONBLOCK)					116002 116024
SFQDR (COMMONBLOCK)					116025 116047
SFQDP (COMMONBLOCK)					116050 116072
SFSHDC (COMMONBLOCK)					116073 116115
SFPROG	\$ (1)	043631 043643	\$ (0)		116116 116121
	\$ (3)	SFSHDC	\$ (2)		BLANK\$COMMON
	\$ (5)	SFQDR	\$ (4)		SFQDP
			\$ (6)		SFQDS

SEGMENT NP#	030661	051266	104535	111024
FOLLOWS SEGMENT TR				

ALOGS/FOR-E3	\$ (1)	030661 030777	\$ (2)	104533 104575
NVECZ	\$ (1)	031000 031025	\$ (0)	104576 104577
VECTZ	\$ (1)	031026 031571	\$ (0)	104600 104742
			\$ (2)	BLANK\$COMMON
PUTCZZ	\$ (1)	031572 031610		
GETCZZ	\$ (1)	031611 031627		
SCALZZ	\$ (1)	031630 032124	\$ (0)	104743 104763
			\$ (2)	BLANK\$COMMON
NFLNKS/LL1B11	\$ (1)	032125 032272	\$ (0)	104764 105004
	\$ (013)	DEPTH		
VECSZZ	\$ (1)	032273 033560	\$ (0)	105005 105161
			\$ (2)	BLANK\$COMMON
YMODZ	\$ (1)	033561 033600	\$ (0)	105162 105170
			\$ (2)	BLANK\$COMMON
XMODZ	\$ (1)	033601 033620	\$ (0)	105171 105177
			\$ (2)	BLANK\$COMMON
UNSCZZ	\$ (1)	033621 034004	\$ (0)	105200 105214
			\$ (2)	BLANK\$COMMON
UNYMDZ	\$ (1)	034005 034025	\$ (0)	105215 105224
			\$ (2)	BLANK\$COMMON
UNXMDZ	\$ (1)	034026 034046	\$ (0)	105225 105234
			\$ (2)	BLANK\$COMMON
METAZZ	\$ (1)	034047 035243	\$ (0)	105235 105401
			\$ (2)	BLANK\$COMMON
OBJECTG	\$ (1)	035244 035620	\$ (0)	105402 105451
			\$ (2)	BLANK\$COMMON
SUBJEG	\$ (1)	035621 036216	\$ (0)	105452 105505
			\$ (2)	BLANK\$COMMON
PAGEG	\$ (1)	036217 036430	\$ (0)	105506 105565
			\$ (2)	BLANK\$COMMON
TEXTG	\$ (1)	036431 036544	\$ (0)	105566 105603
			\$ (2)	BLANK\$COMMON
LINESG	\$ (1)	036545 036704	\$ (0)	105604 105640
			\$ (2)	BLANK\$COMMON
RSETMG	\$ (1)	036705 037075	\$ (0)	105641 106210
			\$ (2)	BLANK\$COMMON
SETSMG	\$ (1)	037076 041241	\$ (0)	106211 106343

MODESG/NMC	\$(1)	041242 041302	\$(2)	BLANK\$COMMON
			\$(0)	106344 106353
LINE	\$(1)	041303 041333	\$(2)	BLANK\$COMMON
	\$(3)	IGS	\$(0)	106354 106368
LINEOP	\$(1)	041334 041363	\$(2)	BLANK\$COMMON
	\$(3)	IGS	\$(0)	106367 106375
NUMBER	\$(1)	041364 041421	\$(2)	BLANK\$COMMON
	\$(3)	IGS	\$(0)	106376 106415
HAP	\$(1)	041422 041506	\$(2)	BLANK\$COMMON
	\$(3)	IGS	\$(0)	106416 106434
NPDOTL	\$(1)	041507 042023	\$(2)	BLANK\$COMMON
	\$(3)	NCONST	\$(0)	106435 106505
	\$(5)	PLOT	\$(2)	BLANK\$COMMON
SETBEA	\$(1)	042024 042046	\$(4)	NPMASS
	\$(3)	IGS	\$(0)	106506 106512
NPFPLT	\$(1)	042047 042301	\$(2)	BLANK\$COMMON
	\$(3)	CAL280	\$(0)	106513 106522
NPSCAL	\$(1)	042302 042400	\$(2)	BLANK\$COMMON
	\$(3)	CAL280	\$(0)	106523 106542
NPINFO	\$(1)	042401 042702	\$(2)	BLANK\$COMMON
	\$(3)	CCONST	\$(0)	106543 106720
	\$(5)	TAPE	\$(2)	BLANK\$COMMON
NPTPLT	\$(1)	042703 043042	\$(4)	NCONST
	\$(3)	NCONST	\$(0)	106721 106735
			\$(2)	BLANK\$COMMON
NPAVEC	\$(1)	043043 043551	\$(4)	NPMASS
	\$(3)	CCONST	\$(0)	106736 106770
FRAME	\$(1)	043552 043570	\$(2)	BLANK\$COMMON
	\$(3)	IGS	\$(0)	106771 106776
SYMBOL	\$(1)	043571 043716	\$(2)	BLANK\$COMMON
	\$(3)	IGS	\$(0)	106777 107040
ABSBEA	\$(1)	043717 043762	\$(2)	BLANK\$COMMON
	\$(3)	IGS	\$(0)	107041 107053
CHAROP	\$(1)	043763 044057	\$(2)	BLANK\$COMMON
	\$(3)	IGS	\$(0)	107054 107071
ZNPMAX	\$(1)	044060 044305	\$(2)	BLANK\$COMMON
	\$(3)	HNP	\$(0)	107072 107223
	\$(5)	NODE	\$(2)	BLANK\$COMMON
	\$(7)	INDXS	\$(4)	NCONST
	\$(011)	CCONST	\$(6)	TAPE
NPPARA	\$(1)	044306 044755	\$(010)	INDXN
	\$(3)	CCONST	\$(0)	107224 107300
			\$(2)	BLANK\$COMMON
			\$(4)	NPMASS
NPSPHE	\$(1)	044756 045441	\$(0)	107301 107355
	\$(3)	CCONST	\$(2)	BLANK\$COMMON
			\$(4)	NPMASS
NPCONE	\$(1)	045442 045755	\$(0)	107356 107433
	\$(3)	CCONST	\$(2)	BLANK\$COMMON
	\$(5)	PLOT	\$(4)	NPMASS
NPCYLO	\$(1)	045756 046237	\$(0)	107434 107502
	\$(3)	CCONST	\$(2)	BLANK\$COMMON
	\$(5)	NPMASS	\$(4)	NCONST
NPTRAP	\$(1)	046240 046361	\$(0)	107503 107521
	\$(3)	NPMASS	\$(2)	BLANK\$COMMON
			\$(4)	CCONST
NPDISC	\$(1)	046362 046544	\$(0)	107522 107551

	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
			\$ (4)	NPHASS
NPRECT	\$ (1)	046945 046622	\$ (0)	107552 107584
	\$ (3)	NPHASS	\$ (2)	BLANK\$COMMON
NPAXES	\$ (1)	046623 047075	\$ (0)	107565 107631
	\$ (3)	NCONST	\$ (2)	BLANK\$COMMON
			\$ (4)	NPHASS
NPROTA	\$ (1)	047076 047403	\$ (0)	107632 107727
	\$ (3)	NCONST	\$ (2)	BLANK\$COMMON
			\$ (4)	CCONST
NPCONV	\$ (1)	047404 050130	\$ (0)	107730 110040
	\$ (3)	ARRAYS	\$ (2)	BLANK\$COMMON
	\$ (5)	PLOT	\$ (4)	MNP
	\$ (7)	CCONST	\$ (6)	NCONST
	\$ (011)	TITLE	\$ (010)	TAPE
INIT28	\$ (1)	050131 050225	\$ (0)	110041 110102
	\$ (3)	TAPE	\$ (2)	BLANK\$COMMON
	\$ (5)	IGS	\$ (4)	PLOTTR
CAL280 (COMMONBLOCK)				110103 110105
NPHASS (COMMONBLOCK)				110108 110142
NCONST (COMMONBLOCK)				110143 110201
NPMAIN	\$ (1)	050226 051253	\$ (0)	110202 110775
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	NCONST	\$ (4)	MNP
	\$ (7)	TAPE	\$ (6)	NPHASS
	\$ (011)	AREA	\$ (010)	NODE
	\$ (013)	INXS	\$ (012)	PLOT
	\$ (015)	TITLE	\$ (014)	INDXN
			\$ (016)	CAL280
MNP (COMMONBLOCK)				110778 111020
NPPROG	\$ (1)	051254 051268	\$ (0)	111021 111024
	\$ (3)	MNP	\$ (2)	BLANK\$COMMON

SEGMENT GB*
FOLLOWS SEGMENT TR

030661 037606 104535 107314

WRITHT	\$ (1)	030661 031003	\$ (0)	104535 104556
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	TITLE	\$ (4)	TAPE
	\$ (7)	ISTPOR	\$ (6)	RSTRT
			\$ (010)	ACCESS
GBRT1	\$ (1)	031004 031626	\$ (0)	104557 104741
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	TITLE	\$ (4)	TAPE
	\$ (7)	ISTPOR	\$ (6)	RSTRT
GBINVG	\$ (1)	031627 034700	\$ (0)	104742 105123
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	XSPACE	\$ (4)	TAPE
	\$ (7)	NOROLO	\$ (6)	NOROUN
	\$ (011)	FA	\$ (010)	BLOCK
	\$ (013)	ISTPOR	\$ (012)	SPACE
	\$ (015)	RSTRT	\$ (014)	TITLE
GBEND	\$ (1)	034701 034710	\$ (0)	105124 105127
			\$ (2)	BLANK\$COMMON
GBSCFA	\$ (1)	034711 035716	\$ (0)	105130 105365
	\$ (3)	AREA	\$ (2)	BLANK\$COMMON

	\$ (5)	EMISS	\$ (4)	ALPH
	\$ (7)	SRSO	\$ (6)	SRIR
	\$ (011)	TRSO	\$ (010)	TRIR
	\$ (013)	CCONST	\$ (012)	BLKGB
	\$ (015)	SPACE	\$ (014)	NODE
	\$ (017)	TITLE	\$ (016)	TAPE
	\$ (021)	ACCESS	\$ (020)	RSTRT
	\$ (023)	XSPACE	\$ (022)	ISTPDR
	\$ (025)	BLOCK	\$ (024)	FA
	\$ (027)	NOROLO	\$ (026)	NOROU
GBFFTP	\$ (1)	035717 036165	\$ (0)	105368 105525
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	TAPE	\$ (4)	TITLE
			\$ (6)	NHODIR
GBRSI	\$ (1)	036168 036727	\$ (0)	105528 105657
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	NODE	\$ (4)	TAPE
	\$ (7)	RSTRT	\$ (6)	TITLE
	\$ (011)	FA	\$ (010)	ACCESS
GBPRE	\$ (1)	036730 036737	\$ (0)	105660 105683
			\$ (2)	BLANK\$COMMON
GBHEAD	\$ (1)	036740 036768	\$ (0)	105664 105740
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
			\$ (4)	TAPE
NOROLO (COMMONBLOCK)				105741 106250
NOROU (COMMONBLOCK)				106251 106360
BLOCK (COMMONBLOCK)				106561 106563
GBMAIN	\$ (1)	036767 037573	\$ (0)	106564 106721
	\$ (3)	AREA	\$ (2)	BLANK\$COMMON
	\$ (5)	CCONST	\$ (4)	ALPH
	\$ (7)	NOROU	\$ (6)	BLOCK
	\$ (011)	EMISS	\$ (010)	NOROLO
	\$ (013)	SRIR	\$ (012)	NODE
	\$ (015)	TRIR	\$ (014)	SRSO
	\$ (017)	TAPE	\$ (016)	TRSO
	\$ (021)	NSPEC	\$ (020)	TITLE
	\$ (023)	ACCESS	\$ (022)	LN05E0
BLKGB (COMMONBLOCK)				106722 107217
XSPACE (COMMONBLOCK)				107220 107242
SPACE (COMMONBLOCK)				107243 107265
FA (COMMONBLOCK)				107268 107310
GBPROG	\$ (1)	037574 037608	\$ (0)	107311 107314
	\$ (3)	FA	\$ (2)	BLANK\$COMMON
	\$ (5)	XSPACE	\$ (4)	SPACE
			\$ (6)	BLKGB

SEGMENT RC* 030661 041331 104535 110752
FOLLOWS SEGMENT TR

BTAPE (COMMONBLOCK)				104535 104537
RCBTP	\$ (1)	030661 031013	\$ (0)	104540 105235
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
	\$ (5)	ISTPDR	\$ (4)	TAPE
			\$ (6)	BTAPE
SORTDL	\$ (1)	031014 031422	\$ (0)	105238 105330
			\$ (2)	BLANK\$COMMON

CLEAR	\$ (1)	031423 031445	\$ (0)	105331 105335
RCEND	\$ (1)	031446 031453	\$ (2)	BLANK\$COMMON
	\$ (3)	CCONST	\$ (0)	105336 105341
	\$ (5)	SPCNO	\$ (2)	BLANK\$COMMON
RCPRT	\$ (1)	031458 031681	\$ (4)	NODE
	\$ (3)	RCSUM1	\$ (6)	TAPE
ENDTP	\$ (1)	031662 031764	\$ (0)	105342 105438
	\$ (3)	CCONST	\$ (2)	BLANK\$COMMON
RCPNCH	\$ (1)	031765 032434	\$ (4)	RCSUM2
	\$ (3)	CCONST	\$ (0)	105437 105532
	\$ (5)	RCEMIT	\$ (2)	BLANK\$COMMON
	\$ (7)	RCSUM1	\$ (4)	TAPE
RCPSS2	\$ (1)	032435 033547	\$ (6)	RCARET
	\$ (3)	CCONST	\$ (10)	RCSUM2
	\$ (5)	TITLE	\$ (0)	105716 106043
	\$ (7)	RCEMIT	\$ (2)	BLANK\$COMMON
	\$ (011)	MSND	\$ (4)	TAPE
	\$ (013)	SFS	\$ (6)	RCARET
	\$ (015)	RCVAR	\$ (010)	ISPN
	\$ (017)	RCSUM2	\$ (012)	NDS
RCPSS1	\$ (1)	033550 034447	\$ (014)	SPCNO
	\$ (3)	CCONST	\$ (018)	RCSUM1
	\$ (5)	SPCNO	\$ (0)	106044 106160
	\$ (7)	RCEMIT	\$ (2)	BLANK\$COMMON
	\$ (011)	ISPN	\$ (4)	TAPE
	\$ (013)	NDS	\$ (6)	ODTEMP
RCCMBN	\$ (1)	034450 035037	\$ (010)	RCARET
	\$ (3)	CCONST	\$ (012)	MSND
	\$ (5)	TITLE	\$ (0)	106161 106221
	\$ (7)	RCARET	\$ (2)	BLANK\$COMMON
	\$ (011)	MSND	\$ (4)	TAPE
	\$ (013)	ODTEMP	\$ (6)	RCEMIT
	\$ (015)	SPCNO	\$ (010)	ISPN
RCTRAN	\$ (1)	035040 037030	\$ (012)	NDS
	\$ (3)	TAPE	\$ (014)	SFS
	\$ (5)	NODE	\$ (016)	RCVAR
	\$ (7)	SPCNO	\$ (0)	106222 106443
RCINIT	\$ (1)	037031 037520	\$ (2)	BLANK\$COMMON
	\$ (3)	CCONST	\$ (4)	TITLE
	\$ (5)	TITLE	\$ (6)	NDS
	\$ (7)	RCARET	\$ (0)	106444 106540
	\$ (011)	MSND	\$ (2)	BLANK\$COMMON
	\$ (013)	NODE	\$ (4)	TAPE
	\$ (015)	EMISS	\$ (6)	RCEMIT
RCPRE	\$ (1)	037521 037530	\$ (010)	ISPN
	\$ (3)	CCONST	\$ (012)	NDS
	\$ (5)	SPCNO	\$ (014)	AREA
RCHEAD	\$ (1)	037531 037576	\$ (0)	106541 106544
	\$ (3)	TAPE	\$ (2)	BLANK\$COMMON
			\$ (4)	NODE
			\$ (6)	TAPE
			\$ (0)	106545 107057
			\$ (2)	BLANK\$COMMON
			\$ (4)	CCONST

RCVAR (COMMONBLOCK)
RCHAIN

\$(1) 037577 041316
\$(3) BLKRC
\$(5) TAPE
\$(7) ALPH
\$(011) LNGSEQ
\$(013) MSND
\$(015) SFS
\$(017) NDS
\$(021) DIHS
\$(023) RCARET
\$(025) RCSUM1

\$(0) 107061 107430
\$(2) BLANKSCOMMON
\$(4) CCONST
\$(6) NODE
\$(010) TITLE
\$(012) ISPN
\$(014) ARRAYS
\$(016) SPCNO
\$(020) ODTEMP
\$(022) RCEMIT
\$(024) RCVAR
\$(026) RCSUM2

107060 107060

107431 110224
110225 110247
110250 110272
110273 110316
110317 110342
110343 110368
110367 110412
110413 110436
110437 110602
110603 110748
110747 110752

BLKRC (COMMONBLOCK)
RCSUM2 (COMMONBLOCK)
RCSUM1 (COMMONBLOCK)
RCARET (COMMONBLOCK)
RCEMIT (COMMONBLOCK)
SPCNO (COMMONBLOCK)
SFS (COMMONBLOCK)
NDS (COMMONBLOCK)
MSND (COMMONBLOCK)
ISPN (COMMONBLOCK)
RCPR00

\$(1) 041317 041331
\$(3) ISPN
\$(5) NDS
\$(7) SPCNO
\$(011) RCARET
\$(013) RCSUM2

\$(0) BLANKSCOMMON
\$(2) MSND
\$(4) SFS
\$(6) RCEMIT
\$(010) RCSUM1
\$(012) RCSUM2
\$(014) BLKRC

IBANK DRAWN TO SCALE: 300 WORDS DECIMAL PER DASH

TR (12209)

RC* (4393)

GB* (3542)

NP* (8454)

SF* (5619)

FF* (13984)

OD* (1955)

RD* (817)

DBANK DRAWN TO SCALE: 200 WORDS DECIMAL PER DASH

TR (7538)

RC* (2190)

OB* (1392)

NP* (2232)

SF* (4853)

FF* (7339)

OD* (636)

RD* (477)

SYSS*RLIBS. LEVEL 72-8
END MAP

@COPY,GM 15,RSO
FURPUR 27R1 RL72-8 06/22/78 20:30:00
3 BLOCKS COPIED.

@FREE 15

OUT,A TRASYSR,RSO.
FURPUR 27R1 RL72-8 06/22/78 20:30:01
1 ABS

@COPY,GM DIR,RSO
1 BLOCK COPIED.

@COPY,GM FFR,RSO
1 BLOCK COPIED.

@COPY,GM GBIRR,RSO
1 BLOCK COPIED.

@COPY,GM RIO,RSO
120 BLOCKS COPIED.

@COPY,GM SQNTL,RSO
1 BLOCK COPIED.

@COPY,GM PLSR,RSO
1 BLOCK COPIED.

@COPY,GM TQR,RSO
1 BLOCK COPIED.

@TEST TE/0/S6
INTERVENING STATEMENTS SKIPPED

@TEST TE/1/S3
INTERVENING STATEMENTS SKIPPED

@JUMP L6
INTERVENING STATEMENTS SKIPPED

@L6;FREE ES3-TRASYS*LIBRYN.

@ASG,T DI.,F17/0/TRK/320

@ASG,T GB1R.,F17/0/TRK/320

@ASG,T GBS0.,F17/0/TRK/320

@ASG,T FF.,F17/0/POS/9

@ASG,T PLS.,F17/0/TRK/320

@ASG,T TQ.,F17/0/TRK/320

0ASG.T RARR..F17/0/TRK/320

0ASG.T SCRR..F17/0/POS/10

0USE 4,SCRR

0USE 9,FF

0USE 10,DI

0USE 11,G01R

0USE 12,G0S0

0USE 13,PLS

0USE 14,MASS2

0USE 15,RS0

0USE 17,RTI

0USE 18,RT0

0USE 19,USER1

0USE 20,USER2

0USE 24,RARR

0USE 27.TQ

0USE 28.TRAJ

0USE 29.BCDOU

0ENABLE, *RSS
FURPUR 27R1 RL72-B 06/22/78 20:30:57
ES3-N03711*RSS(1)
HAS NOT BEEN DISABLED

0XQT TRASYSP

NASA/MARTIN MARIETTA
THERMAL RADIATION ANALYSIS SYSTEM
UNIVAC 1110/EXEC 8

TTTTTTTTTTTT
TTTTTTTTTTTT
TT TTT TT
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RRRRRRRR
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RRR RRR

AAAAAA
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PROCESSOR EXECUTION

VERSION.MODIFICATION ... UL2EG
MODIFICATION DATE 061978

DATE OF RUN 062278
TIME OF RUN 203529
JOB NUMBER RVMH01

DATE 062276 TIME 203532

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 1

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
PROCESSING OPERATIONS DATA

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

SEQUENCE	NODE	BOS	AREA	ALPH	EMISS	SURF. TYPE	ACTIVE	-----COMMENTS-----
1	1	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
2	2	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
3	3	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
4	4	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
5	11	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
6	12	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
7	13	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
8	14	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
9	5	LIDINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT LID
10	15	LIDINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER LEFT LID
11	21	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
12	22	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
13	23	BOXOUT	1.04040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
14	24	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
15	25	BOXOUT	1.04040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
16	26	LIDOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACE OF LID

NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE.
BY -BUILDG- (ACCESS NUMBER = 1)

DATE 062278 TIME 203559 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 2
 MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPLLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
 NODE PLOTTER DATA OUTPUT

NODE PLOTTER

PARAMETER	DESCRIPTION	OPTION #.	DEFAULT
NV	VIEW NUMBER	1-6	1
IVU	VIEW	3HALL 3H3-D 1HX 1HY 1HZ 3HGEN	3HALL
SCL	SCALE FACTOR (3.15/LARGEST DISTANCE FROM CCS ORIGIN IN USER S UNITS)		AUTOMATIC SCALE
NACT	ACTIVE SIDE ARROW FLAG	YES , NO	NO
ISHO	SHADOWER-ONLY SURFACE PLOT FLAG	YES, NO	NO
ISELN	ARRAY NAME CONTAINING NUMBER OF NODES TO BE SELECTIVELY PLOTTED	ARRAY NAME	PLOTS ALL NODES
ITIT	ARRAY NAME OF PLOT TITLE	AY NAME	USES JOB TITLE
ROTX, ROTY, ROTZ.	VIEW ROTATIONS (FOR IVU = 3HGEN)	0 : ANG : 360	0.0 0.0 0.0
IROTX, IROTY, IROTZ	ORDER OF ROTATIONS (FOR IVU = 3HGEN)	1,2,3 (ANY ORDER)	1,2,3

*INPUT ZERO FOR DEFAULT ACTION

CALLING SEQUENCE-

CALL NDATA (NV, IVU, SCL, NACT, ISHO, ISELN, ITIT, ROTX, ROTY, ROTZ, IROTX, IROTY, IROTZ)

OR

CALL NDATAS (NV, IVU, SCL)

NOTE- IF NO CALLS TO NDATA/NDATAS ARE MADE, A CALL TO NPLLOT WILL RESULT IN ALL VIEWS AUTOMATICALLY SCALED GENERATED FOR NODES.

DATE 062278 TIME 203608 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 3
MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
NODE PLOTTER DATA OUTPUT

VIEW=3-D	SCALE= 1.2261	VIEW NUMBER=1
VIEW=Z-AXIS	SCALE= 1.2261	VIEW NUMBER=1
VIEW=X-AXIS	SCALE= 1.2261	VIEW NUMBER=1
VIEW=Y-AXIS	SCALE= 1.2261	VIEW NUMBER=1

DATE 062278 TIME 203620

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 4

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 1 - WPLLOT/SFCAL/FFCAL/OBCAL/RKCAL - ORIGINAL RUN

		CLOCK ANGLE																			
MODE	1	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONC
SHADOW TABLE																					ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
		.00	.00	.00	.00	.00	.81	.64	.33	.11	.00	.00	.17	.67	1.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	.58	.42	.19	.08	.00	.00	.00	.03	1.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.19	.25	.17	.08	.00	.00	.00	.17	.61	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
MODE	1	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONC
SHADOW TABLE																					ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
		.00	.00	.00	.00	.00	.81	.64	.33	.11	.00	.00	.17	.67	1.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	.58	.42	.19	.08	.00	.00	.00	.03	1.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.19	.25	.17	.08	.00	.00	.00	.17	.61	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062278 TIME 203656

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 5

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

		CLOCK ANGLE																			
NODE	2	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW TABLE																					ANGLE
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.61	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.06	.17	.33	.44	.56	.58	.61	22.5
		.42	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.42	.64	.61	.58	.42	45.0
		.19	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.61	.42	.25	.22	.19	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE	2	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW TABLE																					ANGLE
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.61	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.06	.17	.33	.44	.56	.58	.61	22.5
		.42	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.42	.64	.61	.58	.42	45.0
		.19	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.61	.42	.25	.22	.19	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																		CONE ANGLE
NODE	3	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
SOLAR SHADOW TABLE																				
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.06	.08	.03	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.81	.53	.31	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.33	.83	1.00	45.0
		.33	.42	.31	.25	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.25	.72	.50	.50	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																		CONE ANGLE
NODE	3	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
INFRA RED SHADOW TABLE																				
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.06	.08	.03	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.81	.53	.31	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.33	.83	1.00	45.0
		.33	.42	.31	.25	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.25	.72	.50	.50	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062270 TIME 203708 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 7
 MODEL=SAFPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
 SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																			
NODE	4	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR SHADOW TABLE																					CONE ANGLE
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.67	.56	.36	.39	.39	.28	.11	.00	.00	.00	.00	.00	.00	.17	.33	.50	.50	.67	.67	22.5
		.00	.00	.06	.08	.00	.00	.06	.00	.00	.00	.00	.00	.03	.28	.64	.50	.17	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE	4	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED SHADOW TABLE																					CONE ANGLE
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.67	.56	.36	.39	.39	.28	.11	.00	.00	.00	.00	.00	.00	.17	.33	.50	.50	.67	.67	22.5
		.00	.00	.06	.08	.00	.00	.06	.00	.00	.00	.00	.00	.03	.28	.64	.50	.17	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062278 TIME 203714 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 8

MODEL=SAHPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																			
NODE 11		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW	TABLE																				ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		.00	.00	.00	.00	.00	1.00	.67	.17	.00	.00	.11	.33	.64	.81	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	1.00	.03	.00	.00	.00	.06	.19	.42	.59	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.61	.17	.00	.00	.00	.08	.17	.25	.19	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE 11		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW	TABLE																				ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		.00	.00	.00	.00	.00	1.00	.67	.17	.00	.00	.11	.33	.64	.81	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	1.00	.03	.00	.00	.00	.06	.19	.42	.59	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.61	.17	.00	.00	.00	.08	.17	.25	.19	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

		CLOCK ANGLE																				
NODE		12	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR SHADOW TABLE																					CONE ANGLE	
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.61	.58	.56	.44	.33	.17	.06	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.61	22.5
		.42	.58	.61	.64	.42	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.42	45.0
		.19	.22	.25	.42	.61	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.19	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																					
NODE	12	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.			
INFRA RED SHADOW TABLE																						CONE ANGLE	
	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0		
	.61	.58	.56	.44	.33	.17	.06	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.61	22.5		
	.42	.58	.61	.64	.42	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.42	45.0		
	.19	.22	.25	.42	.61	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.19	67.5		
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0		
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5		
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0		
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5		
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0		

DATE 062278 TIME 203732

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 10

MODEL=SAFPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 1 - M/PLOT/SFCAL/FFCAL/GBAL/RKCAL - ORIGINAL RUN

		CLOCK ANGLE																		CONE	
NODE	13	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	ANGLE
SOLAR																					
SHADOW TABLE		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.03	.08	.06	.00	22.5
	1.00	1.00	.83	.33	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.31	.53	.81	1.00	45.0
	.33	.50	.50	.72	.25	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.25	.31	.42	.33	67.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																		CONE	
NODE	13	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	ANGLE
INFRA RED																					
SHADOW TABLE		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.03	.08	.06	.00	22.5
	1.00	1.00	.83	.33	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.31	.53	.81	1.00	45.0
	.33	.50	.50	.72	.25	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.25	.31	.42	.33	67.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062278 TIME 203751 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 11

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

CLOCK ANGLE

NODE 14 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

SOLAR SHADOW TABLE

CONE ANGLE

.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
.67	.67	.50	.50	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.28	.39	.39	.36	.56	.67	22.5
.00	.00	.17	.50	.64	.28	.03	.00	.00	.00	.00	.00	.00	.06	.00	.00	.08	.06	.00	.00	45.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

CLOCK ANGLE

NODE 14 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

INFRA RED SHADOW TABLE

CONE ANGLE

.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
.67	.67	.50	.50	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.28	.39	.39	.36	.56	.67	22.5
.00	.00	.17	.50	.64	.28	.03	.00	.00	.00	.00	.00	.00	.06	.00	.00	.08	.06	.00	.00	45.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062270 TIME 203758

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 12

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 1 - NSLOT/SFCAL/FFCAL/OBCAL/RKCAL - ORIGINAL RUN

		CLOCK ANGLE																			
NODE	5	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																				CONE	
SHADOW TABLE																				ANGLE	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0
		1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
		.67	.56	.67	.67	.72	.72	.00	.00	.00	.00	.00	.00	.00	.14	.14	.33	.50	.50	.67	112.5
		.33	.39	.33	.31	.33	.33	.31	.22	.11	.00	.00	.00	.00	.00	.00	.00	.17	.33	.33	135.0
		.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE	5	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																				CONE	
SHADOW TABLE																				ANGLE	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0
		1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
		.67	.56	.67	.67	.72	.72	.00	.00	.00	.00	.00	.00	.00	.14	.14	.33	.50	.50	.67	112.5
		.33	.39	.33	.31	.33	.33	.31	.22	.11	.00	.00	.00	.00	.00	.00	.00	.17	.33	.33	135.0
		.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062278 TIME 203803

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 13

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

		CLOCK ANGLE																			
NODE 15		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0
		1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
		.67	.50	.50	.33	.14	.14	.00	.00	.00	.00	.00	.00	.00	.72	.72	.67	.67	.56	.67	112.5
		.33	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.22	.31	.33	.33	.31	.33	.39	.33	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE 15		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0
		1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
		.67	.50	.50	.33	.14	.14	.00	.00	.00	.00	.00	.00	.00	.72	.72	.67	.67	.56	.67	112.5
		.33	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.22	.31	.33	.33	.31	.33	.39	.33	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062278 TIME 203812 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 14
 MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
 SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																			
NODE	21	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

		CLOCK ANGLE																			
NODE	21	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

DATE 062278 TIME 203820 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 15
 MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
 SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																				
NODE	22	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
SOLAR SHADOW TABLE		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	CONE ANGLE	
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		22.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		45.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		90.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		112.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		135.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		180.0

		CLOCK ANGLE																				
NODE	22	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
INFRA RED SHADOW TABLE		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	CONE ANGLE	
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		22.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		45.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		90.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		112.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		135.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00		157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		180.0

DATE 062270 TIME 203025 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 16

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPLT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																				
NODE	23	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
SOLAR SHADOW TABLE		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	CONE ANGLE	.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		45.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		67.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		90.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		112.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		135.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		180.0

		CLOCK ANGLE																				
NODE	23	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
INFRA RED SHADOW TABLE		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	CONE ANGLE	.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		45.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		67.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		90.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		112.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		135.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		180.0

DATE 062278 TIME 203034

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 17

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

CLOCK ANGLE

NODE 24 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

SOLAR
SHADOW TABLECONE
ANGLE

1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	22.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	45.0
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	157.5
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

CLOCK ANGLE

NODE 24 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

INFRA RED
SHADOW TABLECONE
ANGLE

1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	22.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	45.0
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	157.5
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

DATE 062278 TIME 203843 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC @ VERSION PAGE 18
 MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPLT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
 SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																				
NODE	25	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
SOLAR SHADOW TABLE		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	CONE ANGLE	.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		22.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		45.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		67.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		90.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		112.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		135.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		180.0

		CLOCK ANGLE																				
NODE	25	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
INFRA RED SHADOW TABLE		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	CONE ANGLE	.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		22.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		45.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		67.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		90.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		112.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		135.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00		157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		180.0

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DATE 052270 TIME 203050

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 19

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

CLOCK ANGLE
NODE 26 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

SOLAR SHADOW TABLE	CLOCK ANGLE																			CONE ANGLE
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	22.5
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	45.0
.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

CLOCK ANGLE
NODE 26 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

INFRA RED SHADOW TABLE	CLOCK ANGLE																			CONE ANGLE
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	22.5
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	45.0
.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

SHADOW FACTORS FOR CONFIGURATION CASE1 HAVE BEEN STORED ON RSO.
LAST RECORD WRITTEN = 52

TOTAL TIME FOR SHADOW FACTOR TABLES 46.4

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPLT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
FORM FACTOR CALCULATION LINK.

FORM FACTORS AND COMBINED FORM FACTORS - USER INPUT AND DEFAULT PARAMETERS

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
FFACC	.0500	.0500	ORIENTATION ACCURACY PARAMETER	N/A
FFACCS	.1000	.1000	SHADOWING ACCURACY PARAMETER	N/A
FFMIN	.1-05	1.0E-06	PARAMETER TO ELIMINATE SMALL FORM FACTORS	N/A
FFNOSH	SHAD	SHAD	OVER RIDE SHADOWING PARAMETER	(SHAD,NOSH)
*FFPNCH	NO	NO	PARAMETER TO PUNCH FORM FACTORS	(YES,NO)
FFPRNT	YES	YES	FLAG FOR COMPREHENSIVE FF AND CM PRINT	(YES,NO,FF,CM,RB)
FFRATL	15.0	15.0	RATIO FOR USING SUB-NODE TECHNIQUE	N/A
FFCHB	NO	CORR	FLAG FOR COMBINING FORM FACTORS	(YES,NO,AUTO,CORR)

* -FFPNCH WILL DEFAULT TO -YES- ON CALCULATED VALUES IF THE -RSO- FILE IS NOT SPECIFIED IN THE OPTIONS DATA BLOCK

DATE 062278 TIME 203853

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/OBCAL/RKCAL - ORIGINAL RUN

SEQUENCE	NODE	AREA	ALPH	EMISS
1	1	1.00000	.800	.900
2	2	1.00000	.900	.900
3	3	1.00000	.800	.900
4	4	1.00000	.800	.900
5	11	1.00000	.900	.900
6	12	1.00000	.800	.900
7	13	1.00000	.900	.900
8	14	1.00000	.900	.900
9	5	1.00000	.900	.900
10	15	1.00000	.900	.900
11	21	2.06040	.200	.900
12	22	2.06040	.200	.900
13	23	1.04040	.200	.900
14	24	2.06040	.200	.900
15	25	1.04040	.200	.900
16	26	2.06040	.200	.900

NUMBER OF NODES = 16 NUMBER OF SURFACES = 10

MODEL=SAMPLE CONFIG=CASE1 STEP=-1

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RXCAL - ORIGINAL RUN

FORM FACTOR CALCULATION LINK.

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ	
1	2	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	16.359	1108	1108	*
1	3	CAL	.201522	.201522	.201522	.201522	.201522	1.000000	1.000000	.417	36	36	
1	4	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	16.418	1108	1108	*
1	12	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.231	36	36	
1	13	CAL	.086058	.086058	.086058	.086058	.086058	1.000000	1.000000	.290	36	36	
1	14	CAL	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	16.627	1024	1024	*
1	5	CAL	.137203	.137203	.137203	.137203	.137203	1.000000	1.000000	.436	36	36	
1	15	CAL	.056006	.056006	.056006	.056006	.056006	1.000000	1.000000	.235	36	36	
1	FF SUM = .9690		ROW CP TIME = 51.084										
1	FORM FACTOR RESTART (RSO) RECORD = 56												
2	3	EQUIV	.207379	.207379	.207379	.207379	.000000	1.000000	1.000000	.005	0	0	
2	4	EQUIV	.207379	.207379	.207379	.207379	.000000	1.000000	1.000000	.001	0	0	
2	11	EQUIV	.032922	.032922	.032922	.032922	.000000	.000000	.000000	.001	0	0	
2	12	CAL	.068832	.068832	.068832	.068832	.068832	1.000000	1.000000	.265	36	36	
2	13	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.218	36	36	
2	14	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.234	36	36	
2	5	CAL	.096343	.096343	.096343	.096343	.096343	1.000000	1.000000	15.431	1024	1024	*
2	15	CAL	.034262	.034262	.034262	.034262	.034262	1.000000	1.000000	.223	36	36	
2	FF SUM = .9203		ROW CP TIME = 18.445										
2	FORM FACTOR RESTART (RSO) RECORD = 57												
3	4	EQUIV	.207379	.207379	.207379	.207379	.000000	1.000000	1.000000	.004	0	0	
3	11	EQUIV	.086058	.086058	.086058	.086058	.000000	.000000	.000000	.001	0	0	
3	12	EQUIV	.032922	.032922	.032922	.032922	.000000	1.000000	1.000000	.003	0	0	
3	14	CAL	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	16.246	1024	1024	*
3	5	CAL	.050426	.050426	.050426	.050426	.050426	1.000000	1.000000	15.560	1024	1024	*
3	15	CAL	.011660	.011660	.011660	.011660	.011660	1.000000	1.000000	15.634	1024	1024	*
3	FF SUM = .8378		ROW CP TIME = 47.510										

DATE 062270 TIME 204133

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIT/AC EXEC 0 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
FORM FACTOR RESTART (RSO) RECORD = 58												
4	11	EQUIV	.040501	.040501	.040501	.040501	.000000	.000000	.000000	.004	0	0
4	12	EQUIV	.032922	.032922	.032922	.032922	.000000	1.000000	1.000000	.004	0	0
4	13	EQUIV	.040501	.040501	.040501	.040501	.000000	1.000000	1.000000	.005	0	0
4	5	CAL	.107798	.107798	.107798	.107798	.107798	1.000000	1.000000	.290	36	36
4	15	CAL	.056851	.056851	.056851	.056851	.056851	1.000000	1.000000	.233	36	36
4	FF SUM = .8007		ROW CP TIME = .588									
FORM FACTOR RESTART (RSO) RECORD = 59												
11	12	EQUIV	.207379	.207379	.207379	.207379	.000000	1.000000	1.000000	.004	0	0
11	13	EQUIV	.201522	.201522	.201522	.201522	.000000	1.000000	1.000000	.001	0	0
11	14	EQUIV	.207379	.207379	.207379	.207379	.000000	1.000000	1.000000	.001	0	0
11	5	EQUIV	.056006	.056006	.056006	.056006	.000000	1.000000	1.000000	.001	0	0
11	15	EQUIV	.137203	.137203	.137203	.137203	.000000	1.000000	1.000000	.001	0	0
11	FF SUM = .9690		ROW CP TIME = .052									
FORM FACTOR RESTART (RSO) RECORD = 60												
12	13	EQUIV	.207379	.207379	.207379	.207379	.000000	1.000000	1.000000	.005	0	0
12	14	EQUIV	.207379	.207379	.207379	.207379	.000000	1.000000	1.000000	.001	0	0
12	5	EQUIV	.034262	.034262	.034262	.034262	.000000	1.000000	1.000000	.001	0	0
12	15	EQUIV	.096343	.096343	.096343	.096343	.000000	1.000000	1.000000	.001	0	0
12	FF SUM = .9203		ROW CP TIME = .049									
FORM FACTOR RESTART (RSO) RECORD = 61												
13	14	EQUIV	.207379	.207379	.207379	.207379	.000000	1.000000	1.000000	.003	0	0
13	5	EQUIV	.011660	.011660	.011660	.011660	.000000	1.000000	1.000000	.001	0	0
13	15	EQUIV	.050426	.050426	.050426	.050426	.000000	1.000000	1.000000	.001	0	0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUES OF RS1, RT1, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
13		FF SUM = .8378 FORM FACTOR RESTART (RS0) RECORD = 62										
14	5	EQUIV	.056851	.056851	.056851	.056851	.000000	1.000000	1.000000	.004	0	0
14	15	EQUIV	.107798	.107798	.107798	.107798	.000000	1.000000	1.000000	.002	0	0
14		FF SUM = .9007 FORM FACTOR RESTART (RS0) RECORD = 63										
5		FF SUM = .5505 FORM FACTOR RESTART (RS0) RECORD = 64										
15		FF SUM = .5505 FORM FACTOR RESTART (RS0) RECORD = 65										
21		FF SUM = .0000 FORM FACTOR RESTART (RS0) RECORD = 66										
22		FF SUM = .0000 FORM FACTOR RESTART (RS0) RECORD = 66										

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THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
FORM FACTOR RESTART (RSO) RECORD = 67												
23		FF SUM = .0000								ROW CP TIME = .007		
FORM FACTOR RESTART (RSO) RECORD = 68												
24		FF SUM = .0000								ROW CP TIME = .011		
FORM FACTOR RESTART (RSO) RECORD = 69												
25		FF SUM = .0000								ROW CP TIME = .007		
FORM FACTOR RESTART (RSO) RECORD = 70												
26		FF SUM = .0000								ROW CP TIME = .006		
FORM FACTOR RESTART (RSO) RECORD = 71												

FF FORM FACTORS FOR CONFIGURATION CASE1 HAVE BEEN STORED ON RSO.
LAST RESTART RECORD WRITTEN = 71

MODEL=SAMPLE CONFIG=CASE1 STEP=1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

SUMMARY OF FORM FACTOR SUMS FOR ALL NODES

NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM
1- .9690	2- .9203	3- .8378	4- .9007	11- .9690	12- .9203
13- .8378	14- .9007	5- .5505	15- .5505	21- .0000	22- .0000
23- .0000	24- .0000	25- .0000	26- .0000		
TOTAL TIME FOR FORM FACTOR SEGMENT		116.634			
TOTAL TIME SINCE START OF RUN		215.549			

DATE 062278 TIME 204140 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 27

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - NPLT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN
GRAY BODIES COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	GREY BODIES DEFINITION	OPTIONS
GBMBND	BOTH	BOTH	WAVEBAND DEFINITION PARAMETER	(2H1R.3HSOL.4HBOTH)

.....

IR GRAY BODIES FOR CONFIGURATION CASE1 HAVE BEEN COMPUTED AND STORED ON RSO.
LAST RESTART RECORD WRITTEN = 89

.....

.....

SOL GRAY BODIES FOR CONFIGURATION CASE1 HAVE BEEN COMPUTED AND STORED ON RSO.
LAST RESTART RECORD WRITTEN = 107

.....

TOTAL TIME TO COMPUTE GRAY BODIES .83

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
 RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

VARIABLE NAME	CURRENT VALUE	DEFAULT	RADIATION CONDUCTORS	OPTIONS
			DEFINITION	
RKPNCH	PUN	NO	PUNCH/NO PUNCH PARAMETER FOR RADKS	(YES,NO)
RKMIN	.0001	0.0001	PARAMETER TO ELIMINATE SMALL RADK S	N/A
IRKCN	1	1	INITIAL RADIATION CONDUCTOR ID NUMBER	N/A
RKSP	SPACE	NO	MNEHONIC FLAG FOR COMPUTATION OF RADKS TO SPACE	(SPACE,NO)
IRKNSP	999	32767	SPACE NODE ID NUMBER	N/A
SIGMA	.17-08	1.713E-9	STEFAN-BOLTZMANN CONSTANT	N/A
RKAMPF	1.00	1.0	AREA MULTIPLYING FACTOR	N/A
RKTAPE	NO	NO	PARAMETER TO OUTPUT TO BCD TAPE	(TAPE,NO)
RFRAC	.7+00	0.7	SIGNIFICANT RADIATION FRACTION	(0. TO 1.)
RTOL	.990	0.99	DECIMAL FRACTION OF LAST RADK SAVED	N/A
NERN	0	0	EFFECTIVE RADIATION NODE (ERN) NUMBER	N/A

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THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 29

MODEL=SAHPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

SPECIAL RADIATION NODES

NONE

MESS SPECIAL NODES

PRIMARY SECONDARY

NONE

DATE 062278 TIME 204148

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

RADIATION CONDUCTOR (RADKS) CARDS

AREA UNITS = INPUT UNITS * AMPF. WHERE AMPF = 1.00000

PUNCHED AND/OR BCDOU RADKS -	-	1.	1.	2.	.30388-09\$
PUNCHED AND/OR BCDOU RADKS -	-	2.	1.	3.	.29434-09\$
PUNCHED AND/OR BCDOU RADKS -	-	3.	1.	4.	.30399-09\$
PUNCHED AND/OR BCDOU RADKS -	-	4.	1.	11.	.12030-10\$
PUNCHED AND/OR BCDOU RADKS -	-	5.	1.	12.	.55485-10\$
PUNCHED AND/OR BCDOU RADKS -	-	6.	1.	13.	.12522-09\$
PUNCHED AND/OR BCDOU RADKS -	-	7.	1.	14.	.64507-10\$
PUNCHED AND/OR BCDOU RADKS -	-	8.	1.	5.	.19915-09\$
PUNCHED AND/OR BCDOU RADKS -	-	9.	1.	15.	.82979-10\$
PUNCHED AND/OR BCDOU RADKS -	-	10.	2.	3.	.30243-09\$
PUNCHED AND/OR BCDOU RADKS -	-	11.	2.	4.	.30341-09\$
PUNCHED AND/OR BCDOU RADKS -	-	12.	2.	11.	.55485-10\$
PUNCHED AND/OR BCDOU RADKS -	-	13.	2.	12.	.10306-09\$
PUNCHED AND/OR BCDOU RADKS -	-	14.	2.	13.	.54412-10\$
PUNCHED AND/OR BCDOU RADKS -	-	15.	2.	14.	.54024-10\$
PUNCHED AND/OR BCDOU RADKS -	-	16.	2.	5.	.14389-09\$
PUNCHED AND/OR BCDOU RADKS -	-	17.	2.	15.	.54005-10\$
PUNCHED AND/OR BCDOU RADKS -	-	18.	3.	4.	.30228-09\$
PUNCHED AND/OR BCDOU RADKS -	-	19.	3.	11.	.12522-09\$
PUNCHED AND/OR BCDOU RADKS -	-	20.	3.	12.	.54412-10\$
PUNCHED AND/OR BCDOU RADKS -	-	21.	3.	13.	.89273-11\$
PUNCHED AND/OR BCDOU RADKS -	-	22.	3.	14.	.63116-10\$
PUNCHED AND/OR BCDOU RADKS -	-	23.	3.	5.	.81540-10\$
PUNCHED AND/OR BCDOU RADKS -	-	24.	3.	15.	.23578-10\$
PUNCHED AND/OR BCDOU RADKS -	-	25.	4.	11.	.64507-10\$
PUNCHED AND/OR BCDOU RADKS -	-	26.	4.	12.	.54024-10\$
PUNCHED AND/OR BCDOU RADKS -	-	27.	4.	13.	.63116-10\$
PUNCHED AND/OR BCDOU RADKS -	-	28.	4.	14.	.90305-11\$
PUNCHED AND/OR BCDOU RADKS -	-	29.	4.	5.	.15910-09\$
PUNCHED AND/OR BCDOU RADKS -	-	30.	4.	15.	.83921-10\$
PUNCHED AND/OR BCDOU RADKS -	-	31.	11.	12.	.30388-09\$
PUNCHED AND/OR BCDOU RADKS -	-	32.	11.	13.	.29434-09\$
PUNCHED AND/OR BCDOU RADKS -	-	33.	11.	14.	.30399-09\$
PUNCHED AND/OR BCDOU RADKS -	-	34.	11.	5.	.82979-10\$
PUNCHED AND/OR BCDOU RADKS -	-	35.	11.	15.	.19915-09\$
PUNCHED AND/OR BCDOU RADKS -	-	36.	12.	13.	.30243-09\$
PUNCHED AND/OR BCDOU RADKS -	-	37.	12.	14.	.30341-09\$
PUNCHED AND/OR BCDOU RADKS -	-	38.	12.	5.	.54005-10\$
PUNCHED AND/OR BCDOU RADKS -	-	39.	12.	15.	.14389-09\$
PUNCHED AND/OR BCDOU RADKS -	-	40.	13.	14.	.30228-09\$

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THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 31

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

RADIATION CONDUCTOR (RADK) CARDS

AREA UNITS = INPUT UNITS * AMPF, WHERE AMPF = 1.00000

PUNCHED AND/OR BCD0U RADKS -	-	41,	13,	5,	.23578-10\$
PUNCHED AND/OR BCD0U RADKS -	-	42,	13,	15,	.81540-10\$
PUNCHED AND/OR BCD0U RADKS -	-	43,	14,	5,	.83921-10\$
PUNCHED AND/OR BCD0U RADKS -	-	44,	14,	15,	.15910-09\$
PUNCHED AND/OR BCD0U RADKS -	-	45,	5,	15,	.52902-11\$
PUNCHED AND/OR BCD0U RADKS -	-	46,	1,	999,	.76855-10\$
PUNCHED AND/OR BCD0U RADKS -	-	47,	2,	999,	.14541-09\$
PUNCHED AND/OR BCD0U RADKS -	-	48,	3,	999,	.26442-09\$
PUNCHED AND/OR BCD0U RADKS -	-	49,	4,	999,	.17657-09\$
PUNCHED AND/OR BCD0U RADKS -	-	50,	11,	999,	.76855-10\$
PUNCHED AND/OR BCD0U RADKS -	-	51,	12,	999,	.14541-09\$
PUNCHED AND/OR BCD0U RADKS -	-	52,	13,	999,	.26442-09\$
PUNCHED AND/OR BCD0U RADKS -	-	53,	14,	999,	.17657-09\$
PUNCHED AND/OR BCD0U RADKS -	-	54,	5,	999,	.70085-09\$
PUNCHED AND/OR BCD0U RADKS -	-	55,	15,	999,	.70085-09\$
PUNCHED AND/OR BCD0U RADKS -	-	56,	21,	999,	.31765-08\$
PUNCHED AND/OR BCD0U RADKS -	-	57,	22,	999,	.31765-08\$
PUNCHED AND/OR BCD0U RADKS -	-	58,	23,	999,	.16040-08\$
PUNCHED AND/OR BCD0U RADKS -	-	59,	24,	999,	.31765-08\$
PUNCHED AND/OR BCD0U RADKS -	-	60,	25,	999,	.16040-08\$
PUNCHED AND/OR BCD0U RADKS -	-	61,	26,	999,	.31765-08\$

DATE 062278 TIME 204148 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 32
 MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 1 - MLOT/SFCAL/FFCAL/OBCAL/RKCAL - ORIGINAL RUN
 RADIATION CONDUCTOR GENERATION LINK.

CONSERVATION CHECKS
 RADIATION SUMS FOR EACH NODE BEFORE RKHIN SCREENING

1 - .10000+01	2 - .10000+01	3 - .10000+01	4 - .10000+01	11 - .10000+01	12 - .10000+01
13 - .10000+01	14 - .10000+01	5 - .10000+01	15 - .10000+01	21 - .10000+01	22 - .10000+01
23 - .10000+01	24 - .10000+01	25 - .10000+01	26 - .10000+01		

DATE 062278 TIME 204149 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 33

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 1 - NPL0T/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE AFTER RKMIN SCREENING

1 - .10000+01	2 - .10000+01	3 - .10000+01	4 - .10000+01	11 - .10000+01	12 - .10000+01
13 - .10000+01	14 - .10000+01	5 - .10000+01	15 - .10000+01	21 - .10000+01	22 - .10000+01
23 - .10000+01	24 - .10000+01	25 - .10000+01	26 - .10000+01		

TOTAL TIME TO COMPUTE AND CONDENSE RADKS = .65

IT HAS BEEN A PLEASURE SERVING YOU. I HOPE YOU ENJOY YOUR 4. FRAMES OF S-C 4060 OUTPUT.

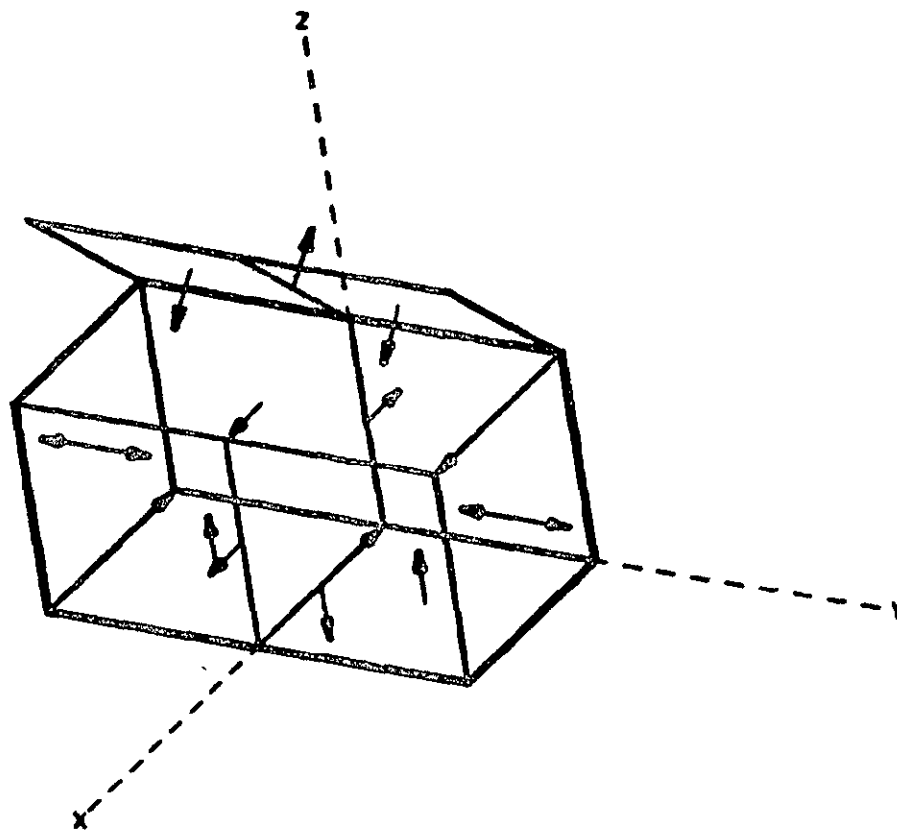
++NOTE++ TRASYS GENERATED 4 PLOT FRAMES

NORMAL TERMINATION BY PROCESSOR

OPHD,PLEB

BRKPT PRINTS

SAMPLE CASE 1 - WPLT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN



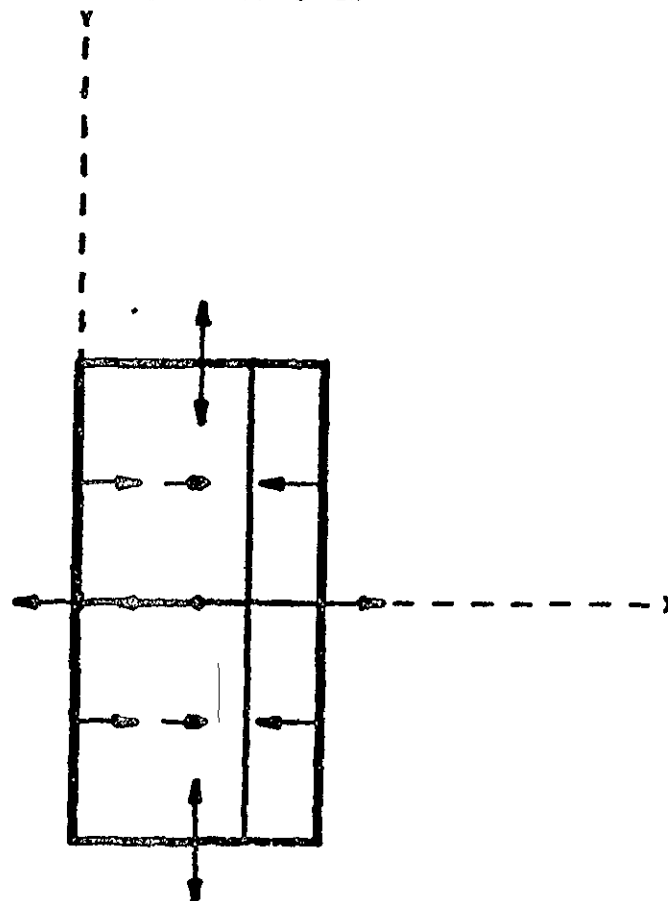
H-109

VIEW = 3-D

SCALE = 1.2261

+ VIEW NUMBER = 1

SAMPLE CASE 1 - HPLT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN



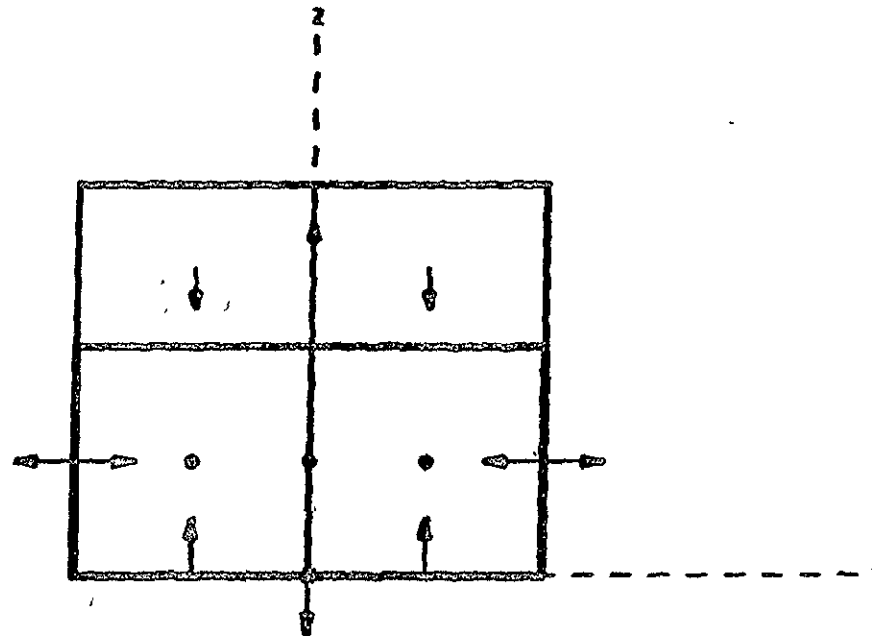
H-110

VIEW = Z-AXIS

SCALE = 1.2261

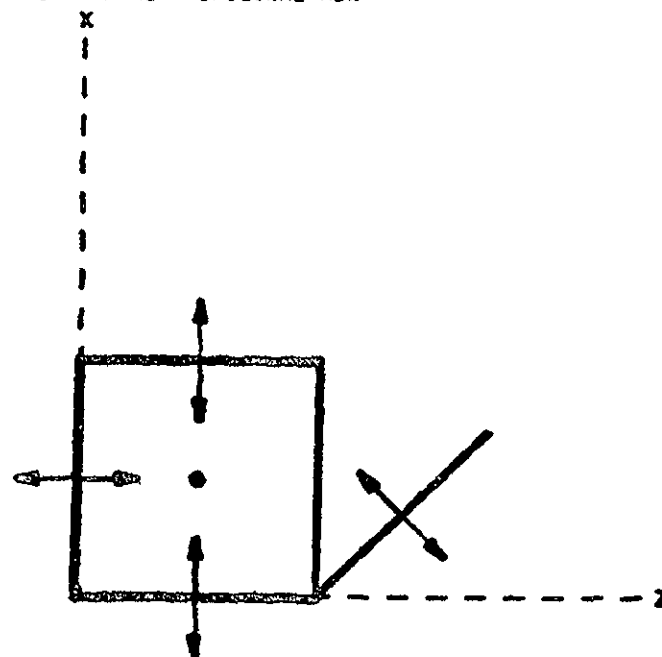
+ VIEW NUMBER = 1

SAMPLE CASE 1 - EPLT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN



H-111
 VIEW = X-AXIS
 SCALE = 1.2261
 * VIEW NUMBER = 1

SAMPLE CASE 1 - NPLOT/SFCAL/FFCAL/GBCAL/RKCAL - ORIGINAL RUN



H-112

VIEW = Y-AXIS

SCALE = 1.2261

+ VIEW NUMBER = 1

SAMPLE CASE 2

SAMPLE CASE 2

0ED,R VOGTB.CASE2
 FILE IN FIELD 1 DISABLED--ACCEPTED
 FILE IN FIELD 1 IN USE BY ANOTHER RUN
 READ-ONLY MODE
 CASE UPPER ASSUMED
 ED 14.02-06/27-00:50-10.)
 EDIT

1:0RUN,R/R RVMM02,3248-F261-C,ES3-N03711,07,300 NO DECK VOGT
 10:0ASG,T RSI,.0C,X04861
 11:0ADD ES3-TRASYS*TRASYS.STARTM
 12:0SETC 0100
 13:0ADD PREPRO
 14:HEADER OPTIONS DATA
 15:TITLE SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T
 16:C RESTARTING SFCAL/FFCAL/GBCAL FROM SAMPLE CASE 1
 17:C COMBINING NODES IN RCCAL
 18:C CALCULATING DIRECT INCIDENT FLUXES USING SHADOW
 19:C FACTOR TABLES FROM SAMPLE CASE 1.
 20:C
 21: MODEL = SAMPLE
 22: RSI = RSTSAM
 23: RSO = RSTSAM2
 24:HEADER EDIT DATA
 25:*0,127,171
 26:*0,195
 27:C-----BUILD THE CASE 1 CONFIGURATION FOR SFCAL/FFCAL/GBCAL RESTART
 28:*0,198,203
 29:*0,205
 30:C-----READ AND PRINT THE SHADOW FACTOR TABLES FROM RSI FOR USE IN
 31:*1,207
 32: SFRNT=YES
 33:*0,210
 34:C-----READ THE FORM FACTOR MATRIX FROM RSI
 35:*0,214
 36:C-----READ THE GRAY BODY MATRICES FROM RSI
 37:*0,219,221
 38:C-----CALCULATE AND PUNCH RADKS WITH COMBINED NODES
 39:C
 40: CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,5HCASE2)
 41:*1,222
 42:C
 43:C-----DEFINE ORBIT AND VEHICLE ORIENTATION (CIRCULAR - PLANET ORIENTED)
 44:C
 45: CALL ORBIT2(EAR,0,60.,0,0,0,100.*6080.,100.*6080.)
 46: CALL ORIENT(4HPLAN,1,2,3,300.,270.,0.)
 47:C
 48:ORBGEN CIRP,0.,180.,2,A0
 49:C
 50:C-----THE CONFIGURATION NAME IS REDEFINED SO THE QC'S WILL USE
 51:C-----THE DESIRED(CASE2) CORRESPONDENCE DATA.
 52:C
 53: MODELN=5HCASE2
 54: CALL Q0DATA(3HALL,0,0,0,0,0,0,0)
 55:L Q0CAL
 56:C
 57:C-----MAKE ORBIT PLOTS
 58:C

59: CALL ODATAS(1,0,0,0,0,0,0,0)
60: CALL ODATAS(2,0,0,0,0,90,0,0)
61: CALL ODATAS(3,0,0,0,0,180,0,0)
62:L OPL0T
63:0PMD,0LEP
64:0ASG,T/S RSO.,0C,RSO,02,RSO APPENDIX H, CASE 2.
65:0ADD PROCSS
73:0FIN

NO CORRECTIONS APPLIED.

0ASG,T RSI.,0C,X04861

0FREE TPF\$.

0ASG,T TPF\$..F4/0/TRK/400

NASA/MARTIN HARIETTA
THERMAL RADIATION ANALYSIS SYSTEM
UNIVAC 1110/EXEC 6

TTTTTTTTTTTT
TTTTTTTTTTTT
TT TTT TT
TTT
TTT
TTT
TTT
TTT
TTTTTT

RRRRRRRR
RRRRRRRR
RRR RRR
RRR RRR
RRRRRRRR
RRR RRR
RRR RRR
RRR RRR
RRR RRR

AAAAAA
AAAAAA
AAAAAA
AAA AAA
AAA AAA
AAAAAA
AAA AAA
AAA AAA
AAA AAA
AAAA AAAA

SSSSSSSS
SSSSSSSSSS
SSS SS
SSS
SSSSSSSS
SSS
SS SS
SSSSSSSSSS
SSSSSSSSSS

TRASYS 11

YYYY YYYY
YYY YYY
YYY YYY
YYY YYY
YYYYY
YYY
YYY
YYYYYY

SSSSSSSS
SSSSSSSSSS
SSS SS
SSS
SSSSSSSS
SSS
SS SS
SSSSSSSSSS
SSSSSSSSSS

PRE-PROCESSOR EXECUTION

VERSION/MODIFICATION ... UC2E3
MODIFICATION DATE 052678
DATE OF RUN 062778
TIME OF RUN 005219
JOB NUMBER RVHH02

DATE 062770 TIME 005224 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 0 VERSION PAGE 1

MODEL = N/A

OPTION AND TITLE DATA BLOCKS

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

INPUT	HEADER OPTIONS DATA	
INPUT	TITLE	SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOTT
INPUT	C	RESTARTING SFCAL/FFCAL/GBCAL FROM SAMPLE CASE 1
INPUT	C	COMBINING NODES IN RCCAL
INPUT	C	CALCULATING DIRECT INCIDENT FLUXES USING SHADOW
INPUT	C	FACTOR TABLES FROM SAMPLE CASE 1.
INPUT	C	
INPUT	MODEL	= SAMPLE
INPUT	RSI	= RSTSAM
INPUT	RSO	= RSTSAM2

MODEL = SAMPLE SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLLOT
TRASYS INFORMATION TO USER

* ATTENTION TRASYS USERS *

THIS SECTION OF THE TRASYS PRINTOUT WAS DEvised TO
INFORM THE TRASYS USERS OF THE STATUS OF THE TRASYS
PROGRAM WITHOUT HAVING TO PRINTOUT ALL THE STATUS
INFORMATION ON EVERY RUN. TO OBTAIN ADDITIONAL
INFORMATION ON HOW TO USE THIS SECTION OF THE TRASYS
PRINTOUT. PLACE A (INFO=INFO) IN THE OPTIONS DATA
BLOCK.

FOR TRASYS ASSISTANCE AND/OR POSSIBLE TRASYS PROGRAM
PROBLEMS, PLEASE CONTACT BOB VOGT AT JSC-2326.

NEHRL 08/29/77 DOCUMENTATION ADDITION

THE TRASYS -N- VERSION HAS BEEN UPDATED TO THE UC2E2
AND UL2E4 LEVEL.
SEE LATEST USERS MANUAL FOR INFORMATION ON USER-
CALLED SUBROUTINE ARGUMENT CHANGES AND NEW
CAPABILITIES.

END OF TRASYS INFORMATION FILE

DATE 062778 TIME 005226 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC B VERSION PAGE 3

MODEL = SAMPLE
MODEL HISTORY

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

MODEL NAME SAMPLE

MODEL TITLE SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

MOD LABEL	RUN JOB NUMBER	RUN DATA	RUN TIME	RSI TAPE	RSO TAPE	RTI TAPE	RTO TAPE	CMERO TAPE	EMERG TAPE	BCDOU TAPE	TRAJ TAPE	USER1 TAPE	USER2 TAPE
AA	RVMH01	062278	202625										RSTSAM
AB	RVMH02	062778	005225										RSTSAM RSTSAM

DATE 062776 TIME 005227

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION

PAGE 4

MODEL = SAMPLE
SOURCE DATA EDIT DIRECTIVES

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBOEN/OPL0T

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

****	HEADER EDIT DATA		
0	40,127,171		
0	HEADER FORM FACTOR DATA	OLD-	127 AA
0	C	OLD-	128 AA
0	C-----ENTER KNOWN ZERO FORM FACTORS AND EQUIVALENT FORM FACTORS FOR	OLD-	129 AA
0	C-----CASE1.	OLD-	130 AA
0	C	OLD-	131 AA
0	FIG CASE1	OLD-	132 AA
0	NODEA 1,2,3,4,11,12,13,14,5,15,21,22,23,24,25,26.END	OLD-	133 AA
0	BOTH 21,ZERO	OLD-	134 AA
0	22,ZERO	OLD-	135 AA
0	23,ZERO	OLD-	136 AA
0	24,ZERO	OLD-	137 AA
0	25,ZERO	OLD-	138 AA
0	26,ZERO	OLD-	139 AA
0	1,1,0.	OLD-	140 AA
0	11,12,1,2	OLD-	141 AA
0	11,13,1,3	OLD-	142 AA
0	11,14,1,4	OLD-	143 AA
0	11,15,1,5	OLD-	144 AA
0	1,11,0.	OLD-	145 AA
0	11,2,1,12	OLD-	146 AA
0	11,3,1,13	OLD-	147 AA
0	11,4,1,14	OLD-	148 AA
0	11,5,1,15	OLD-	149 AA
0	2,2,0.	OLD-	150 AA
0	2,3,1,2	OLD-	151 AA
0	2,4,1,4	OLD-	152 AA
0	12,13,2,3	OLD-	153 AA
0	12,14,2,4	OLD-	154 AA
0	12,15,2,5	OLD-	155 AA
0	12,3,2,13	OLD-	156 AA
0	12,4,2,14	OLD-	157 AA
0	12,5,2,15	OLD-	158 AA
0	3,3,0.	OLD-	159 AA
0	3,4,1,4	OLD-	160 AA
0	13,14,3,4	OLD-	161 AA
0	13,15,3,5	OLD-	162 AA
0	3,13,0.	OLD-	163 AA
0	13,4,3,14	OLD-	164 AA
0	13,5,3,15	OLD-	165 AA
0	4,4,0.	OLD-	166 AA
0	14,15,4,5	OLD-	167 AA
0	4,14,0.	OLD-	168 AA
0	14,5,4,15	OLD-	169 AA
0	5,5,0.	OLD-	170 AA
0	5,15,0.	OLD-	171 AA

CARD	ORIGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL
****	D			*D,195																
I				C-----BUILD THE CASE 1 CONFIGURATION														OLD-	195	AA
****	D			C-----BUILD THE CASE 1 CONFIGURATION FOR SFCAL/FFCAL/GBCAL RESTART														150		AB
I				*D,198,203																
D				C														OLD-	198	AA
D				C-----PLOT THE CASE 1 CONFIGURATION INDICATING THE ACTIVE														OLD-	199	AA
D				C-----SIDES OF THE NODES.														OLD-	200	AA
D				C														OLD-	201	AA
D				CALL NODATAS(0,0,0,YE5,0)														OLD-	202	AA
D				L NPL0T														OLD-	203	AA
****	D			*D,205																
I				C-----CALCULATE SHADOW FACTOR TABLES FOR SUBSEQUENT USE														OLD-	205	AA
****	D			C-----READ AND PRINT THE SHADOW FACTOR TABLES FROM RSI FOR USE IN														154		AB
I				*I,207																
I				SFPRNT=YES														157		AB
****	D			*D,210																
I				C-----CALCULATE THE FORM FACTOR MATRIX.														OLD-	210	AA
****	D			C-----READ THE FORM FACTOR MATRIX FROM RSI														160		AB
I				*D,214																
D				C-----CALCULATE THE GRAY BODY MATRIX.														OLD-	214	AA
I				C-----READ THE GRAY BODY MATRICES FROM RSI														164		AB
****	D			*D,219,221																
D				C-----CALCULATE AND PUNCH RADIATION CONDUCTORS.														OLD-	219	AA
D				C														OLD-	220	AA
I				CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,0)													OLD-	221	AA	
I				C-----CALCULATE AND PUNCH RADKS WITH COMBINED NODES														169		AB
I				C														170		AB
****	D			CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,5HCASE2)														171		AB
I				*I,222																
I				C														173		AB
I				C-----DEFINE ORBIT AND VEHICLE ORIENTATION (CIRCULAR - PLANET ORIENTED)														174		AB
I				C														175		AB
I				CALL ORBIT2(EAR,0.60,,0,0,0,100,*6080.,100.*6080.)														176		AB
I				CALL ORIENT(4HPLAN,1,2,3,300.,270.,0.)														177		AB
I				C														178		AB
I				ORBGEN CIRP,0.,180.,2.AQ														179		AB
I	</																			

DATE 062778 TIME 005244 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 5

MODEL = SAMPLE
SOURCE DATA EDIT DIRECTIVES SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

CARD	ORGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL
I																		191		AB
I																		192		AB
I	L																	193		AB

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

RSI	HEADER SURFACE DATA	1	OLD-	1	AA
RSI	C	2	OLD-	2	AA
RSI	C-----THIS SURFACE DATA BLOCK IS USED IN SAMPLE CASES 1 THROUGH 5	3	OLD-	3	AA
RSI	C-----WITH VARIOUS PORTIONS OF IT BEING ACTIVATED FOR THE DIFFERENT	4	OLD-	4	AA
RSI	C-----CASES.	5	OLD-	5	AA
RSI	C	6	OLD-	6	AA
RSI	BCS BOXINR	7	OLD-	7	AA
RSI	S SURFN = 1	8	OLD-	8	AA
RSI	TYPE = RECT	9	OLD-	9	AA
RSI	ACTIVE = BOTTOM	10	OLD-	10	AA
RSI	PROP = 0.9,0.9	11	OLD-	11	AA
RSI	P1 = 1.0, 0.0, 1.0	12	OLD-	12	AA
RSI	P2 = 1.0, 0.0, 0.0	13	OLD-	13	AA
RSI	P3 = 1.0, 1.0, 0.0	14	OLD-	14	AA
RSI	COM = * INNER RIGHT FRONT *	15	OLD-	15	AA
RSI	S SURFN = 2	16	OLD-	16	AA
RSI	TYPE = RECT	17	OLD-	17	AA
RSI	ACTIVE = BOTTOM	18	OLD-	18	AA
RSI	PROP = 0.9,0.9	19	OLD-	19	AA
RSI	P1 = 1.0, 1.0, 1.0	20	OLD-	20	AA
RSI	P2 = 1.0, 1.0, 0.0	21	OLD-	21	AA
RSI	P3 = 0.0, 1.0, 0.0	22	OLD-	22	AA
RSI	COM = * INNER RIGHT SIDE *	23	OLD-	23	AA
RSI	S SURFN = 3	24	OLD-	24	AA
RSI	TYPE = RECT	25	OLD-	25	AA
RSI	ACTIVE = TOP	26	OLD-	26	AA
RSI	PROP = 0.9,0.9	27	OLD-	27	AA
RSI	P1 = 0.0, 0.0, 1.0	28	OLD-	28	AA
RSI	P2 = 0.0, 0.0, 0.0	29	OLD-	29	AA
RSI	P3 = 0.0, 1.0, 0.0	30	OLD-	30	AA
RSI	COM = * INNER RIGHT BACK *	31	OLD-	31	AA
RSI	S SURFN = 4	32	OLD-	32	AA
RSI	TYPE = RECT	33	OLD-	33	AA
RSI	ACTIVE = TOP	34	OLD-	34	AA
RSI	PROP = 0.9,0.9	35	OLD-	35	AA
RSI	P1 = 1.0, 1.0, 0.0	36	OLD-	36	AA
RSI	COM = * INNER RIGHT BOTTOM *	37	OLD-	37	AA
RSI	BCS BOXINL.IMGBCS=BOXINR.NINC=10,IREFSF=1000	38	OLD-	38	AA
RSI	C	39	OLD-	39	AA
RSI	C-----THE FOREGOING CAPD IMAGES BCS BOXINR IN REFERENCE PLANE 1000	40	OLD-	40	AA
RSI	C-----TO CREATE BCS BOXINL. THE INTERIOR OF THE BOX WAS INPUT IN	41	OLD-	41	AA
RSI	C-----THIS MANNER TO FACILITATE THE INPUT OF SAMPLE CASE 4 TO SHOW	42	OLD-	42	AA
RSI	C-----THE USE OF 'MESS' AND 'ERN' NODES.	43	OLD-	43	AA
RSI	C	44	OLD-	44	AA

IMAGING SURFACE (1) BCS (BOXINR), GENERATING SURFACE (11) BCS (BOXINL)
IMAGING SURFACE (2) BCS (BOXINR), GENERATING SURFACE (12) BCS (BOXINL)
IMAGING SURFACE (3) BCS (BOXINR), GENERATING SURFACE (13) BCS (BOXINL)

DATE 062778 TIME 005248

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION

PAGE 8

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

		IMAGING SURFACE (4) BCS (BOXINR), GENERATING SURFACE (14) BCS (BOXINL)					
RSI	R	REFNO	= 1000	45	OLD-	45	AA
RSI		P1	= 1.0, 0.0, 1.0	46	OLD-	46	AA
RSI		P2	= 1.0, 0.0, 0.0	47	OLD-	47	AA
RSI		P3	= 0.0, 0.0, 0.0	48	OLD-	48	AA
RSI		COM	= * IMAGING PLANE *	49	OLD-	49	AA
RSI	BCS	LIDINR		50	OLD-	50	AA
RSI	S	SURFN	= 5	51	OLD-	51	AA
RSI		TYPE	= RECT	52	OLD-	52	AA
RSI		ACTIVE	= BOTTOM	53	OLD-	53	AA
RSI		PROP	= 0.9,0.9	54	OLD-	54	AA
RSI		P1	= 1.0, 1.0, 0.0	55	OLD-	55	AA
RSI		COM	= * INNER RIGHT LID *	56	OLD-	56	AA
RSI	S	SURFN	= 15	57	OLD-	57	AA
RSI		IMAGSF	= 5	58	OLD-	58	AA
RSI		IREFSF	= 1000	59	OLD-	59	AA
RSI		COM	= * INNER LEFT LID *	60	OLD-	60	AA
RSI	BCS	BOXOUT		61	OLD-	61	AA
RSI	S	SURFN	= 21	62	OLD-	62	AA
RSI		TYPE	= BOX5	63	OLD-	63	AA
RSI		ACTIVE	= OUT	64	OLD-	64	AA
RSI		SHADE	= NO	65	OLD-	65	AA
RSI		PROP	= 0.2,0.9	66	OLD-	66	AA
RSI		P1	= 1.01,-1.01, 1.01	67	OLD-	67	AA
RSI		P2	= 1.01, 1.01, 1.01	68	OLD-	68	AA
RSI		P3	= -0.01, 1.01, 1.01	69	OLD-	69	AA
RSI		P4	= -0.01, 1.01,-0.01	70	OLD-	70	AA
RSI		COM	= * OUTER SURFACES *	71	OLD-	71	AA
RSI	BCS	LIDOUT		72	OLD-	72	AA
RSI	S	SURFN	= 26	73	OLD-	73	AA
RSI		TYPE	= RECT	74	OLD-	74	AA
RSI		ACTIVE	= TOP	75	OLD-	75	AA
RSI		SHADE	= NO	76	OLD-	76	AA
RSI		PROP	= 0.2,0.9	77	OLD-	77	AA
RSI		P1	= 1.01,-1.01, 0.01	78	OLD-	78	AA
RSI		P2	= 1.01, 1.01, 0.01	79	OLD-	79	AA
RSI		P3	= -0.01, 1.01, 0.01	80	OLD-	80	AA
RSI		COM	= * OUTER SURFACE OF LID *	81	OLD-	81	AA
RSI	C			82	OLD-	82	AA
RSI	C	-----THE NEXT TWO BCS'S (HESSR AND HESSL) ARE ACTIVATED IN SAMPLE		83	OLD-	83	AA
RSI	C	-----CASE 4 ONLY.		84	OLD-	84	AA
RSI	C			85	OLD-	85	AA
RSI	BCS	HESSR		86	OLD-	86	AA
RSI	S	SURFN	= 101	87	OLD-	87	AA
RSI		TYPE	= RECT	88	OLD-	88	AA
RSI		ACTIVE	= TOP	89	OLD-	89	AA
RSI		PROP	= 1.0,1.0	90	OLD-	90	AA

DATE 062778 TIME 005253 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 9

MODEL = SAMPLE SURFACE DATA INPUT BLOCK SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPILOT

CARD	ORIGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL		
RSI			P1		=	1.0.	0.0.	1.0										91	OLD-	91	AA	
RSI			P2		=	1.0.	0.0.	0.0										92	OLD-	92	AA	
RSI			P3		=	0.0.	0.0.	0.0										93	OLD-	93	AA	
RSI			COM		=	* PRIMARY MESS NODE, RIGHT SIDE *													94	OLD-	94	AA
RSI	BCS		MESSL															95	OLD-	95	AA	
RSI	S		SURFN		=	111												96	OLD-	96	AA	
RSI			TYPE		=	RECT												97	OLD-	97	AA	
RSI			ACTIVE		=	BOTTOM												98	OLD-	98	AA	
RSI			PROP		=	1.0,1.0												99	OLD-	99	AA	
RSI			P1		=	1.0.	0.0.	1.0										100	OLD-	100	AA	
RSI			P2		=	1.0.	0.0.	0.0										101	OLD-	101	AA	
RSI			P3		=	0.0.	0.0.	0.0										102	OLD-	102	AA	
RSI			COM		=	* PRIMARY MESS NODE, LEFT SIDE *													103	OLD-	103	AA
RSI	C																	104	OLD-	104	AA	
RSI	C		C-----THE FOLLOWING BCS (LIDSP) IS ACTIVATED IN SAMPLE CASE 5 ONLY.																105	OLD-	105	AA
RSI	C																	106	OLD-	106	AA	
RSI	BCS		LIDSP															107	OLD-	107	AA	
RSI	S		SURFN		=	200												108	OLD-	108	AA	
RSI			TYPE		=	RECT												109	OLD-	109	AA	
RSI			ACTIVE		=	BOTTOM												110	OLD-	110	AA	
RSI			PROP		=	0.1,0.1												111	OLD-	111	AA	
RSI			SPRI		=	0.8												112	OLD-	112	AA	
RSI			SPRS		=	0.8												113	OLD-	113	AA	
RSI			P1		=	1.0,-1.0.	0.0											114	OLD-	114	AA	
RSI			P2		=	1.0.	1.0.	0.0										115	OLD-	115	AA	
RSI			P3		=	0.0.	1.0.	0.0										116	OLD-	116	AA	
RSI			COM		=	* SPECULAR LID *													117	OLD-	117	AA

DATE 062770 TIME 005303 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 10

MODEL = SAMPLE SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEM/OPIOT
BCS DATA INPUT BLOCK

CARD ORGIN	12345678 1	2345678 2	2345678 3	2345678 4	2345678 5	2345678 6	2345678 7	2345678 8	EDIT NO.	OLD EDIT NO.	LABEL	
RSI	HEADER BCS DATA								118	OLD-	118	AA
RSI	BCS BOXINR								119	OLD-	119	AA
RSI	BCS BOXINL								120	OLD-	120	AA
RSI	BCS LIDINR .0..0..1..0..-45..0.								121	OLD-	121	AA
RSI	BCS BOXOUT								122	OLD-	122	AA
RSI	BCS LIDOUT .0..0..1..0..-45..0.								123	OLD-	123	AA
RSI	BCS MESSR								124	OLD-	124	AA
RSI	BCS MESSL								125	OLD-	125	AA
RSI	BCS LIDSP .0..0..1..0..-45..0.								126	OLD-	126	AA

DATE 062770 TIME 005306 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC B VERSION PAGE 11

MODEL = SAMPLE CORRESPONDENCE DATA INPUT BLOCK SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

CARD	ORGIN	12345678 1	2345678 2	2345678 3	2345678 4	2345678 5	2345678 6	2345678 7	2345678 8	EDIT NO.	OLD EDIT NO.	LABEL	
RS1	HEADER CORRESPONDENCE DATA									127	OLD-	172	AA
RS1	C									128	OLD-	173	AA
RS1	C-----ENTER CORRESPONDENCE DATA FOR CASE 2									129	OLD-	174	AA
RS1	C									130	OLD-	175	AA
RS1	F10 CASE2									131	OLD-	176	AA
RS1	1	=	1,11,22							132	OLD-	177	AA
RS1	2	=	2,25							133	OLD-	178	AA
RS1	3	=	3,13,24							134	OLD-	179	AA
RS1	4	=	4,14,21							135	OLD-	180	AA
RS1	5	=	5,15,26							136	OLD-	181	AA
RS1	12	=	12,23							137	OLD-	182	AA
RS1	C									138	OLD-	183	AA
RS1	C-----ENTER CORRESPONDENCE DATA FOR CASE 3 TO COMBINE FORM FACTORS									139	OLD-	184	AA
RS1	C									140	OLD-	185	AA
RS1	F10 CASE3,FF									141	OLD-	186	AA
RS1	1	=	1,11,22							142	OLD-	187	AA
RS1	2	=	2,25							143	OLD-	188	AA
RS1	3	=	3,13,24							144	OLD-	189	AA
RS1	4	=	4,14,21							145	OLD-	190	AA
RS1	5	=	5,15,26							146	OLD-	191	AA
RS1	12	=	12,23							147	OLD-	192	AA

DATE 062778 TIME 005307 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 12

MODEL = SAMPLE
OPERATION DATA INPUT BLOCK (PASS 1) SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPILOT

CARD ORIGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL	
RSI	HEADER OPERATIONS DATA																148	OLD-	193	AA

+++++ OPERATIONS DATA BLOCK (PASS 1) COMPLETE +++++

MODEL = SAMPLE
OPERATION DATA INPUT BLOCK (PASS 2) SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

CARD ORGIN	12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8	EDIT NO.	OLD EDIT NO.	LABEL
RSI	C	149	OLD-	194 AA
INPUT	C-----BUILD THE CASE 1 CONFIGURATION FOR SFCAL/FFCAL/GBCAL RESTART	150		AB
RSI	C	151	OLD-	196 AA
PROG	STEP -1	0		
RSI	BUILD CASE1,BOXINR,BOXINL,LIDINR,BOXOUT,LIDOUT	152	OLD-	197 AA
PROG	CALL BUILD0 (BOXINR,6HCASE1)	0		
PROG	CALL ADD (BOXINL)	0		
PROG	CALL ADD (LIDINR)	0		
PROG	CALL ADD (BOXOUT)	0		
PROG	CALL ADD (LIDOUT)	0		
RSI	C	153	OLD-	204 AA
INPUT	C-----READ AND PRINT THE SHADOW FACTOR TABLES FROM RSI FOR USE IN	154		AB
RSI	C-----SAMPLE CASE 2 IN THE CALCULATION OF DIRECT FLUXES.	155	OLD-	206 AA
RSI	C	156	OLD-	207 AA
INPUT	SFPRNT=YES	157		AB
RSI	L SFCAL	158	OLD-	208 AA
RSI	C	159	OLD-	209 AA
INPUT	C-----READ THE FORM FACTOR MATRIX FROM RSI	160		AB
RSI	C	161	OLD-	211 AA
RSI	L FFCAL	162	OLD-	212 AA
RSI	C	163	OLD-	213 AA
INPUT	C-----READ THE GRAY BODY MATRICES FROM RSI	164		AB
RSI	C	165	OLD-	215 AA
RSI	CALL GBDATA(BOTH,0,FF)	166	OLD-	216 AA
RSI	L GBCAL	167	OLD-	217 AA
RSI	C	168	OLD-	218 AA
INPUT	C-----CALCULATE AND PUNCH RADKS WITH COMBINED NODES	169		AB
INPUT	C	170		AB
INPUT	CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,5HCASE2)	171		AB
RSI	L RCCAL	172	OLD-	222 AA
INPUT	C	173		AB
INPUT	C-----DEFINE ORBIT AND VEHICLE ORIENTATION (CIRCULAR - PLANET ORIENTED)	174		AB
INPUT	C	175		AB
INPUT	CALL ORBIT2(EAR,0,60.,0,0,0,100.*6080.,100.*6080.)	176		AB
INPUT	CALL ORIENT(4HPLAN,1,2,3,300.,270.,0.)	177		AB
INPUT	C	178		AB
PROG	C	0		
PROG	C***** ORBIT GENERATION STARTS HERE *****	0		
INPUT	COR0GEN CIRP,0.,180.,2,AQ	179		AB
PROG	C	0		
PROG	STEP 10000	0		
PROG	TRUEAN = .000	0		
PROG	TRUANG = 180.000	0		
PROG	TRUANI = .000	0		
PROG	IAI = 0	0		
PROG	IAS = 0	0		
PROG	PLTYPE = 6HPLSAVE	0		
PROG	CALL D1COMP(0,0,0)	0		
PROG	L DICAL	0		

PROG	NSPFF	= 10000			0
PROG	PLTYPE	= 6HPLREAD			0
PROG	CALL AQDATA(1A1,1AS,0,0,0)				0
PROG	L	AQCAL			0
PROG	STEP 10001				0
PROG	TRUEAN	= 90.000			0
PROG	CALL DICOMP(0,0,10000)				0
PROG	L	DICAL			0
PROG	CALL AQDATA(1A1,1AS,0,0,0)				0
PROG	L	AQCAL			0
PROG	STEP 10002				0
PROG	TRUEAN	= 180.000			0
PROG	CALL DICOMP(0,0,10000)				0
PROG	L	DICAL			0
PROG	CALL AQDATA(1A1,1AS,0,0,0)				0
PROG	L	AQCAL			0
PROG	STEP 10003				0
PROG	IF(SHADIN.LT.0.)	GO TO 90400			0
PROG	TRUEAN	= SHADIN-0.1			0
PROG	IF(TRUEAN.LT.TRUANI.OR.				0
PROG	1 TRUEAN.GT.TRUANF)	GO TO 90000			0
PROG	CALL DICOMP(0,4HZERO,10000)				0
PROG	L	DICAL			0
PROG	CALL AQDATA(1A1,1AS,0,0,0)				0
PROG	L	AQCAL			0
PROG	90000 CONTINUE				0
PROG	STEP 10004				0
PROG	TRUEAN	= SHADIN+0.1			0
PROG	IF(TRUEAN.LT.TRUANI.OR.				0
PROG	1 TRUEAN.GT.TRUANF)	GO TO 90100			0
PROG	CALL DICOMP(0,0,10000)				0
PROG	L	DICAL			0
PROG	CALL AQDATA(1A1,1AS,0,0,0)				0
PROG	L	AQCAL			0
PROG	90100 CONTINUE				0
PROG	STEP 10005				0
PROG	TRUEAN	= SHAOUT+0.1			0
PROG	IF(TRUEAN.LT.TRUANI.OR.				0
PROG	1 TRUEAN.GT.TRUANF)	GO TO 90200			0
PROG	CALL DICOMP(0,4HZERO,10000)				0
PROG	L	DICAL			0
PROG	CALL AQDATA(1A1,1AS,0,0,0)				0
PROG	L	AQCAL			0
PROG	90200 CONTINUE				0
PROG	STEP 10006				0
PROG	TRUEAN	= SHAOUT-0.1			0
PROG	IF(TRUEAN.LT.TRUANI.OR.				0
PROG	1 TRUEAN.GT.TRUANF)	GO TO 90300			0
PROG	CALL DICOMP(0,0,10000)				0
PROG	L	DICAL			0
PROG	CALL AQDATA(1A1,1AS,0,0,0)				0
PROG	L	AQCAL			0
PROG	90300 CONTINUE				0
PROG	90400 CONTINUE				0
PROG	CALL QODATA(3HALL,0,0,0,0,0,0,0)				0
PROG	L	QOCAL			0
PROG.	C				0

PROG	C***** ORBIT GENERATION ENDS HERE *****	0	
PROG	C	0	
INPUT	C	180	AB
INPUT	C-----THE CONFIGURATION NAME IS REDEFINED SO THE QO'S WILL USE	181	AB
INPUT	C-----THE DESIRED(CASE2) CORRESPONDENCE DATA.	182	AB
INPUT	C	183	AB
INPUT	MODELN=5HCASE2	184	AB
INPUT	CALL QODATA(3HALL,0.0,0.0,0.0,0)	185	AB
INPUT	L QOCAL	186	AB
INPUT	C	187	AB
INPUT	C-----MAKE ORBIT PLOTS	188	AB
INPUT	C	189	AB
INPUT	CALL ODATAS(1,0.0,0.0,0.0,0)	190	AB
INPUT	CALL ODATAS(2,0.0,0.0,0.90,0.0)	191	AB
INPUT	CALL ODATAS(3,0.0,0.0,0.180,0.0)	192	AB
INPUT	L OPLOT	193	AB
RS1	END OF DATA	194	AA

DATE 062778 TIME 005316 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC B VERSION PAGE 14

MODEL = SAMPLE
PROCESSOR CORE ALLOCATION

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

THE FOLLOWING IS THE PROCESSOR CORE ALLOCATION FOR THOSE SEGMENTS WHICH WILL BE LOADED IN THIS EXECUTION (APPROX.) ...

OCTAL/DECIMAL

TRASYS (0) SEGMENT	121213/	41611	
OPERATIONS DATA (NOT KNOWN AT THIS TIME).....	175000/	64000	
INITIALIZATION SEGMENT	122300/	42176	
FORM FACTOR SEGMENT	136100/	48192	
SHADOW FACTOR SEGMENT	136000/	48128	
ORBITAL PLOTTER SEGMENT	125700/	43968	
DIRECT FLUX SEGMENT	150500/	53568	
GRAY BODY SEGMENT	124000/	43008	
ABSORBED Q-S SEGMENT	122500/	42304	
-QO- SEGMENT	130600/	45440	
RADATION CONDUCTOR SEGMENT	125500/	43840	
GRAY BODY DYNAMIC COMMON	000276/	190	
-QO- DYNAMIC COMMON	003554/	1900	
RADATION CONDUCTOR DYNAMIC COMMON	000574/	380	
GRAY BODY MINIMUM - MAXIMUM CORE	123566/	42870	- 123716/ 42958
-QO- MINIMUM - MAXIMUM CORE	125142/	43618	- 130552/ 45418
RADATION CONDUCTOR MINIMUM - MAXIMUM CORE	125221/	43665	- 125465/ 43829
MINIMUM CORE NEEDED FOR PROCESSOR EXECUTION	150500/	53568	
MAXIMUM CORE NEEDED FOR PROCESSOR EXECUTION	150500/	53568	
AMOUNT OF CORE THAT WILL BE USED BY PROCESSOR .	150500/	53568	

MODEL = SAMPLE SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT
 WRAP UP OF THE PRE-PROCESSOR

PRE-PROCESSOR ACCOUNTING INFORMATION	CP-SEC	DYM-STORAGE
SOURCE EDITING	2.251	676
DOCUMENTATION DATA PRE-PROCESSING000	0
QUANTITIES DATA PRE-PROCESSING039	266
ARRAY DATA PRE-PROCESSING000	0
SURFACE DATA PRE-PROCESSING (PASS 1) ...	2.009	64
SURFACE DATA PRE-PROCESSING (PASS 2)743	1141
BCS DATA PRE-PROCESSING269	106
FORM FACTOR DATA PRE-PROCESSING000	0
SHADOW DATA PRE-PROCESSING000	0
FLUX DATA PRE-PROCESSING000	0
CORRESPONDENCE DATA PRE-PROCESSING243	101
OPERATIONS DATA PRE-PROCESSING	4.114	879
SUBROUTINE DATA PRE-PROCESSING312	0
SEQUENTIAL TAPE INITIALIZATION027	0

TOTAL CP TIME FOR PRE-PROCESSOR 10.739 DECIMAL SECONDS OR 000013 OCTAL SECONDS

MINIMUM DYNAMIC STORAGE NEEDED BY PRE-PROCESSOR .. 1141 DECIMAL WORDS

DYNAMIC STORAGE AVAILABLE TO PRE-PROCESSOR 10000 DECIMAL WORDS

NORMAL TERMINATION BY PRE-PROCESSOR

@PHD,BLEP

@ASG,T/S R50,.8C,R50,92,R50 APPENDIX H, CASE 2.

@TEST TNE/1/53

@JUMP L3
 - INTERVENING STATEMENTS SKIPPED

@L3:FREE DATA1.

@FREE 14

NASA/MARTIN MARIETTA
THERMAL RADIATION ANALYSIS SYSTEM
UNIVAC 1110/EXEC 8

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TTTTTTTTTTTT
TTTTTTTTTTTT
TT  TTT  TT
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TTTTTT

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RRRRRRRRR
RRRRRRRRR
RRR  RRR
RRR  RRR
RRRRRRRRR
RRR  RRR
RRR  RRR
RRR  RRR
RRR  RRR

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AAAAAAA
AAAAAAAAA
AAAAAAAAA
AAA  AAA
AAA  AAA
AAAAAAAAA
AAA  AAA
AAA  AAA
AAA  AAA
AAAAA  AAAA

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SSSSSSSSSS
SSSSSSSSSS
SSS  SS
SSS
SSSSSSSSSS
      SSS
SS      SS
SSSSSSSSSS
SSSSSSSSSS

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YYYY  YYYY
YYY  YYY
YYY  YYY
YYY  YYY
YYYYY
YYY
YYY
YYYYYYY

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SSSSSSSSSS
SSSSSSSSSS
SSS  SS
SSS
SSSSSSSSSS
      SSS
SS      SS
SSSSSSSSSS
SSSSSSSSSS

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PROCESSOR EXECUTION

```

VERSION.MODIFICATION ... UL2E6
MODIFICATION DATE ..... 061978

DATE OF RUN ..... 062778
TIME OF RUN ..... 010030
JOB NUMBER ..... RVMH02

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DATE 062778 TIME 010034

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE

1

MODEL=SAMPLE CONFIG=CASE1 STEP=-1

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

PROCESSING OPERATIONS DATA

SEQUENCE	NODE	BCS	AREA	ALPH	EMISS	SURF. TYPE	ACTIVE	-----COMMENTS-----
1	1	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
2	2	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
3	3	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
4	4	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
5	11	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
6	12	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
7	13	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
8	14	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
9	5	LIDINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT LID
10	15	LIDINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER LEFT LID
11	21	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
12	22	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
13	23	BOXOUT	1.04040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
14	24	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
15	25	BOXOUT	1.04040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
16	26	LIDOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACE OF LID

NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE
 BY -BUILD- (ACCESS NUMBER = 1)

PAGE 2

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

DATE 062770 TIME 010109 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 3

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

		CLOCK ANGLE																			
NODE	2	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																				CONE	
SHADOW TABLE																				ANGLE	
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.61	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.06	.17	.33	.44	.56	.58	.61	22.5
		.42	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.42	.64	.61	.58	.42	45.0
		.19	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.61	.42	.25	.22	.19	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE	2	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																				CONE	
SHADOW TABLE																				ANGLE	
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.61	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.06	.17	.33	.44	.56	.58	.61	22.5
		.42	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.42	.64	.61	.58	.42	45.0
		.19	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.61	.42	.25	.22	.19	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062778 TIME 010111

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC. 8 VERSION

PAGE 4

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

		CLOCK ANGLE																		CONE ANGLE
NODE	3	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
SOLAR SHADOW TABLE																				
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.06	.08	.03	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.81	.53	.31	.17	.00	.00	.00	.00	.00	.00	.00	.00	.03	.33	.83	1.00	1.00	45.0
		.33	.42	.31	.25	.08	.00	.00	.00	.00	.00	.00	.00	.00	.25	.72	.50	.50	.33	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																		CONE ANGLE
NODE	3	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
INFRA RED SHADOW TABLE																				
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.06	.08	.03	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.81	.53	.31	.17	.00	.00	.00	.00	.00	.00	.00	.00	.03	.33	.83	1.00	1.00	45.0
		.33	.42	.31	.25	.08	.00	.00	.00	.00	.00	.00	.00	.00	.25	.72	.50	.50	.33	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

		CLOCK ANGLE																				
NODE	%	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
SOLAR SHADOW TABLE																					CONE ANGLE	
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0	
		.67	.56	.36	.39	.39	.28	.11	.00	.00	.00	.00	.00	.00	.17	.33	.50	.50	.67	.67	22.5	
		.00	.00	.06	.08	.00	.00	.06	.00	.00	.00	.00	.00	.00	.03	.28	.64	.50	.17	.00	45.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

		CLOCK ANGLE																			
NODE	4	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED SHADOW TABLE																					CONE ANGLE
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.67	.56	.36	.39	.39	.28	.11	.00	.00	.00	.00	.00	.00	.17	.33	.50	.50	.67	.67	22.5
		.00	.00	.06	.08	.00	.00	.06	.00	.00	.00	.00	.00	.00	.03	.28	.64	.50	.17	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062770 TIME 010115 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 6

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SHADOW FACTOR GENERATOR LINK SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

		CLOCK ANGLE																			
NODE	11	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW TABLE																					ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		.00	.00	.00	.00	.00	1.00	.67	.17	.00	.00	.11	.33	.64	.91	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	1.00	.03	.00	.00	.00	.06	.19	.42	.59	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.61	.17	.00	.00	.00	.08	.17	.25	.19	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE	11	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW TABLE																					ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		.00	.00	.00	.00	.00	1.00	.67	.17	.00	.00	.11	.33	.64	.91	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	1.00	.03	.00	.00	.00	.06	.19	.42	.59	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.61	.17	.00	.00	.00	.08	.17	.25	.19	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPILOT

		CLOCK ANGLE																			CONE ANGLE
NODE	12	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR SHADOW TABLE																					
	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
	.61	.58	.56	.44	.33	.17	.06	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.61	22.5
	.42	.58	.61	.64	.42	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.42	45.0
	.19	.22	.25	.42	.61	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.19	67.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			CONE ANGLE
NODE	12	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED SHADOW TABLE																					
	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
	.61	.58	.56	.44	.33	.17	.06	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.61	22.5
	.42	.58	.61	.64	.42	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.42	45.0
	.19	.22	.25	.42	.61	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.19	67.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062779 TIME 010110

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 8

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

		CLOCK ANGLE																			
NODE	13	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.03	.08	.06	.00	22.5
	1.00	1.00	.83	.33	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.31	.53	.81	1.00	45.0
		.33	.50	.50	.72	.25	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.25	.31	.42	.33	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE	13	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.03	.08	.06	.00	22.5
	1.00	1.00	.83	.33	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.31	.53	.81	1.00	45.0
		.33	.50	.50	.72	.25	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.25	.31	.42	.33	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062770 TIME 010119

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 9

MODEL=SAMPLE CONFIG=CASE1 STEP=-1

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLT

SHADOW FACTOR GENERATOR LINK

CLOCK ANGLE

NODE 14 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

SOLAR
SHADOW TABLECONE
ANGLE

.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
.67	.67	.50	.50	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.28	.39	.39	.36	.56	.67	22.5
.00	.00	.17	.50	.64	.28	.03	.00	.00	.00	.00	.00	.00	.06	.00	.00	.08	.06	.00	.00	45.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

CLOCK ANGLE

NODE 14 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

INFRA RED
SHADOW TABLECONE
ANGLE

.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
.67	.67	.50	.50	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.28	.39	.39	.36	.56	.67	22.5
.00	.00	.17	.50	.64	.28	.03	.00	.00	.00	.00	.00	.00	.06	.00	.00	.08	.06	.00	.00	45.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

		CLOCK ANGLE																				CONE ANGLE
NODE	5	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
SOLAR SHADOW TABLE																						
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5	
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0	
		1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5	
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0	
		.67	.56	.67	.67	.72	.72	.00	.00	.00	.00	.00	.00	.00	.14	.14	.33	.50	.50	.67	112.5	
		.33	.39	.33	.31	.33	.33	.31	.22	.11	.00	.00	.00	.00	.00	.00	.00	.17	.33	.33	135.0	
		.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

		CLOCK ANGLE																				CONE ANGLE
NODE	5	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
INFRA RED SHADOW TABLE																						
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5	
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0	
		1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5	
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0	
		.67	.56	.67	.67	.72	.72	.00	.00	.00	.00	.00	.00	.00	.14	.14	.33	.50	.50	.67	112.5	
		.33	.39	.33	.31	.33	.33	.31	.22	.11	.00	.00	.00	.00	.00	.00	.00	.17	.33	.33	135.0	
		.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

[illegible][illegible]

DATE 062778 TIME 010124 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 12

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

		CLOCK ANGLE																			
NODE	21	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

		CLOCK ANGLE																			
NODE	21	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

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SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

	CLOCK ANGLE																			
NODE	22	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.

**CONE
ANGLE**

[illegible]

SEVER ANGLES

NODE	22	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
------	----	----	-----	-----	-----	-----	------	------	------	------	------	------	------	------	------	------	------	------	------	------

**CONE
ANGLE**

[illegible]

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

	CLOCK ANGLE																			
NODE	23	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.

SOLAR SHADOW TABLE

**CONE
ANGLE**

[illegible]

	CLOCK ANGLE																			
NODE	23	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.

INFRARED
SHADOW TABLE

**CONE
ANGLE**

[illegible]

DATE 062778 TIME 010128

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

SHADOW FACTOR GENERATOR LINK

CLOCK ANGLE

NODE	24	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
------	----	----	-----	-----	-----	-----	------	------	------	------	------	------	------	------	------	------	------	------	------	------

SOLAR
SHADOW TABLECONE
ANGLE

1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	22.5
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	45.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	157.5
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

CLOCK ANGLE

NODE	24	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
------	----	----	-----	-----	-----	-----	------	------	------	------	------	------	------	------	------	------	------	------	------	------

INFRA RED
SHADOW TABLECONE
ANGLE

1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	22.5
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	45.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	157.5
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

[illegible][illegible]

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

CLOCK ANGLE

MODE 26 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

SOLAR
SHADOW TABLE

CONE
ANGLE

1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	22.5
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	45.0
.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

CLOCK ANGLE

MODE 26 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

INFRA RED
SHADOW TABLE

CONE
ANGLE

1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	22.5
1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	45.0
.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	67.5
.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	90.0
.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	112.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

SHADOW FACTORS FOR CONFIGURATION CASE1 HAVE BEEN STORED ON R50.
LAST RECORD WRITTEN = 52

TOTAL TIME FOR SHADOW FACTOR TABLES 9.6

DATE 062770 TIME 010133 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 18

MODEL=SAHLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPIOT
FORM FACTOR CALCULATION LINK.

FORM FACTORS AND COMBINED FORM FACTORS - USER INPUT AND DEFAULT PARAMETERS

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
FFACC	.0500	.0500	ORIENTATION ACCURACY PARAMETER	N/A
FFACCS	.1000	.1000	SHADOWING ACCURACY PARAMETER	N/A
FFMIN	.1-05	1.0E-06	PARAMETER TO ELIMINATE SMALL FORM FACTORS	N/A
FFNOSH	SHAD	SHAD	OVER RIDE SHADOWING PARAMETER	(SHAD,NOSH)
+FFPNCH	NO	NO	PARAMETER TO PUNCH FORM FACTORS	(YES,NO)
FFPRNT	YES	YES	FLAG FOR COMPREHENSIVE FF AND CM PRINT	(YES,NO,FF,CM,RB)
FFRATL	15.0	15.0	RATIO FOR USING SUB-NODE TECHNIQUE	N/A
FFCMB	NO	CORR	FLAG FOR COMBINING FORM FACTORS	(YES,NO,AUTO,CORR)

+ -FFPNCH WILL DEFAULT TO -YES- ON CALCULATED VALUES IF THE -RSO- FILE IS NOT SPECIFIED IN THE OPTIONS DATA BLOCK

RESTARTING - FFCAL - DATA FOR CONFIGURATION- CASE1 -FROM UNIT - 14

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

SEQUENCE	NODE	AREA	ALPH	EMISS
1	1	1.00000	.900	.900
2	2	1.00000	.900	.900
3	3	1.00000	.900	.900
4	4	1.00000	.900	.900
5	11	1.00000	.900	.900
6	12	1.00000	.900	.900
7	13	1.00000	.900	.900
8	14	1.00000	.900	.900
9	5	1.00000	.900	.900
10	15	1.00000	.900	.900
11	21	2.06040	.200	.900
12	22	2.06040	.200	.900
13	23	1.04040	.200	.900
14	24	2.06040	.200	.900
15	25	1.04040	.200	.900
16	26	2.06040	.200	.900

NUMBER OF NODES = 16 NUMBER OF SURFACES = 16

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W0/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ	
1	2	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
1	3	RSI	.201522	.201522	.201522	.201522	.201522	1.000000	1.000000	.000	0	0	UN
1	4	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
1	12	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
1	13	RSI	.086058	.086058	.086058	.086058	.086058	1.000000	1.000000	.000	0	0	UN
1	14	RSI	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	.000	0	0	UN
1	5	RSI	.137203	.137203	.137203	.137203	.137203	1.000000	1.000000	.000	0	0	UN
1	15	RSI	.056006	.056006	.056006	.056006	.056006	1.000000	1.000000	.000	0	0	UN
1	FFSUM = .9690 ROW CP TIME = .143												
1	FORM FACTOR RESTART (RS0) RECORD = 56												
2	3	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN

DATE 062778 TIME 010136

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ	
2	4	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
2	11	RSI	.032922	.032922	.032922	.032922	.032922	.000000	.000000	.000	0	0	UN
2	12	RSI	.068832	.068832	.068832	.068832	.068832	1.000000	1.000000	.000	0	0	UN
2	13	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
2	14	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
2	5	RSI	.096343	.096343	.096343	.096343	.096343	1.000000	1.000000	.000	0	0	UN
2	15	RSI	.034262	.034262	.034262	.034262	.034262	1.000000	1.000000	.000	0	0	UN
2	FFSUM = .9203		ROW CP TIME = .153										
	FORM FACTOR RESTART		(RSI) RECORD = 57										
3	4	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
3	11	RSI	.086058	.086058	.086058	.086058	.086058	.000000	.000000	.000	0	0	UN
3	12	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
3	14	RSI	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	.000	0	0	UN
3	5	RSI	.050426	.050426	.050426	.050426	.050426	1.000000	1.000000	.000	0	0	UN
3	15	RSI	.011660	.011660	.011660	.011660	.011660	1.000000	1.000000	.000	0	0	UN
3	FFSUM = .8378		ROW CP TIME = .081										
	FORM FACTOR RESTART		(RSI) RECORD = 58										
4	11	RSI	.040501	.040501	.040501	.040501	.040501	.000000	.000000	.000	0	0	UN
4	12	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
4	13	RSI	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	.000	0	0	UN
4	5	RSI	.107798	.107798	.107798	.107798	.107798	1.000000	1.000000	.000	0	0	UN
4	15	RSI	.056851	.056851	.056851	.056851	.056851	1.000000	1.000000	.000	0	0	UN
4	FFSUM = .9007		ROW CP TIME = .069										
	FORM FACTOR RESTART		(RSI) RECORD = 59										
11	12	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
11	13	RSI	.201522	.201522	.201522	.201522	.201522	1.000000	1.000000	.000	0	0	UN

DATE 062770 TIME 010130 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 21

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT
FORM FACTOR CALCULATION LINK.

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) H/SHAD	FIR(J,I) H/SHAD	FSOL(I,J) H/SHAD	FSOL(J,I) H/SHAD	FF(I,J) H/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ	
11	14	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
11	5	RSI	.056006	.056006	.056006	.056006	.056006	1.000000	1.000000	.000	0	0	UN
11	15	RSI	.137203	.137203	.137203	.137203	.137203	1.000000	1.000000	.000	0	0	UN
11	FFSUM = .9690 ROW CP TIME = .126 FORM FACTOR RESTART (RSO) RECORD = 60												
12	13	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
12	14	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
12	5	RSI	.034262	.034262	.034262	.034262	.034262	1.000000	1.000000	.000	0	0	UN
12	15	RSI	.096343	.096343	.096343	.096343	.096343	1.000000	1.000000	.000	0	0	UN
12	FFSUM = .9203 ROW CP TIME = .060 FORM FACTOR RESTART (RSO) RECORD = 61												
13	14	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
13	5	RSI	.011660	.011660	.011660	.011660	.011660	1.000000	1.000000	.000	0	0	UN
13	15	RSI	.050426	.050426	.050426	.050426	.050426	1.000000	1.000000	.000	0	0	UN
13	FFSUM = .8378 ROW CP TIME = .048 FORM FACTOR RESTART (RSO) RECORD = 62												
14	5	RSI	.056851	.056851	.056851	.056851	.056851	1.000000	1.000000	.000	0	0	UN
14	15	RSI	.107798	.107798	.107798	.107798	.107798	1.000000	1.000000	.000	0	0	UN
14	FFSUM = .9007 ROW CP TIME = .028 FORM FACTOR RESTART (RSO) RECORD = 63												

DATE 062770 TIME 010139

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 22

MODEL=SAMPLE CONFID=CASE1 STEP=1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) H/SHAD	FIR(J,I) H/SHAD	FSOL(I,J) H/SHAD	FSOL(J,I) H/SHAD	FF(I,J) NO/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
5		FFSUM = .5505 FORM FACTOR RESTART (RSO) RECORD =										
15		FFSUM = .5505 FORM FACTOR RESTART (RSO) RECORD =										
21		FFSUM = .0000 FORM FACTOR RESTART (RSO) RECORD =										
22		FFSUM = .0000 FORM FACTOR RESTART (RSO) RECORD =										
23		FFSUM = .0000 FORM FACTOR RESTART (RSO) RECORD =										
24		FFSUM = .0000 FORM FACTOR RESTART (RSO) RECORD =										

DATE 062778 TIME 010141 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 23

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGGEN/OPLLOT
FORM FACTOR CALCULATION LINK.

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUES OF RSI, RTI, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
25		FFSUM = .0000										
		FORM FACTOR RESTART (RSO) RECORD =										
26		FFSUM = .0000										
		FORM FACTOR RESTART (RSO) RECORD =										

FF FORM FACTORS FOR CONFIGURATION CASE1 HAVE BEEN STORED ON RSO.
LAST RESTART RECORD WRITTEN = 71

DATE 062778 TIME 010141 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 24

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

SUMMARY OF FORM FACTOR SUMS FOR ALL NODES

NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM
1- .9690	2- .9203	3- .8378	4- .9007	11- .9690	12- .9203
13- .8378	14- .9007	5- .5505	15- .5505	21- .0000	22- .0000
23- .0000	24- .0000	25- .0000	26- .0000		
TOTAL TIME FOR FORM FACTOR SEGMENT		1.557			
TOTAL TIME SINCE START OF RUN		91.175			

DATE 062778 TIME 010142 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION PAGE 25

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T
GRAY BODIES COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	GREY BODIES DEFINITION	OPTIONS
GBWBND	BOTH	BOTH	HAVEBAND DEFINITION PARAMETER	(2H1R,3HSOL,4HBOTH)

RESTARTING - GB1R - DATA FOR CONFIGURATION- CASE1 -FROM UNIT - 14

RESTARTING - GB50 - DATA FOR CONFIGURATION- CASE1 -FROM UNIT - 14

IR GRAY BODIES STORED FOR CONFIG. CASE1 LAST RESTART RECORD WRITTEN = 89

SOL GRAY BODIES STORED FOR CONFIG. CASE1 LAST RESTART RECORD WRITTEN = 107

TOTAL TIME TO COMPUTE GRAY BODIES .73

DATE 062778 TIME 010149

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 26

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

VARIABLE NAME	CURRENT VALUE	DEFAULT	RADIATION CONDUCTORS DEFINITION	OPTIONS
RKPNCH	PUN	NO	PUNCH/NO PUNCH PARAMETER FOR RADKS	(YES,NO)
RKMIN	.0001	0.0001	PARAMETER TO ELIMINATE SMALL RADK S	N/A
IRKCN	1	1	INITIAL RADIATION CONDUCTOR ID NUMBER	N/A
RKSP	SPACE	NO	MNEMONIC FLAG FOR COMPUTATION OF RADKS TO SPACE	(SPACE,NO)
IRKNSP	999	32767	SPACE NODE ID NUMBER	N/A
SIGMA	.17-08	1.713E-9	STEFAN-BOLTZMANN CONSTANT	N/A
RKAMPF	1.00	1.0	AREA MULTIPLYING FACTOR	N/A
RKTAPE	NO	NO	PARAMETER TO OUTPUT TO BCD TAPE	(TAPE,NO)
RFRAC	.7+00	0.7	SIGNIFICANT RADIATION FRACTION	(0. TO 1.)
RTOL	.990	0.99	DECIMAL FRACTION OF LAST RADK SAVED	N/A
NERN	0	0	EFFECTIVE RADIATION NODE (ERN) NUMBER	N/A

DATE 062778 TIME 010151

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

SPECIAL RADIATION NODES

NONE

MESS SPECIAL NODES

PRIMARY SECONDARY

NONE

DATE 062770 TIME 010151

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

RADIATION CONDUCTOR (RADKS) CARDS

AREA UNITS = INPUT UNITS * AMPF, WHERE AMPF = 1.00000

PUNCHED AND/OR BCD0U RADKS -	-	1.	1.	2.	.35937-09\$
PUNCHED AND/OR BCD0U RADKS -	-	2.	1.	3.	.83913-09\$
PUNCHED AND/OR BCD0U RADKS -	-	3.	1.	4.	.73699-09\$
PUNCHED AND/OR BCD0U RADKS -	-	4.	1.	12.	.35937-09\$
PUNCHED AND/OR BCD0U RADKS -	-	5.	1.	5.	.56426-09\$
PUNCHED AND/OR BCD0U RADKS -	-	6.	2.	3.	.35685-09\$
PUNCHED AND/OR BCD0U RADKS -	-	7.	2.	4.	.35743-09\$
PUNCHED AND/OR BCD0U RADKS -	-	8.	2.	12.	.10306-09\$
PUNCHED AND/OR BCD0U RADKS -	-	9.	2.	5.	.19789-09\$
PUNCHED AND/OR BCD0U RADKS -	-	10.	3.	4.	.73080-09\$
PUNCHED AND/OR BCD0U RADKS -	-	11.	3.	12.	.35685-09\$
PUNCHED AND/OR BCD0U RADKS -	-	12.	3.	5.	.21024-09\$
PUNCHED AND/OR BCD0U RADKS -	-	13.	4.	12.	.35743-09\$
PUNCHED AND/OR BCD0U RADKS -	-	14.	4.	5.	.48604-09\$
PUNCHED AND/OR BCD0U RADKS -	-	15.	12.	5.	.19789-09\$
PUNCHED AND/OR BCD0U RADKS -	-	16.	1.	999.	.33302-08\$
PUNCHED AND/OR BCD0U RADKS -	-	17.	2.	999.	.17494-08\$
PUNCHED AND/OR BCD0U RADKS -	-	18.	3.	999.	.37054-08\$
PUNCHED AND/OR BCD0U RADKS -	-	19.	4.	999.	.35297-08\$
PUNCHED AND/OR BCD0U RADKS -	-	20.	12.	999.	.17494-08\$
PUNCHED AND/OR BCD0U RADKS -	-	21.	5.	999.	.45782-08\$

DATE 062778 TIME 010152 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 29

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK. SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOTT

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE BEFORE RKMIN SCREENING

1 - .10000+01 2 - .10000+01 3 - .10000+01 4 - .10000+01 12 - .10000+01 5 - .10000+01

DATE 062770 TIME 010152 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 30

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOTT
RADIATION CONDUCTOR GENERATION LINK.

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE AFTER RKMIN SCREENING

1 - .10000+01 2 - .10000+01 3 - .10000+01 4 - .10000+01 12 - .10000+01 5 - .10000+01

TOTAL TIME TO COMPUTE AND CONDENSE RADKS = .81

MODEL=SAMPLE CONFIG=CASE1 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
0	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX,IROTY,IROTZ		1 2 3	
.300+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.300+02	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCH POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062770 TIME 010155 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 32

MODEL=SAMPLE CONFIG=CASE1 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

+++++ NSTEP NO = 10000

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	HDS
.20900+09	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	HSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAY CONSTANT	GRAY		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062778 TIME 010156 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 33

MODEL=SAMPLE CONFIG=CASE1 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

++NOTE++ AN EOF HAS BEEN ENCOUNTERED ON RSI. LAST RECORD NO. READ = 107

++NOTE++ INITIATING CALCULATIONS

-DICAL - RESTART DATA FOR CONFIGURATION -CASE1 - NOT FOUND ON UNIT-RSI-. INITIATING CALCULATIONS.

DATE 062778 TIME 010159 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 34

MODEL=SAMPLE CONFIG=CASE1 STEP=10000 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT
DIRECT IRRADIATION CALCULATION LINK.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10000 TRUE ANOMALY = .00000 TIME = .00000
++++ IN THE SUN +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	SFTAPE	.001	9	0
2	.94028+02	.18576+03	.5062	CALC	.190	81	5
3	.00000	.10725+03	.0000	CALC	.307	64	9
4	.18576+03	.37152+03	.5000	SFTAPE	.372	81	0
11	.00000	.00000	.0000	SFTAPE	.420	9	0
12	.00000	.00000	.0000	SFTAPE	.469	9	0
13	.10055+02	.10725+03	.0938	CALC	.591	64	6
14	.10664+03	.37152+03	.2870	SFTAPE	.653	81	0
5	.00000	.00000	.0000	SFTAPE	.699	9	0
15	.00000	.00000	.0000	SFTAPE	.747	9	0
21	.00000	.00000	.0000	SFTAPE	.796	8	0
22	.10725+03	.10725+03	1.0000	CALC	.984	66	10
23	.18576+03	.18576+03	1.0000	CALC	1.158	81	8
24	.00000	.00000	.0000	SFTAPE	1.206	8	0
25	.00000	.00000	.0000	SFTAPE	1.255	9	0
26	.18687+03	.18687+03	1.0000	CALC	1.469	78	10

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RTI, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 94.820 SECONDS

MODEL=SAMPLE CONFIG=CASE1 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10000 TRUE ANOMALY = .00000 TIME = .00000
++++ IN THE SUN +++++

NODE NUMBER	COMPUT	---DIRECT INCID. ALBEDO	FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS--- ALBEDO PLAN	CP TIME (SECONDS)	---ELEMENTS--- PLAN SURF	SHAD SURF
1	SFTAPE	.000	.000	.391+02	.268+02	.000 .000	.001	66 9	9
2	SFTAPE	.000	.000	.400+02	.264+02	.000 .000	.309	66 9	9
3	SFTAPE	.000	.000	.402+02	.268+02	.000 .000	.556	61 9	9
4	SFTAPE	.000	.000	.000	.000	.000 .000	.670	52 9	9
11	SFTAPE	.000	.000	.391+02	.268+02	.000 .000	.935	66 9	9
12	SFTAPE	.000	.000	.382+02	.264+02	.000 .000	1.210	66 9	9
13	SFTAPE	.000	.000	.402+02	.268+02	.000 .000	1.463	61 9	9
14	SFTAPE	.000	.000	.000	.000	.000 .000	1.578	52 9	9
5	CALC	.231+02	.155+02	.834+02	.559+02	.277 .277	2.776	133 16	9
15	CALC	.233+02	.154+02	.834+02	.559+02	.279 .277	3.844	133 16	9
21	CALC	.110+03	.742+02	.110+03	.742+02	1.000 1.000	8.413	112 18	10
22	CALC	.402+02	.268+02	.402+02	.268+02	1.000 1.000	9.362	61 10	10
23	CALC	.400+02	.264+02	.400+02	.264+02	1.000 1.000	10.135	66 9	10
24	CALC	.391+02	.268+02	.391+02	.268+02	1.000 1.000	11.105	66 10	10
25	CALC	.382+02	.264+02	.382+02	.264+02	1.000 1.000	11.854	66 9	10
26	CALC	.659+01	.457+01	.659+01	.457+01	1.000 1.000	12.189	52 2	10

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 107.302 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 120

DATE 062779 TIME 010230 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 36

MODEL=SAMPLE CONFIG=CASE1 STEP=10000
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10000	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10000	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10000	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10000

TOTAL TIME TO COMPUTE ABSORBED Q .26

MODEL=SAMPLE CONFIG=CASE1 STEP=10001
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
90.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX, IROTY, IROTZ		1 2 3	
.000	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.900+02	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCH POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062778 TIME 010235 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 38

MODEL=SAMPLE CONFIG=CASE1 STEP=10001
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

+++++ NSTEP NO = 10001

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	WSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062778 TIME 010237 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 39

MODEL=SAMPLE CONFIG=CASE1 STEP=10001 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLLOT
DIRECT IRRADIATION CALCULATION LINK.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10001 TRUE ANOMALY = 90.00000 TIME = .36701
++++ IN THE SUN +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	SFTAPE	.001	9	0
2	.00000	.00000	.0000	SFTAPE	.101	9	0
3	.00000	.42900+03	.0000	SFTAPE	.157	81	0
4	.00000	.00000	.0000	SFTAPE	.211	9	0
11	.00000	.00000	.0000	SFTAPE	.263	9	0
12	.00000	.00000	.0000	SFTAPE	.313	9	0
13	.00000	.42900+03	.0000	SFTAPE	.368	81	0
14	.00000	.00000	.0000	SFTAPE	.418	9	0
5	.30335+03	.30335+03	1.0000	SFTAPE	.482	81	0
15	.30335+03	.30335+03	1.0000	SFTAPE	.546	81	0
21	.00000	.00000	.0000	SFTAPE	.594	8	0
22	.42900+03	.42900+03	1.0000	SFTAPE	.659	78	0
23	.00000	.00000	.0000	SFTAPE	.704	9	0
24	.00000	.00000	.0000	SFTAPE	.750	8	0
25	.00000	.00000	.0000	SFTAPE	.800	9	0
26	.00000	.00000	.0000	SFTAPE	.854	8	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 109.145 SECONDS

DATE 062778 TIME 010240 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION PAGE 40

MODEL=SAMPLE CONFIG=CASE1 STEP=10001
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORDGEN/OPL0T

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10001 TRUE ANOMALY = 90.00000 TIME = .36701
++++ IN THE SUN +++++

NODE NUMBER	COMPUT	---DIRECT ALBEDO	INCID. FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	--SHADOW FACTORS-- ALBEDO	PLAN	CP TIME (SECONDS)	--ELEMENTS-- PLAN	SURF	SHAD SURF
1	SFTAPE	.000	.000	.000	.000	.000	.000	.001	68	9	9
2	SFTAPE	.000	.000	.638+00	.000	.000	.000	.292	66	9	9
3	SFTAPE	.000	.000	.206+01	.000	.000	.000	.541	61	9	9
4	SFTAPE	.000	.000	.000	.000	.000	.000	.647	52	9	9
11	SFTAPE	.000	.000	.000	.000	.000	.000	.893	66	9	9
12	SFTAPE	.000	.000	.634+00	.000	.000	.000	1.138	66	9	9
13	SFTAPE	.000	.000	.206+01	.000	.000	.000	1.369	61	9	9
14	SFTAPE	.000	.000	.000	.000	.000	.000	1.475	52	9	9
5	CALC	.126+01	.155+02	.247+01	.000	.509	.000	2.652	133	16	9
15	CALC	.125+01	.154+02	.247+01	.000	.504	.000	3.706	133	16	9
21	CALC	.143+01	.742+02	.143+01	.000	1.000	.000	6.716	112	10	10
22	CALC	.206+01	.268+02	.206+01	.000	1.000	.000	7.326	61	10	10
23	CALC	.638+00	.264+02	.638+00	.000	1.000	.000	7.819	66	9	10
24	CALC	.000	.268+02	.000	.000	.000	.000	8.444	66	10	10
25	CALC	.634+00	.264+02	.634+00	.000	1.000	.000	8.895	66	9	10
26	CALC	.000	.457+01	.000	.000	.000	.000	9.109	52	2	10

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 118.517 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 139

DATE 062770 TIME 010305 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 41

MODEL=SAMPLE CONFIG=CASE1 STEP=10001
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10001	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10001	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10001	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10001

TOTAL TIME TO COMPUTE ABSORBED Q .21

MODEL=SAMPLE CONFIG=CASE1 STEP=10002 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORDEN/OPLOT
DIRECT IRRADIATION CALCULATION LINK.

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
----------------	-------------	-----------------	------------------	------------------

++++ BASIC CONTROL PARAMETERS +++++

SHAD	SHADOWING OVERRIDE FLAG	SHAD.NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
180.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST

++++ BASIC ORBIT DATA +++++

.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC

++++ PLANET-ORIENTED. ORIENTATION DATA +++++

300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX, IROTY, IROTZ		1 2 3	
.300+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.150+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.100+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO

++++ SPIN DATA +++++

.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE - CCM POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062778 TIME 010309 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 43

MODEL=SAMPLE CONFIG=CASE1 STEP=10002
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORDGEN/OFLOT

+++++ NSTEP NO = 10002

++++ COMPUTED OR INPUT ORBIT DATA ++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA ++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	WSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 082778 TIME 010310 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 44

MODEL=SAMPLE CONFIG=CASE1 STEP=10002
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBAL/RCCAL/ORBGEN/OPLOT

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10002 TRUE ANOMALY = 180.00000 TIME = .73402
++++ IN THE SHADE +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	+++++	.001	0	0
2	.00000	.00000	.0000	+++++	.046	0	0
3	.00000	.00000	.0000	+++++	.065	0	0
4	.00000	.00000	.0000	+++++	.085	0	0
11	.00000	.00000	.0000	+++++	.106	0	0
12	.00000	.00000	.0000	+++++	.126	0	0
13	.00000	.00000	.0000	+++++	.147	0	0
14	.00000	.00000	.0000	+++++	.171	0	0
5	.00000	.00000	.0000	+++++	.189	0	0
15	.00000	.00000	.0000	+++++	.211	0	0
21	.00000	.00000	.0000	+++++	.232	0	0
22	.00000	.00000	.0000	+++++	.256	0	0
23	.00000	.00000	.0000	+++++	.277	0	0
24	.00000	.00000	.0000	+++++	.302	0	0
25	.00000	.00000	.0000	+++++	.324	0	0
26	.00000	.00000	.0000	+++++	.345	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RTI, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICON

TOTAL ELAPSED TIME IN PROBLEM = 119.611 SECONDS

DATE 062778 TIME 010311 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 45

MODEL=SAFPLE CONFIO=CASE1 STEP=10002
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10002 TRUE ANOMALY = 180.00000 TIME = .73402
++++ IN THE SHADE +++++

NODE NUMBER	COMPUT	---DIRECT INCID. ALBEDO	FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	--SHADOW FACTORS-- ALBEDO PLAN	CP TIME (SECONDS)	--ELEMENTS-- PLAN SURF	SHAD SURF
1	+++++	.000	.000	.000	.000	.000 .000	.001	0 0	0
2	+++++	.000	.000	.000	.000	.000 .000	.049	0 0	0
3	+++++	.000	.000	.000	.000	.000 .000	.071	0 0	0
4	+++++	.000	.000	.000	.000	.000 .000	.091	0 0	0
11	+++++	.000	.000	.000	.000	.000 .000	.112	0 0	0
12	+++++	.000	.000	.000	.000	.000 .000	.132	0 0	0
13	+++++	.000	.000	.000	.000	.000 .000	.156	0 0	0
14	+++++	.000	.000	.000	.000	.000 .000	.175	0 0	0
5	+++++	.000	.155+02	.000	.000	.000 .000	.195	0 0	0
15	+++++	.000	.154+02	.000	.000	.000 .000	.217	0 0	0
21	+++++	.000	.742+02	.000	.000	.000 .000	.237	0 0	0
22	+++++	.000	.268+02	.000	.000	.000 .000	.259	0 0	0
23	+++++	.000	.264+02	.000	.000	.000 .000	.277	0 0	0
24	+++++	.000	.268+02	.000	.000	.000 .000	.303	0 0	0
25	+++++	.000	.264+02	.000	.000	.000 .000	.328	0 0	0
26	+++++	.000	.457+01	.000	.000	.000 .000	.347	0 0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RTI, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 119.991 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 158

DATE 062778 TIME 010315 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 46

MODEL=SAMPLE CONFIG=CASE1 STEP=10002
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10002	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10002	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10002	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10002

TOTAL TIME TO COMPUTE ABSORBED Q .23

DATE 062778 TIME 010318

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 47

MODEL=SAMPLE CONFIG=CASE1 STEP=10003

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOTT

DIRECT IRRADIATION CALCULATION LINK.

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS ++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
105.720	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA ++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA ++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX, IROTY, IROTZ		1 2 3	
.359+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.104+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA ++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCM=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCM POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062770 TIME 010319 - THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 48

MODEL=SAMPLE CONFIG=CASE1 STEP=10003
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLLOT

+++++ NSTEP NO = 10003

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGNA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGNAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	WSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062778 TIME 010320 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 49

MODEL=SAMPLE CONFIG=CASE1 STEP=10003 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLLOT
DIRECT IRRADIATION CALCULATION LINK.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10003 TRUE ANOMALY = 105.71977 TIME = .43111
++++ IN THE SUN +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	SFTAPE	.000	9	0
2	.00000	.69478+01	.0000	SFTAPE	.059	9	0
3	.00000	.41697+03	.0000	SFTAPE	.092	81	0
4	.00000	.00000	.0000	SFTAPE	.127	9	0
11	.00000	.00000	.0000	SFTAPE	.155	9	0
12	.00000	.00000	.0000	SFTAPE	.186	9	0
13	.00000	.41697+03	.0000	SFTAPE	.220	81	0
14	.00000	.00000	.0000	SFTAPE	.250	9	0
5	.28468+03	.36602+03	.7778	CALC	.346	81	5
15	.28468+03	.36602+03	.7778	CALC	.445	81	5
21	.10066+03	.10066+03	1.0000	CALC	.558	55	10
22	.41696+03	.41696+03	1.0000	CALC	.683	78	10
23	.69478+01	.69478+01	1.0000	CALC	.721	9	5
24	.00000	.00000	.0000	SFTAPE	.759	8	0
25	.00000	.00000	.0000	SFTAPE	.793	9	0
26	.00000	.00000	.0000	SFTAPE	.827	8	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 121.615 SECONDS

DATE 062778 TIME 010323 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 50

MODEL=SAMPLE CONFIG=CASE1 STEP=10003 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T
DIRECT IRRADIATION CALCULATION LINK.

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10003 TRUE ANOMALY = 105.71977 TIME = .43111
++++ IN THE SUN +++++

NODE NUMBER	COMPUT	---DIRECT INCID. FLUX-- ALBEDO	PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS-- ALBEDO	PLAN	CP TIME (SECONDS)	---ELEMENTS-- PLAN	SURF	SHAD SURF
1	+++++	.000	.000	.000	.000	.000	.000	.000	0	0	0
2	+++++	.000	.000	.000	.000	.000	.000	.054	0	0	0
3	+++++	.000	.000	.000	.000	.000	.000	.073	0	0	0
4	+++++	.000	.000	.000	.000	.000	.000	.096	0	0	0
11	+++++	.000	.000	.000	.000	.000	.000	.110	0	0	0
12	+++++	.000	.000	.000	.000	.000	.000	.139	0	0	0
13	+++++	.000	.000	.000	.000	.000	.000	.165	0	0	0
14	+++++	.000	.000	.000	.000	.000	.000	.185	0	0	0
5	+++++	.000	.155+02	.000	.000	.000	.000	.206	0	0	0
15	+++++	.000	.154+02	.000	.000	.000	.000	.232	0	0	0
21	+++++	.000	.742+02	.000	.000	.000	.000	.257	0	0	0
22	+++++	.000	.268+02	.000	.000	.000	.000	.278	0	0	0
23	+++++	.000	.264+02	.000	.000	.000	.000	.299	0	0	0
24	+++++	.000	.263+02	.000	.000	.000	.000	.320	0	0	0
25	+++++	.000	.264+02	.000	.000	.000	.000	.340	0	0	0
26	+++++	.000	.457+01	.000	.000	.000	.000	.363	0	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 122.011 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO R50 TAPE, LAST RESTART RECORD WRITTEN = 177

DATE 062778 TIME 010327 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 51

MODEL=SAMPLE CONFIG=CASE1 STEP=10003
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10003	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10003	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10003	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10003

TOTAL TIME TO COMPUTE ABSORBED Q .17

DATE 062778 TIME 010329

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=10004
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOTT

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
105.920	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX,IROTY,IROTZ		1 2 3	
.359+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.104+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCW=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCW POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

MODEL=SAMPLE CONFIG=CASE1 STEP=10004
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

+++++ NSTEP NO = 10004

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	HDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	HSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062778 TIME 010331 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 54

MODEL=SAMPLE CONFIG=CASE1 STEP=10004 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEM/OPLOT
DIRECT IRRADIATION CALCULATION LINK.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10004 TRUE ANOMALY = 105.91977 TIME = .43193
++++ IN THE SHADE +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	+++++	.000	0	0
2	.00000	.00000	.0000	+++++	.049	0	0
3	.00000	.00000	.0000	+++++	.071	0	0
4	.00000	.00000	.0000	+++++	.091	0	0
11	.00000	.00000	.0000	+++++	.110	0	0
12	.00000	.00000	.0000	+++++	.130	0	0
13	.00000	.00000	.0000	+++++	.149	0	0
14	.00000	.00000	.0000	+++++	.176	0	0
5	.00000	.00000	.0000	+++++	.197	0	0
15	.00000	.00000	.0000	+++++	.217	0	0
21	.00000	.00000	.0000	+++++	.230	0	0
22	.00000	.00000	.0000	+++++	.258	0	0
23	.00000	.00000	.0000	+++++	.275	0	0
24	.00000	.00000	.0000	+++++	.296	0	0
25	.00000	.00000	.0000	+++++	.319	0	0
26	.00000	.00000	.0000	+++++	.343	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 123.070 SECONDS

MODEL=SAHPLE CONFIG=CASE1 STEP=10004
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10004 TRUE ANOMALY = 105.91977 TIME = .43193
++++ IN THE SHADE +++++

NODE NUMBER	COMPUT	---DIRECT ALBEDO	INCID. FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS-- ALBEDO PLAN	CP TIME (SECONDS)	---ELEMENTS-- PLAN SURF	SHAD SURF
1	++++++	.000	.000	.000	.000	.000 .000	.001	0 0	0
2	++++++	.000	.000	.000	.000	.000 .000	.048	0 0	0
3	++++++	.000	.000	.000	.000	.000 .000	.069	0 0	0
4	++++++	.000	.000	.000	.000	.000 .000	.094	0 0	0
11	++++++	.000	.000	.000	.000	.000 .000	.116	0 0	0
12	++++++	.000	.000	.000	.000	.000 .000	.141	0 0	0
13	++++++	.000	.000	.000	.000	.000 .000	.162	0 0	0
14	++++++	.000	.000	.000	.000	.000 .000	.182	0 0	0
5	++++++	.000	.155+02	.000	.000	.000 .000	.199	0 0	0
15	++++++	.000	.154+02	.000	.000	.000 .000	.223	0 0	0
21	++++++	.000	.742+02	.000	.000	.000 .000	.244	0 0	0
22	++++++	.000	.268+02	.000	.000	.000 .000	.286	0 0	0
23	++++++	.000	.264+02	.000	.000	.000 .000	.286	0 0	0
24	++++++	.000	.268+02	.000	.000	.000 .000	.306	0 0	0
25	++++++	.000	.264+02	.000	.000	.000 .000	.326	0 0	0
26	++++++	.000	.457+01	.000	.000	.000 .000	.349	0 0	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 123.457 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 196

DATE 062778 TIME 010336 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 56

MODEL=SAMPLE CONFIG=CASE1 STEP=10004
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOTT

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10004	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10004	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10004	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10004

TOTAL TIME TO COMPUTE ABSORBED Q .26

DATE 062770 TIME 010340 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 57

MODEL=SAMPLE CONFIG=CASE1 STEP=10006
 ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
IQOTME	1	1	TIME ARRAY 10 NUMBER FLUX TABLES START AT IQOTME + 1	N/A
QOTAPE	NO	2HNO	PARAMETER TO OUTPUT TO BCD TAPE	(4HTAPE,2HNO)
QOPNCH	NO	2HNO	PUNCH/NO PUNCH PARAMETER FOR OUTPUT	(3HPUN,2HNO)
QOAMPF	1.0000	1.0	AREA MULTIPLYING FACTOR	N/A
QOFMPF	1.0000	1.0	FLUX MULTIPLYING FACTOR	N/A
QOTMPF	1.0000	1.0	TIME MULTIPLYING FACTOR	N/A
QOTYPE	BOTH	NONE	PARAMETER TO DETERMINE TYPE OF OUTPUT	(3HTAB,2HAV,4HBOTH)
IQOARY	ALL	NONE	STEP NO. ARRAY DIRECTIVE	(3HALL,ARRAY NAME)

DATE 062779 TIME 010342

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=10006
 ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT

ABSORBED HEAT RATE TABLES PUNCHED

Q = INPUT * RMPF WHERE RMPF = .10000+01
 TIME = INPUT * TMPF WHERE TMPF = .10000+01
 AREA IS ON SUBROUTINE CALL CARDS

1\$ TIME ARRAY	.000	.367+00.	.431+00.	.432+00.	.734+00
END\$					
2\$ HEAT RATE ARRAY	.675+01.	.586+01.	.549+01.	.283+00.	.283+00
END\$					
3\$ HEAT RATE ARRAY	.893+02.	.411+01.	.385+01.	.199+00.	.199+00
END\$					
4\$ HEAT RATE ARRAY	.619+01.	.218+01.	.205+01.	.105+00.	.105+00
END\$					
5\$ HEAT RATE ARRAY	.170+03.	.505+01.	.473+01.	.244+00.	.244+00
END\$					
6\$ HEAT RATE ARRAY	.412+01.	.586+01.	.549+01.	.283+00.	.283+00
END\$					
7\$ HEAT RATE ARRAY	.407+01.	.411+01.	.385+01.	.198+00.	.198+00
END\$					
8\$ HEAT RATE ARRAY	.125+02.	.218+01.	.205+01.	.105+00.	.105+00
END\$					
9\$ HEAT RATE ARRAY	.974+02.	.505+01.	.473+01.	.244+00.	.244+00
END\$					
10\$ HEAT RATE ARRAY	.381+02.	.288+03.	.270+03.	.139+02.	.139+02
END\$					
11\$ HEAT RATE ARRAY	.374+02.	.288+03.	.270+03.	.139+02.	.139+02
END\$					
12\$ HEAT RATE ARRAY	.183+03.	.138+03.	.179+03.	.138+03.	.138+03
END\$					
13\$ HEAT RATE ARRAY	.111+03.	.227+03.	.222+03.	.497+02.	.497+02
END\$					

MODEL=SAMPLE CONFIG=CASE1 STEP=10006 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLLOT
 ABSORBED Q OUTPUT COMPUTATION LINK.

ABSORBED HEAT RATE TABLES PUNCHED

Q = INPUT * RMPF WHERE RMPF = .10000+01
 TIME = INPUT * TMPF WHERE TMPF = .10000+01
 AREA IS ON SUBROUTINE CALL CARDS

14\$ HEAT RATE ARRAY
 .717+02, .249+02, .262+02, .247+02, .247+02
 ENDS
 15\$ HEAT RATE ARRAY
 .658+02, .497+02, .497+02, .497+02, .497+02
 ENDS
 16\$ HEAT RATE ARRAY
 .327+02, .249+02, .247+02, .247+02, .247+02
 ENDS
 17\$ HEAT RATE ARRAY
 .882+02, .847+01, .847+01, .847+01, .847+01
 ENDS

DATE 062776 TIME 010343

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 60

MODEL=SAMPLE CONFIG=CASE1 STEP=10008
ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/DRBGEN/DPLOT

DA11MC SUBROUTINE CALL CARDS

```
AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000+01
DA11MC(1.46792175E 0,TIMEN,A1 ,A2 ,1.00000000E 0,Q1 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A3 ,1.00000000E 0,Q2 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A4 ,1.00000000E 0,Q3 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A5 ,1.00000000E 0,Q4 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A6 ,1.00000000E 0,Q11 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A7 ,1.00000000E 0,Q12 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A8 ,1.00000000E 0,Q13 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A9 ,1.00000000E 0,Q14 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A10 ,1.00000000E 0,Q5 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A11 ,1.00000000E 0,Q15 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A12 ,1.00000000E 0,Q21 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A13 ,1.00000000E 0,Q22 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A14 ,1.00000000E 0,Q23 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A15 ,1.00000000E 0,Q24 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A16 ,1.00000000E 0,Q25 )$
DA11MC(1.46792175E 0,TIMEN,A1 ,A17 ,1.00000000E 0,Q26 )$
```


DATE 062778 TIME 010343 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 61

MODEL=SAMPLE CONFIG=CASE1 STEP=10006 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOTT
ABSORBED Q OUTPUT COMPUTATION LINK.

AVERAGE ORBITAL HEATING RATE AND AREA CARDS PUNCHED

VALUES ARE RATE = INPUT (UNITS) * RMPF WHERE RMPF = .10000+01
VALUES ARE AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000+01

Q1	=3.76739010E	0
Q2	=2.37882507E	1
Q3	=2.32315344E	0
Q4	=4.42941165E	1
Q11	=3.10908234E	0
Q12	=2.47663051E	0
Q13	=3.90220493E	0
Q14	=2.61343932E	1
Q5	=1.11914322E	2
Q15	=1.11704981E	2
Q21	=1.51001154E	2
Q22	=1.24700665E	2
Q23	=3.65944815E	1
Q24	=5.37007308E	1
Q25	=2.67737952E	1
Q26	=2.84040403E	1

TOTAL TIME TO COMPUTE ABSORBED Q OUT .59

DATE 062770 TIME 010343 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 62

MODEL=SAMPLE CONFIG=CASE2 STEP=10006 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORNGEN/OPLOT
 ABSORBED Q OUTPUT COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
IQOTNE	1	1	TIME ARRAY ID NUMBER FLUX TABLES START AT IQOTNE + 1	N/A
QOTAPE	NO	2HNO	PARAMETER TO OUTPUT TO BCD TAPE	(4HTAPE,2HNO)
QOPNCH	NO	2HNO	PUNCH/NO PUNCH PARAMETER FOR OUTPUT	(3HPUN,2HNO)
QOANPF	1.0000	1.0	AREA MULTIPLYING FACTOR	N/A
QOFMPF	1.0000	1.0	FLUX MULTIPLYING FACTOR	N/A
QOTMPF	1.0000	1.0	TIME MULTIPLYING FACTOR	N/A
QOTYPE	BOTH	NONE	PARAMETER TO DETERMINE TYPE OF OUTPUT	(3HTAB,2HAV,4HBOTH)
IQOARY	ALL	NONE	STEP NO. ARRAY DIRECTIVE	(3HALL,ARRAY NAME)

DATE 062778 TIME 010345

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 63

MODEL=SAMPLE CONFIG=CASE2 STEP=10006

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

ABSORBED Q OUTPUT COMPUTATION LINK.

ABSORBED HEAT RATE TABLES PUNCHED

Q = INPUT * RMPF WHERE RMPF = .10000+01
TIME = INPUT * TMPF WHERE TMPF = .10000+01
AREA IS ON SUBROUTINE CALL CARDS

1\$ TIME ARRAY
.000 , .367+00, .431+00, .432+00, .734+00
END\$
2\$ HEAT RATE ARRAY
.121+03, .239+03, .233+03, .503+02, .503+02
END\$
3\$ HEAT RATE ARRAY
.122+03, .290+02, .286+02, .249+02, .249+02
END\$
4\$ HEAT RATE ARRAY
.845+02, .540+02, .538+02, .499+02, .499+02
END\$
5\$ HEAT RATE ARRAY
.450+03, .148+03, .189+03, .139+03, .139+03
END\$
6\$ HEAT RATE ARRAY
.758+02, .290+02, .300+02, .249+02, .249+02
END\$
7\$ HEAT RATE ARRAY
.164+03, .585+03, .549+03, .363+02, .363+02
END\$

DATE 062778 TIME 010346 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 64

MODEL=SAMPLE CONFIG=CASE2 STEP=10006 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORNGEN/OPL0T
ABSORBED Q OUTPUT COMPUTATION LINK.

DA11KC SUBROUTINE CALL CARDS

AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000+01
DA11MC(1.46792175E 0,TIMEM,A1 ,A2 ,1.00000000E 0,Q1)\$
DA11MC(1.46792175E 0,TIMEM,A1 ,A3 ,1.00000000E 0,Q2)\$
DA11MC(1.46792175E 0,TIMEM,A1 ,A4 ,1.00000000E 0,Q3)\$
DA11MC(1.46792175E 0,TIMEM,A1 ,A5 ,1.00000000E 0,Q4)\$
DA11MC(1.46792175E 0,TIMEM,A1 ,A6 ,1.00000000E 0,Q12)\$
DA11MC(1.46792175E 0,TIMEM,A1 ,A7 ,1.00000000E 0,Q5)\$

DATE 062779 TIME 010346 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 65

MODEL=SAMPLE CONFIG=CASE2 STEP=10006

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T

ABSORBED Q OUTPUT COMPUTATION LINK.

AVERAGE ORBITAL HEATING RATE AND AREA CARDS PUNCHED

VALUES ARE RATE = INPUT (UNITS) * RMPF WHERE RMPF = .10000+01
VALUES ARE AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000+01

Q1 =1.31577134E 2
Q2 =5.05620456E 1
Q3 =5.99260890E 1
Q4 =2.21429661E 2
Q12 =3.90711117E 1
Q5 =2.52023339E 2

TOTAL TIME TO COMPUTE ABSORBED Q OUT .40

MODEL=SAMPLE CONFIG=CASE2 STEP=10006 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPL0T
ORBIT PLOTTER DATA OUTPUT

ODATA. ODATAS INPUT

PARAMETER	DESCRIPTION	OPTION #.	~DEFAULT
NV	VIEW NUMBER	1-6	1
VU	VIEW	3HALL 3H3-D 4HBETA 5HC1GMA 3HSUN 3HGEN	3HALL
SCL	VEHICLE SURFACE SCALING FACTOR INPUT IN INCHES (MAX VALUE = (3.15-SCLR)/2.)	REAL NO.	(3.15-SCLR)/2.
SCLR	ORBIT RADIUS INPUT IN INCHES FROM CENTER OF PLOT (RECOMMENDED VALUE = 1.6)	REAL NO.	8.*RPLN/7.
RPLN	PLANET RADIUS INPUT IN INCHES FROM CENTER OF PLOT (RECOMMENDED VALUE = 1.4)	REAL NO.	1.4
TRUEAN	TRUE ANOMALY (PRESENT VEHICLE POSITION IN DEGREES FROM PERIAPSIS)	REAL NO.	COMPUTED IF TIME Δ 0.
TIMEST	TIME OF PERIAPSIS PASSAGE	REAL NO.	NONE
TIME	TIME AT PRESENT VEHICLE POSITION	REAL NO.	COMPUTED IF TRUEAN Δ 0.
ISELN	ARRAY NAME CONTAINING NUMBER OF SURFACES TO BE SELECTIVELY PLOTTED	ARRAY NAME	PLOTS ALL SURFACES
ITIT	ARRAY NAME OF PLOT TITLE	ARRAY NAME	USES JOB TITLE
IROT _X , IROT _Y , IROT _Z	ORDER OF ROTATIONS (FOR IVU = 3HGEN)	1,2,3 (ANY ORDER)	1,2,3
ROT _X , ROT _Y , ROT _Z	VIEW ROTATIONS (FOR IVU = 3HGEN)	0 : ANG : 360	0.0 0.0 0.0

*INPUT ZERO FOR DEFAULT ACTION

CALLING SEQUENCE.

CALL ODATA (INV, VU, SCL, SCLR, RPLN, TRUEAN, TIMEST, TIME, ISELN, ITIV, IROTX, IROTY, IROTZ, ROTX, ROTY, ROTZ)
OR

CALL ODATAS (INV, VU, SCL, SCLR, RPLN, TRUEAN, TIMEST, TIME)

NOTE: IF NO CALLS TO ODATA/ODATAS ARE MADE, A CALL TO OPLOT WILL
RESULT IN ALL VIEWS BEING AUTOMATICALLY SCALED AND GENERATED.

DATE 062770 TIME 010351 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 67

MODEL=SAMPLE CONFIG=CASE2 STEP=10006 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT
ORBIT PLOTTER DATA OUTPUT

DATE 062770 TIME 010351 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION PAGE 60
 MODEL=SAMPLE CONFIG=CASE2 STEP=10006 SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLOT
 ORBIT PLOTTER DATA OUTPUT

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS ++++				
.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA ++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.00000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA ++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX, IROTY, IROTZ.		1 2 3	
++++ SPIN DATA ++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CW=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCW POSITIVE		0.0	RATE

DATE 062778 TIME 010352 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 69

MODEL=SAMPLE CONFIG=CASE2 STEP=10006
ORBIT PLOTTER DATA OUTPUT

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORBGEN/OPLLOT

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	HDS
.20900+09	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	HSS
.10000+16	PLANET-SUN DISTANCE	PSD		.14679+01	ORBIT PERIOD	PERIOD
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

VIEW=3-D	SCALE= .3037	VIEW NUMBER=1
VIEW=BETA	SCALE= .3037	VIEW NUMBER=1
VIEW=CIGMA	SCALE= .3037	VIEW NUMBER=1
VIEW=SUN VIEW	SCALE= .3037	VIEW NUMBER=1
VIEW=3-D	SCALE= .3037	VIEW NUMBER=2
VIEW=BETA	SCALE= .3037	VIEW NUMBER=2
VIEW=CIGMA	SCALE= .3037	VIEW NUMBER=2
VIEW=SUN VIEW	SCALE= .3037	VIEW NUMBER=2
VIEW=3-D	SCALE= .3037	VIEW NUMBER=3
VIEW=BETA	SCALE= .3037	VIEW NUMBER=3
VIEW=CIGMA	SCALE= .3037	VIEW NUMBER=3
VIEW=SUN VIEW	SCALE= .3037	VIEW NUMBER=3

IT HAS BEEN A PLEASURE SERVING YOU. I HOPE YOU ENJOY YOUR 12. FRAMES OF S-C 4060 OUTPUT.

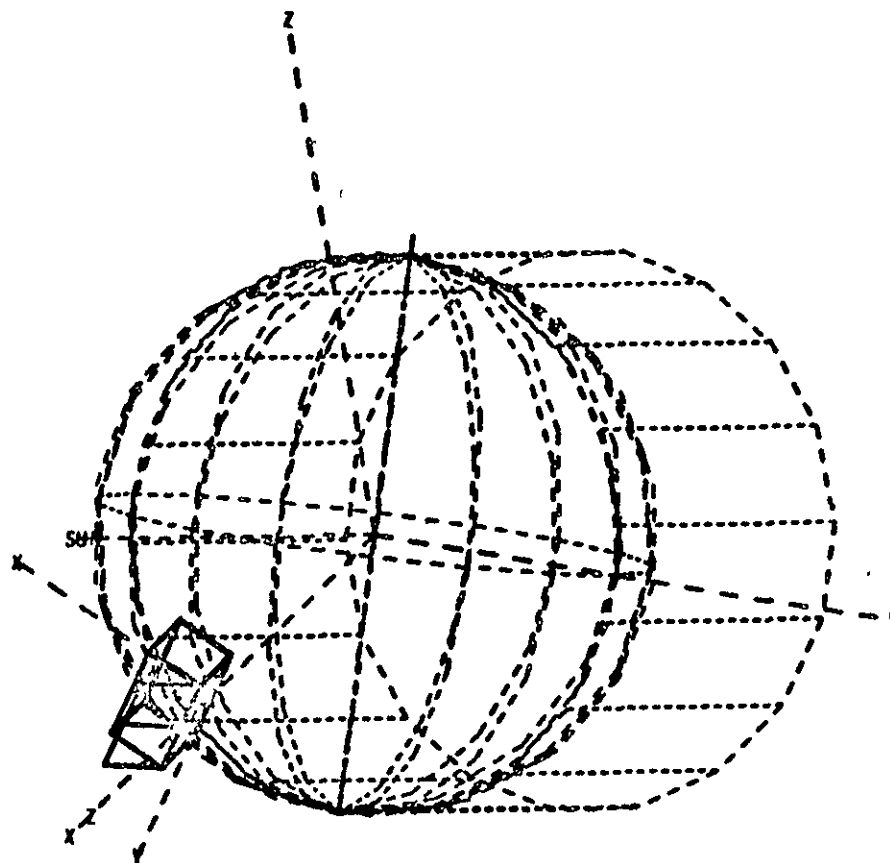
++NOTE++ TRASY5 GENERATED 12 PLOT FRAMES

NORMAL TERMINATION BY PROCESSOR

@PHD.PLED

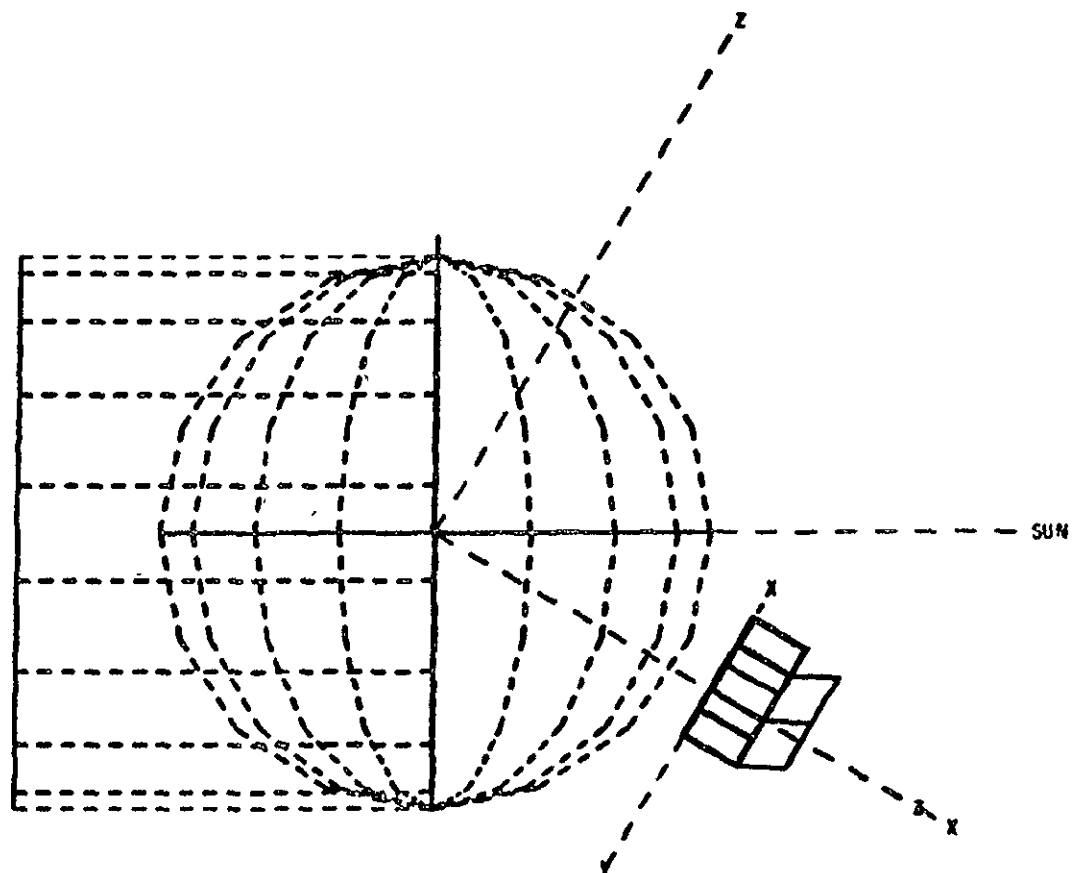
@BRKPT PRINTS

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/BCAL/DR3GEN/OPL0T



H-207
VIEW = 3-D
SCALE = .3037
TIME = .000

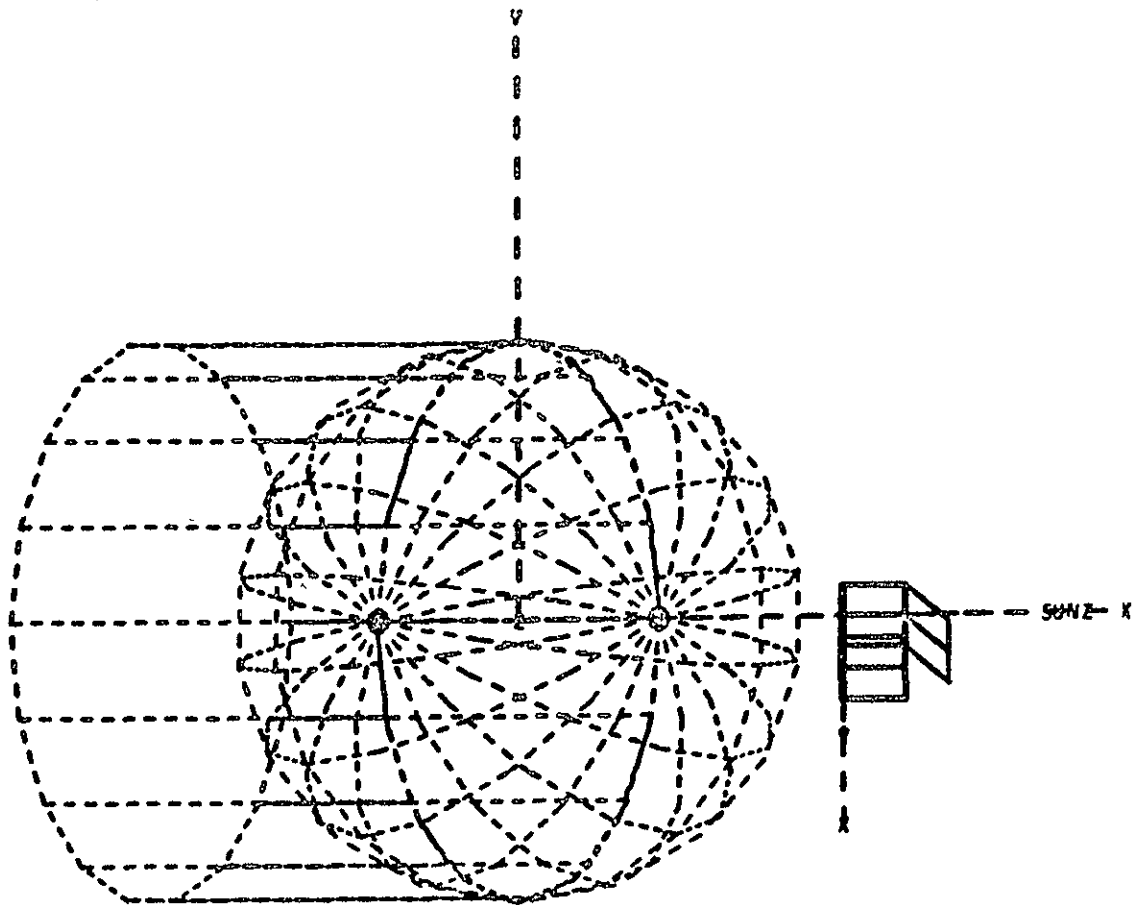
SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/DRAGEN/DPL0T



H-208

VIEW = BETA
SCALE = .3037
TIME = .000

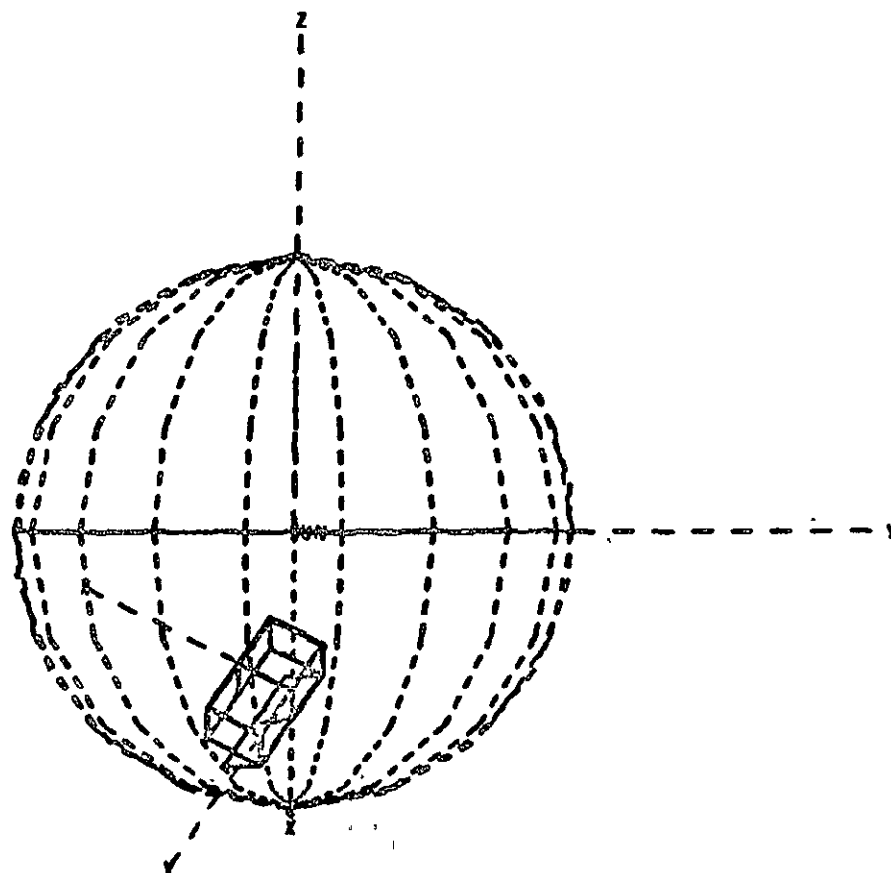
SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/ECCAL/ORDGEN/OPL0T



H-209

VIEW = CIGMA
SCALE = .3037
TIME = .000

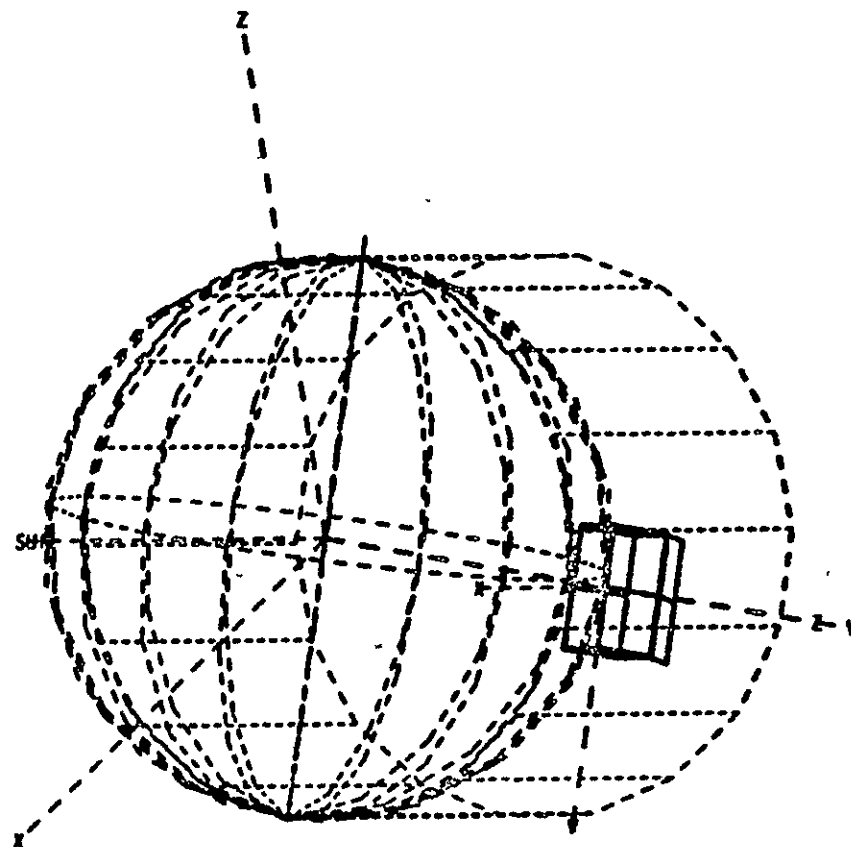
SAMPLE CASE 2 - /SFCAL/FFCAL/GDCAL/RECAL/ORIGEN/OPLOT



H-210

VIEW = SUN VIEW
SCALE = .3037
TIME = .000

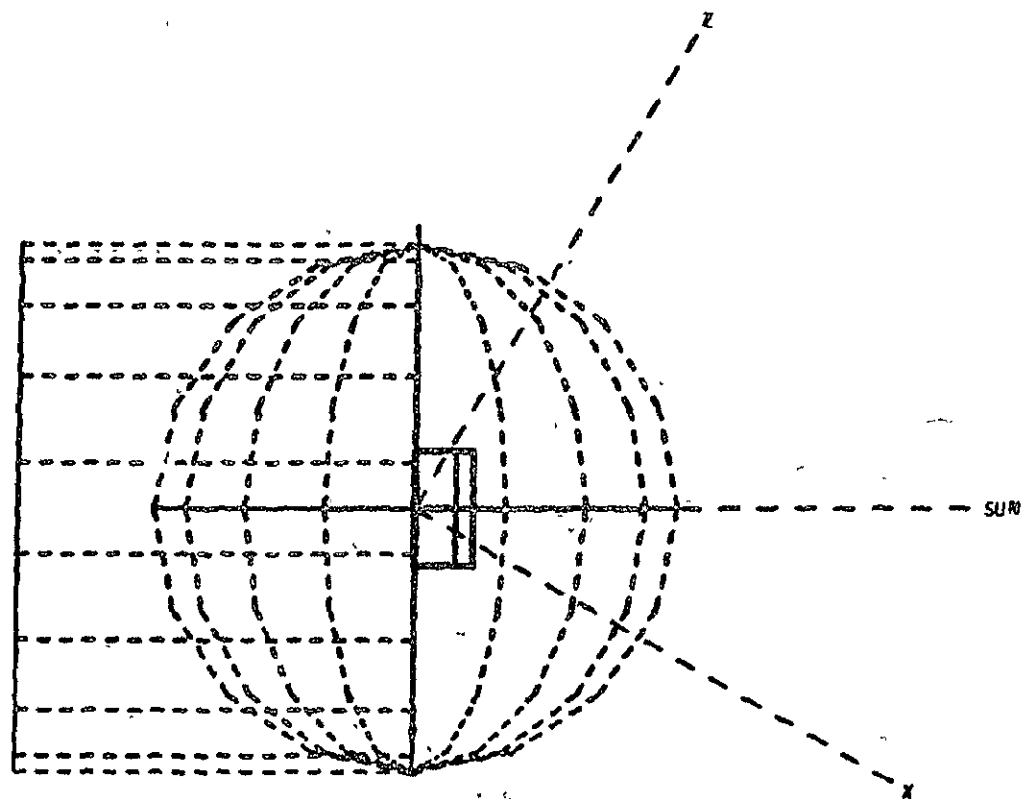
SAMPLE CASE 2 - /SFCAL/FFCAL/BCAL/RCAL/ORIGEN/OPL0T



H-211

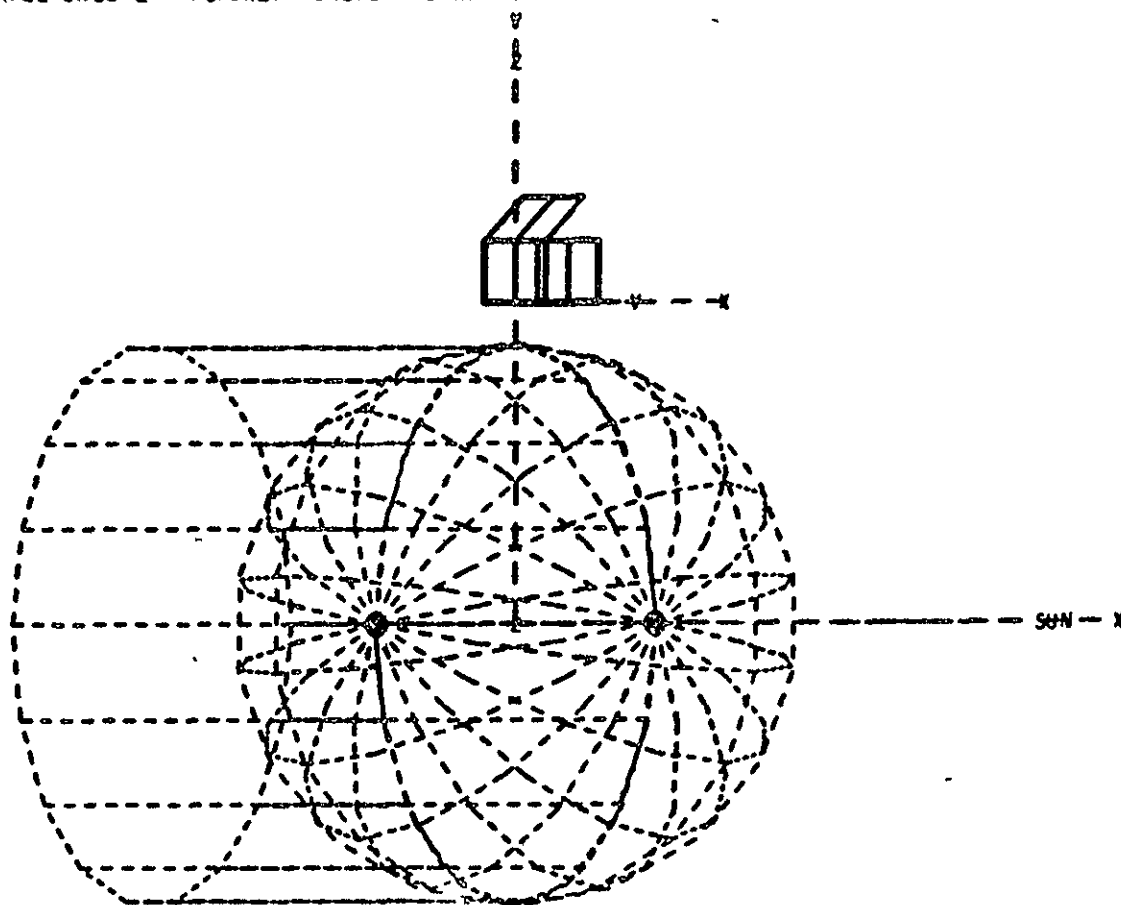
VIEW = 3-D
SCALE = .3037
TIME = .000

SAMPLE CASE 2 - /SFCAL/FFCAL/GDCAL/BCCAL/DRBGEN/DPLDY



H-212
VIEW = BETA
SCALE = .3037
TIME = .000

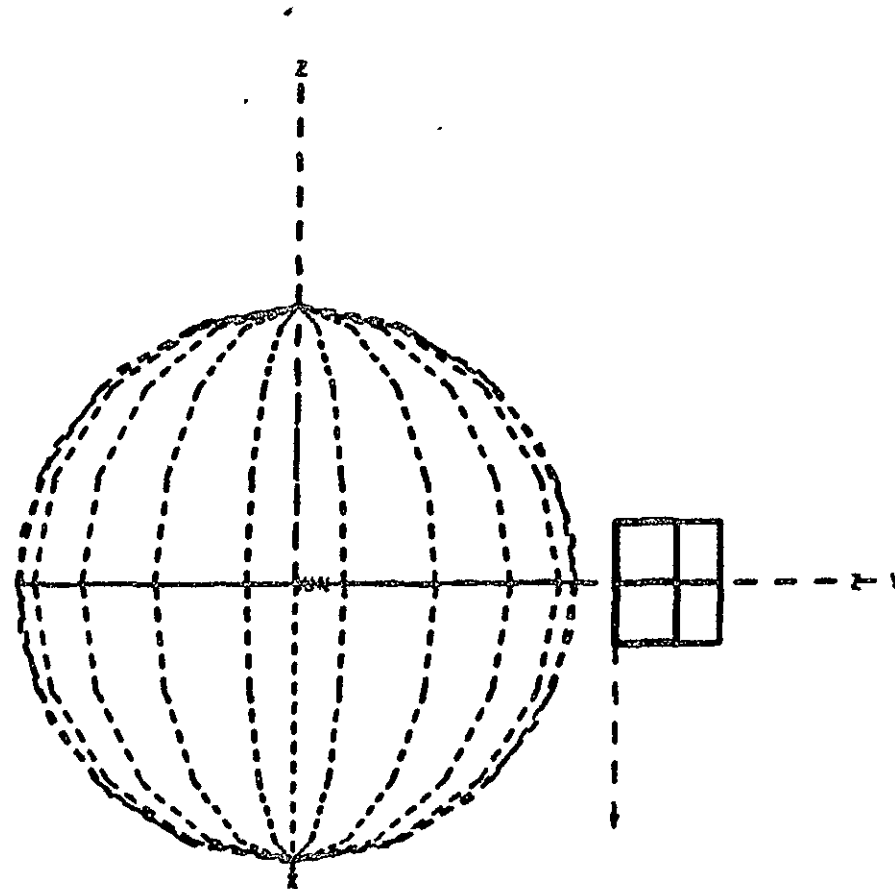
SAMPLE CASE 2 - /SFCAL/FFCAL/6BCAL/RCCAL/ORBGEN/DPLOT



H-213

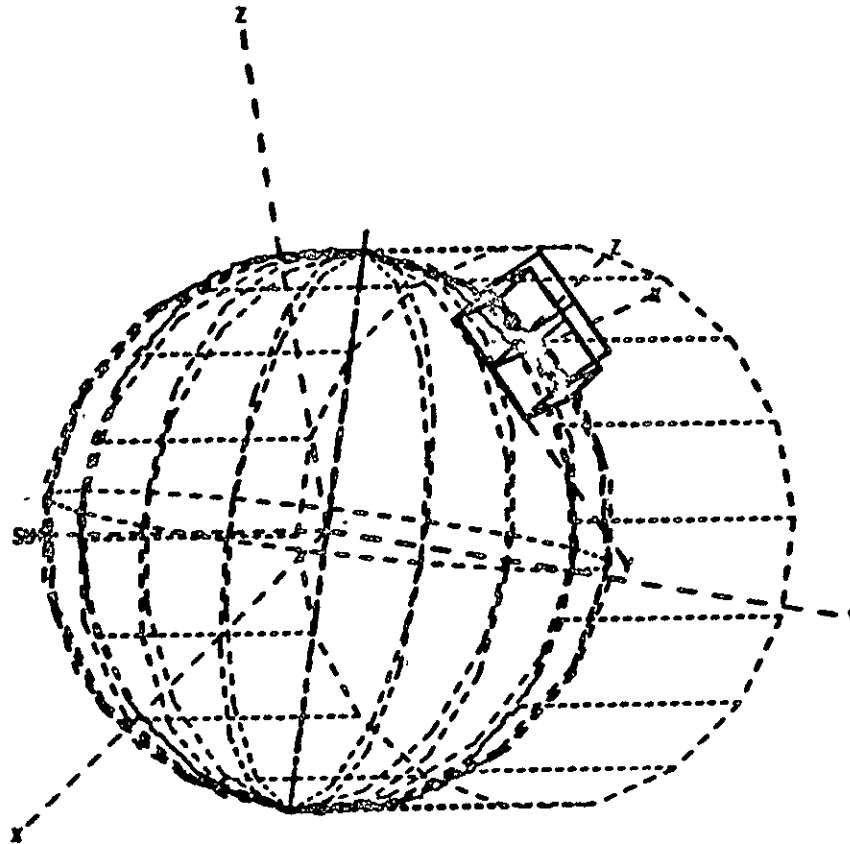
VIEW = CIGMA
SCALE = .3037
TIME = .000

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORDGEN/OPLO7



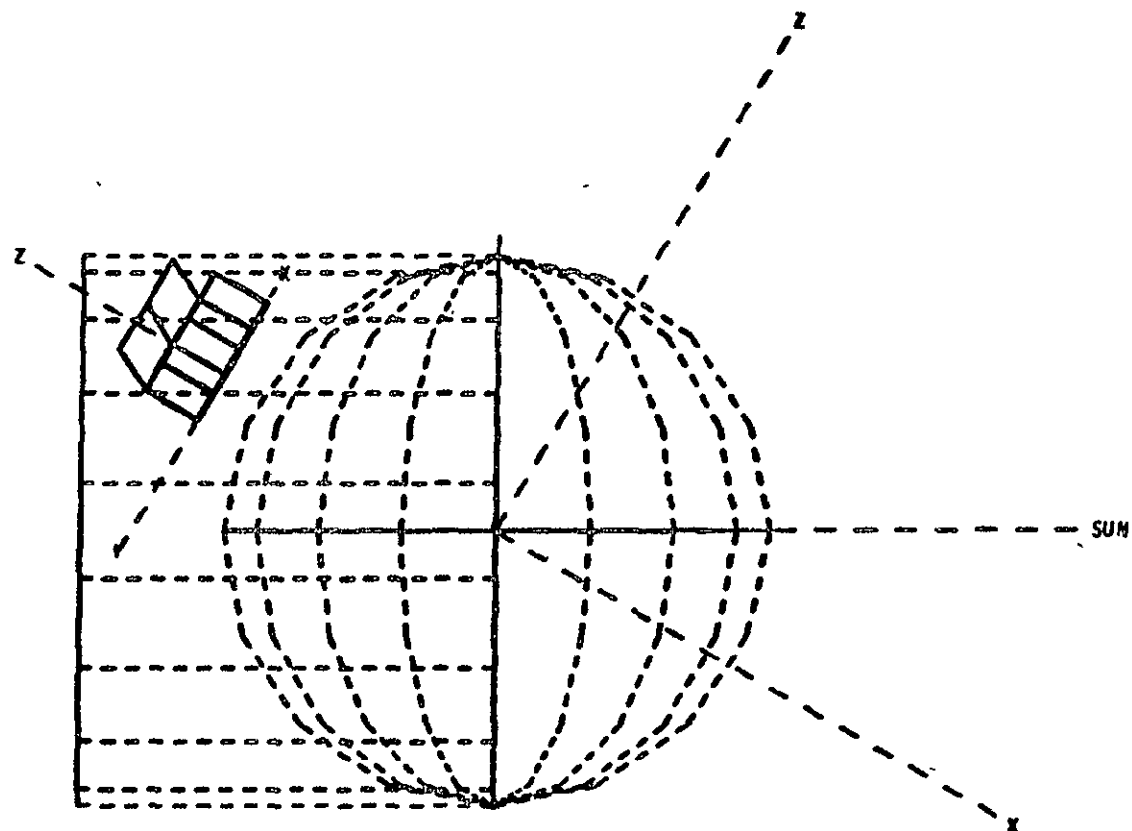
H-214
VIEW = SUN VIEW
SCALE = .3037
TIME = .000

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/ACCAL/ODSGEN/OPL0T



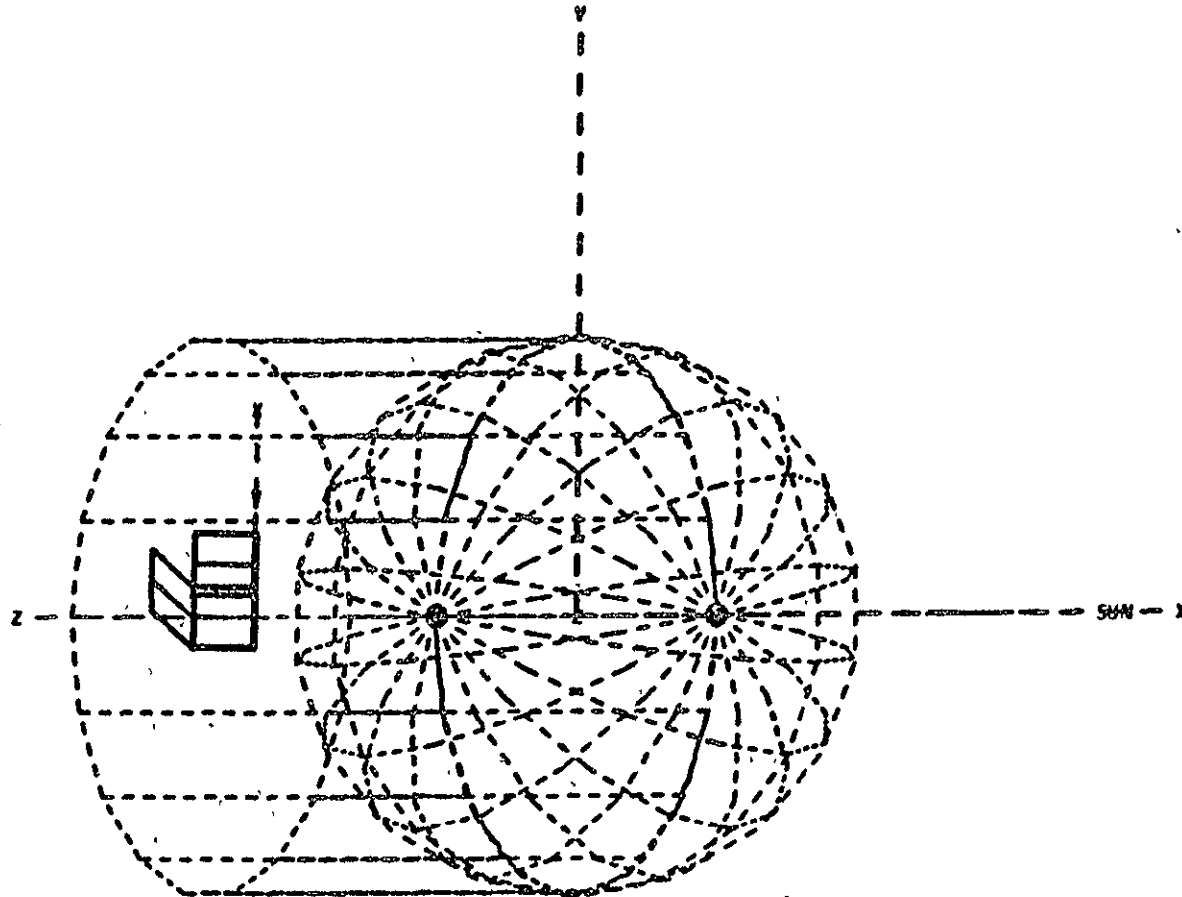
H-215
VIEW = 3-0
SCALE = .3037
TIME = .000

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/DRBGEW/OPLDT



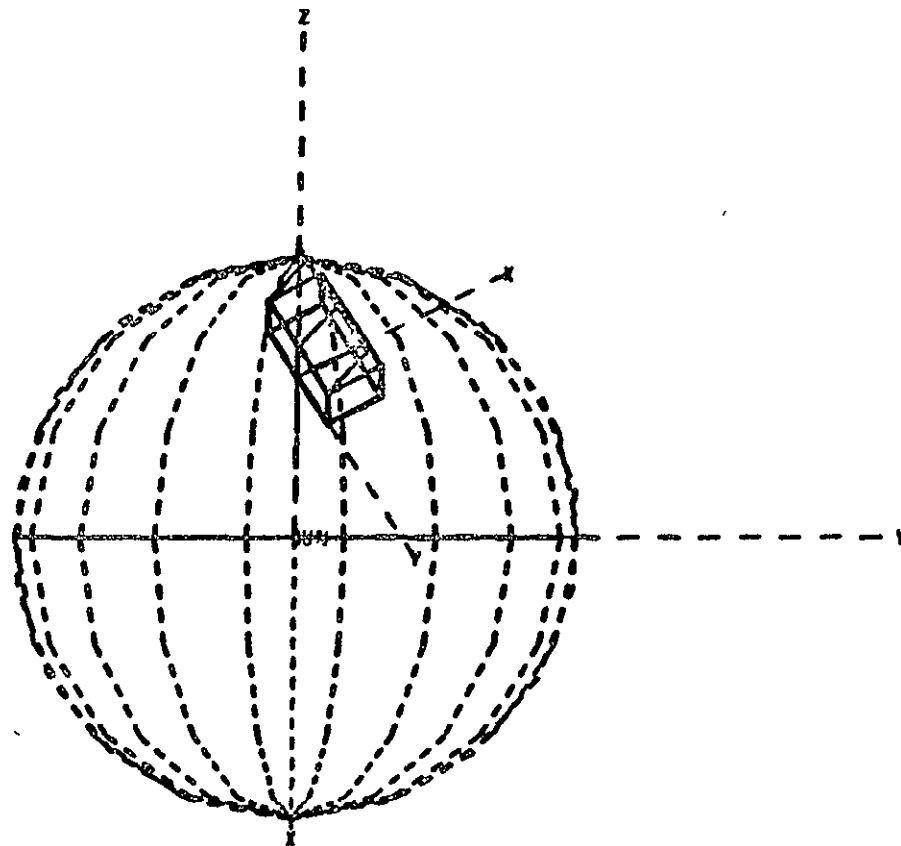
H-216
VIEW = BETA,
SCALE = .3037
TIME = .000

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/DR3GEN/DPLOT



VIEW = CIGMA
SCALE = .3037
TIME = .000

SAMPLE CASE 2 - /SFCAL/FFCAL/GBCAL/RCCAL/ORDGEN/OPL0T



VIEW = SUN VIEW
SCALE = .3037
TIME = .000

H-218

SAMPLE CASE 3

SAMPLE CASE 3

QED,R VOGTB.CASE3
 FILE IN FIELD 1 DISABLED--ACCEPTED
 FILE IN FIELD 1 IN USE BY ANOTHER RUN
 READ-ONLY MODE
 CASE UPPER ASSUMED
 ED 14.02-06/20-20:39-(0.)
 EDIT

NO DECK VOGT

1:ORUN,R/R RVHH03,3240-F261-C,ES3-N03711.06.300
 10:QASG,T RSI.,BC,X03562
 11:QADD ES3-TRASYS*TRASYS.STARTM
 12:QSETC 0100
 13:QADD PREPRO
 14:HEADER OPTIONS DATA
 15:TITLE SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN
 16:C SKIPPING SHADOW FACTOR TABLES ON RSI.
 17:C RESTARTING FORM FACTORS.
 18:C COMBINING FORM FACTORS.
 19:C CALCULATING DIRECT INCIDENT FLUXES WITHOUT THE USE OF
 20:C SHADOW FACTOR TABLES.
 21:C
 22: MODEL = SAMPLE
 23: RSI = RSTSAH2
 24: RSO = RSTSAH3
 25:HEADER EDIT DATA
 26:QD,153,156
 27:C
 28:C-----SKIP THE SHADOW FACTOR TABLES ON RSI. THIS IS ACCOMPLISHED
 29:C-----BY REPLACING THE HL SFCAL CARD WITH A QCALL RSTON CARD
 30:C-----TO SET THE SKIP FLAG
 31:C
 32: CALL RSTON
 33:QD,163,166
 34:C
 35:C-----COMBINE FORM FACTORS
 36:C
 37: CALL RSTOFF
 38: CALL CHDATA(0.5HCASE3,2HFF,0,0)
 39:L CHCAL
 40:C
 41:C-----CALCULATE GRAY BODY MATRICES USING COMBINED FORM FACTORS.
 42:C
 43: CALL GBDATA(BOTH,0,CH)
 44:QD,171
 45: CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,0)
 46:QD,187,193
 47:QPHD,BLEP
 48:QASG,T/S RSO.,BC,RSO,92,RSO APPENDIX H, CASE 3.
 49:QADD PROCSS
 50:QBRKPT PRINTS
 57:QFIN
 NO CORRECTIONS APPLIED.

QASG,T RSI.,BC,X03562

NASA / MARTIN HARRIETTA
THERMAL RADIATION ANALYSIS SYSTEM
UNIVAC 1110 / EXEC 8

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TRASYS 11

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PRE - PROCESSOR EXECUTION

VERSION.MODIFICATION ... UC2E3
MODIFICATION DATE 052678
DATE OF RUN 062878
TIME OF RUN 205235
JOB NUMBER RVMH03

DATE 062878 TIME - 205238 - THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 1
 MODEL = N/A
 OPTION AND TITLE DATA BLOCKS
 CARD ORIGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL
 INPUT HEADER OPTIONS DATA
 INPUT TITLE SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORDGEN
 INPUT C SKIPPING SHADOW FACTOR TABLES ON RSI.
 INPUT C RESTARTING FORM FACTORS.
 INPUT C COMBINING FORM FACTORS.
 INPUT C CALCULATING DIRECT INCIDENT FLUXES WITHOUT THE USE OF
 INPUT C SHADOW FACTOR TABLES.
 INPUT C
 INPUT MODEL = SAMPLE
 INPUT RSI = RSTSAM2
 INPUT RSO = RSTSAM3

DATE 062070 TIME 205230 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 2

MODEL = SAMPLE SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN
TRASYS INFORMATION TO USER

*
* ATTENTION TRASYS USERS *
*

THIS SECTION OF THE TRASYS PRINTOUT WAS DEvised TO
INFORM THE TRASYS USERS OF THE STATUS OF THE TRASYS
PROGRAM WITHOUT HAVING TO PRINTOUT ALL THE STATUS
INFORMATION ON EVERY RUN. TO OBTAIN ADDITIONAL
INFORMATION ON HOW TO USE THIS SECTION OF THE TRASYS
PRINTOUT, PLACE A (INFO=INFO) IN THE OPTIONS DATA
BLOCK.

FOR TRASYS ASSISTANCE AND/OR POSSIBLE TRASYS PROGRAM
PROBLEMS, PLEASE CONTACT BOB VOGT AT JSC-2326.

NEHRL 08/29/77 DOCUMENTATION ADDITION

THE TRASYS -N- VERSION HAS BEEN UPDATED TO THE UC2E2
AND UL2E4 LEVEL.
SEE LATEST USERS MANUAL FOR INFORMATION ON USER-
CALLED SUBROUTINE ARGUMENT CHANGES AND NEW
CAPABILITIES.

, END OF TRASYS INFORMATION FILE

DATE 062878 TIME 205241 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 3

MODEL = SAMPLE
MODEL HISTORY SAMPLE CASE 3 - FFCAL/CHCAL/GDCAL/RCCAL/ORDGEN

MODEL NAME SAMPLE

MODEL TITLE SAMPLE CASE 3 - FFCAL/CHCAL/GDCAL/RCCAL/ORDGEN

MOD LABEL	RUN JOB NUMBER	RUN DATA	RUN TIME	RS1 TAPE	RS0 TAPE	RT1 TAPE	RT0 TAPE	CNERG TAPE	EMERG TAPE	BCDOU TAPE	TRAJ TAPE	USER1 TAPE	USER2 TAPE
AA	RVMH01	062278	202625										RSTSAM
AB	RVMH02	062778	005225	RSTSAM	RSTSAM								
AC	RVMH03	062878	205238	RSTSAM	RSTSAM								

DATE 062070 TIME 205242 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 4

MODEL = SAMPLE
SOURCE DATA EDIT DIRECTIVES

SAMPLE CASE 3 - FFCAL/CHCAL/GDCAL/RCCAL/DRGEN

CARD ORIGIN 12345670 1 2345670 2 2345670 3 2345670 4 2345670 5 2345670 6 2345670 7 2345670 8 EDIT NO. OLD EDIT NO. LABEL

```

HEADER EDIT DATA
****
D      *D,153,156
D      C
D      C-----READ AND PRINT THE SHADOW FACTOR TABLES FROM RSI FOR USE IN
D      C-----SAMPLE CASE 2 IN THE CALCULATION OF DIRECT FLUXES.
D      C
D      C
D      C-----SKIP THE SHADOW FACTOR TABLES ON RSI. THIS IS ACCOMPLISHED
D      C-----BY REPLACING THE BL      SFCALR CARD WITH A RCALL RSTONR CARD
D      C-----TO SET THE SKIP FLAG
D      C
D      CALL RSTON
D      *D,163,166
D      C
D      C-----READ THE GRAY BODY MATRICES FROM RSI
D      C
D      CALL GBDATA(BOTH,0,FF)
D      C
D      C-----COMBINE FORM FACTORS
D      C
D      CALL RSTOFF
D      CALL CHDATA(0,5HCASE3,2HFF,0,0)
D      L      CHCAL
D      C
D      C-----CALCULATE GRAY BODY MATRICES USING COMBINED FORM FACTORS.
D      C
D      CALL GBDATA(BOTH,0,CH)
****
D      *D,171
D      CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,5HCASE2)
D      CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,0)
****
D      *D,187,193
D      C
D      C-----MAKE ORBIT PLOTS
D      C
D      CALL ODATAS(1,0,0,0,0,0,0,0)
D      CALL ODATAS(2,0,0,0,0,90,0,0)
D      CALL ODATAS(3,0,0,0,0,180,0,0)
D      L      OPLOT

```

OLD-	153	AA
OLD-	154	AB
OLD-	155	AA
OLD-	156	AA
	153	AC
	154	AC
	155	AC
	156	AC
	157	AC
	158	AC
OLD-	163	AA
OLD-	164	AB
OLD-	165	AA
OLD-	166	AA
	165	AC
	166	AC
	167	AC
	168	AC
	169	AC
	170	AC
	171	AC
	172	AC
	173	AC
	174	AC
OLD-	171	AB
	179	AC
OLD-	187	AB
OLD-	188	AB
OLD-	189	AB
OLD-	190	AB
OLD-	191	AB
OLD-	192	AB
OLD-	193	AB

DATE 062878 TIME 205253 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 5

MODEL = SAMPLE SURFACE DATA INPUT BLOCK SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORSGEN

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

RSI	HEADER SURFACE DATA	1	OLD-	1	AA
RSI	C	2	OLD-	2	AA
RSI	C-----THIS SURFACE DATA BLOCK IS USED IN SAMPLE CASES 1 THROUGH 5	3	OLD-	3	AA
RSI	C-----WITH VARIOUS PORTIONS OF IT BEING ACTIVATED FOR THE DIFFERENT	4	OLD-	4	AA
RSI	C-----CASES.	5	OLD-	5	AA
RSI	C	6	OLD-	6	AA
RSI	BCS BOXINR	7	OLD-	7	AA
RSI	S SURFN = 1	8	OLD-	8	AA
RSI	TYPE = RECT	9	OLD-	9	AA
RSI	ACTIVE = BOTTOM	10	OLD-	10	AA
RSI	PROP = 0.9,0.9	11	OLD-	11	AA
RSI	P1 = 1.0, 0.0, 1.0	12	OLD-	12	AA
RSI	P2 = 1.0, 0.0, 0.0	13	OLD-	13	AA
RSI	P3 = 1.0, 1.0, 0.0	14	OLD-	14	AA
RSI	CON = * INNER RIGHT FRONT *	15	OLD-	15	AA
RSI	S SURFN = 2	16	OLD-	16	AA
RSI	TYPE = RECT	17	OLD-	17	AA
RSI	ACTIVE = BOTTOM	18	OLD-	18	AA
RSI	PROP = 0.9,0.9	19	OLD-	19	AA
RSI	P1 = 1.0, 1.0, 1.0	20	OLD-	20	AA
RSI	P2 = 1.0, 1.0, 0.0	21	OLD-	21	AA
RSI	P3 = 0.0, 1.0, 0.0	22	OLD-	22	AA
RSI	CON = * INNER RIGHT SIDE *	23	OLD-	23	AA
RSI	S SURFN = 3	24	OLD-	24	AA
RSI	TYPE = RECT	25	OLD-	25	AA
RSI	ACTIVE = TOP	26	OLD-	26	AA
RSI	PROP = 0.9,0.9	27	OLD-	27	AA
RSI	P1 = 0.0, 0.0, 1.0	28	OLD-	28	AA
RSI	P2 = 0.0, 0.0, 0.0	29	OLD-	29	AA
RSI	P3 = 0.0, 1.0, 0.0	30	OLD-	30	AA
RSI	CON = * INNER RIGHT BACK *	31	OLD-	31	AA
RSI	S SURFN = 4	32	OLD-	32	AA
RSI	TYPE = RECT	33	OLD-	33	AA
RSI	ACTIVE = TOP	34	OLD-	34	AA
RSI	PROP = 0.9,0.9	35	OLD-	35	AA
RSI	P1 = 1.0, 1.0, 0.0	36	OLD-	36	AA
RSI	CON = * INNER RIGHT BOTTOM *	37	OLD-	37	AA
RSI	BCS BOXINL,IMGBCS=BOXINR,NINC=10,IREFSF=1000	38	OLD-	38	AA
RSI	C	39	OLD-	39	AA
RSI	C-----THE FOREGOING CARD IMAGES BCS BOXINR IN REFERENCE PLANE 1000	40	OLD-	40	AA
RSI	C-----TO CREATE BCS BOXINL. THE INTERIOR OF THE BOX WAS INPUT IN	41	OLD-	41	AA
RSI	C-----THIS MANNER TO FACILITATE THE INPUT OF SAMPLE CASE 4 TO SHOW	42	OLD-	42	AA
RSI	C-----THE USE OF 'MESS' AND 'ERN' NODES.	43	OLD-	43	AA
RSI	C	44	OLD-	44	AA
	IMAGING SURFACE (1) BCS (BOXINR), GENERATING SURFACE (11) BCS (BOXINL)				
	IMAGING SURFACE (2) BCS (BOXINR), GENERATING SURFACE (12) BCS (BOXINL)				
	IMAGING SURFACE (3) BCS (BOXINR), GENERATING SURFACE (13) BCS (BOXINL)				

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/DRBGEN

CARD ORIGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

		IMAGING SURFACE (4) BCS (BOXINR). GENERATING SURFACE (14) BCS (BOXINL)			
RS1	R	REFNO = 1000	45	OLD-	45 AA
RS1		P1 = 1.0, 0.0, 1.0	46	OLD-	46 AA
RS1		P2 = 1.0, 0.0, 0.0	47	OLD-	47 AA
RS1		P3 = 0.0, 0.0, 0.0	48	OLD-	48 AA
RS1		COM = * IMAGING PLANE *	49	OLD-	49 AA
RS1	BCS	LIDINR	50	OLD-	50 AA
RS1	S	SURFN = 5	51	OLD-	51 AA
RS1		TYPE = RECT	52	OLD-	52 AA
RS1		ACTIVE = BOTTOM	53	OLD-	53 AA
RS1		PROP = 0.9, 0.9	54	OLD-	54 AA
RS1		P1 = 1.0, 1.0, 0.0	55	OLD-	55 AA
RS1		COM = * INNER RIGHT LID *	56	OLD-	56 AA
RS1	S	SURFN = 15	57	OLD-	57 AA
RS1		IMAGSF = 5	58	OLD-	58 AA
RS1		IREFSF = 1000	59	OLD-	59 AA
RS1		COM = * INNER LEFT LID *	60	OLD-	60 AA
RS1	BCS	BOXOUT	61	OLD-	61 AA
RS1	S	SURFN = 21	62	OLD-	62 AA
RS1		TYPE = BOX5	63	OLD-	63 AA
RS1		ACTIVE = OUT	64	OLD-	64 AA
RS1		SHADE = NO	65	OLD-	65 AA
RS1		PROP = 0.2, 0.9	66	OLD-	66 AA
RS1		P1 = 1.01, -1.01, 1.01	67	OLD-	67 AA
RS1		P2 = 1.01, 1.01, 1.01	68	OLD-	68 AA
RS1		P3 = -0.01, 1.01, 1.01	69	OLD-	69 AA
RS1		P4 = -0.01, 1.01, -0.01	70	OLD-	70 AA
RS1		COM = * OUTER SURFACES *	71	OLD-	71 AA
RS1	BCS	LIDOUT	72	OLD-	72 AA
RS1	S	SURFN = 26	73	OLD-	73 AA
RS1		TYPE = RECT	74	OLD-	74 AA
RS1		ACTIVE = TOP	75	OLD-	75 AA
RS1		SHADE = NO	76	OLD-	76 AA
RS1		PROP = 0.2, 0.9	77	OLD-	77 AA
RS1		P1 = 1.01, -1.01, 0.01	78	OLD-	78 AA
RS1		P2 = 1.01, 1.01, 0.01	79	OLD-	79 AA
RS1		P3 = -0.01, 1.01, 0.01	80	OLD-	80 AA
RS1		COM = * OUTER SURFACE OF LID *	81	OLD-	81 AA
RS1	C		82	OLD-	82 AA
RS1		C-----THE NEXT TWO BCS'S (MESSR AND MESSL) ARE ACTIVATED IN SAMPLE	83	OLD-	83 AA
RS1		C-----CASE 4 ONLY.	84	OLD-	84 AA
RS1	C		85	OLD-	85 AA
RS1	BCS	MESSR	86	OLD-	86 AA
RS1	S	SURFN = 101	87	OLD-	87 AA
RS1		TYPE = RECT	88	OLD-	88 AA
RS1		ACTIVE = TOP	89	OLD-	89 AA
RS1		PROP = 1.0, 1.0	90	OLD-	90 AA

DATE 062070 TIME 205300

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 9 VERSION

PAGE 7

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

CARD	ORIGIN	12345670	1	2345670	2	2345670	3	2345670	4	2345670	5	2345670	6	2345670	7	2345670	8	EDIT NO.	OLD EDIT NO.	LABEL			
RSI		P1		1.0, 0.0, 1.0														91	OLD-	91	AA		
RSI		P2		1.0, 0.0, 0.0														92	OLD-	92	AA		
RSI		P3		0.0, 0.0, 0.0														93	OLD-	93	AA		
RSI		COM		* PRIMARY HESS NODE, RIGHT SIDE *													94	OLD-	94	AA			
RSI	BCS	HESSL																95	OLD-	95	AA		
RSI	S	SURFN		111														96	OLD-	96	AA		
RSI		TYPE		RECT														97	OLD-	97	AA		
RSI		ACTIVE		BOTTOM														98	OLD-	98	AA		
RSI		PROP		1.0, 1.0														99	OLD-	99	AA		
RSI		P1		1.0, 0.0, 1.0														100	OLD-	100	AA		
RSI		P2		1.0, 0.0, 0.0														101	OLD-	101	AA		
RSI		P3		0.0, 0.0, 0.0														102	OLD-	102	AA		
RSI		COM		* PRIMARY HESS NODE, LEFT SIDE *													103	OLD-	103	AA			
RSI	C																	104	OLD-	104	AA		
RSI	C			C-----THE FOLLOWING BCS (LIDSP) IS ACTIVATED IN SAMPLE CASE 5 ONLY.																105	OLD-	105	AA
RSI	C																	106	OLD-	106	AA		
RSI	BCS	LIDSP																107	OLD-	107	AA		
RSI	S	SURFN		200														108	OLD-	108	AA		
RSI		TYPE		RECT														109	OLD-	109	AA		
RSI		ACTIVE		BOTTOM														110	OLD-	110	AA		
RSI		PROP		0.1, 0.1														111	OLD-	111	AA		
RSI		SPRI		0.0														112	OLD-	112	AA		
RSI		SPRS		0.0														113	OLD-	113	AA		
RSI		P1		1.0, -1.0, 0.0														114	OLD-	114	AA		
RSI		P2		1.0, 1.0, 0.0														115	OLD-	115	AA		
RSI		P3		0.0, 1.0, 0.0														116	OLD-	116	AA		
RSI		COM		* SPECULAR LID *													117	OLD-	117	AA			

DATE 062878 TIME 205312 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 8

MODEL = SAMPLE
BCS DATA INPUT BLOCK

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORDGEN

CARD	ORIGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL	
RSI	HEADER	BCS DATA																118	OLD-	118	AA
RSI	BCS	BOXINR																119	OLD-	119	AA
RSI	BCS	BOXINL																120	OLD-	120	AA
RSI	BCS	LIDINR	.0.	.0.	.1.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	121	OLD-	121	AA
RSI	BCS	BOXOUT																122	OLD-	122	AA
RSI	BCS	LIDOUT	.0.	.0.	.1.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	123	OLD-	123	AA
RSI	BCS	MESSR																124	OLD-	124	AA
RSI	BCS	MESSL																125	OLD-	125	AA
RSI	BCS	LIDSP	.0.	.0.	.1.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	.0.	126	OLD-	126	AA

DATE 062870 TIME 205315 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 0 VERSION PAGE 9

MODEL = SAMPLE
CORRESPONDENCE DATA INPUT BLOCK

CARD	ORIGIN	12345678 1	2345678 2	2345678 3	2345678 4	2345678 5	2345678 6	2345678 7	2345678 8	EDIT NO.	OLD	EDIT NO.	LABEL
RSI	HEADER CORRESPONDENCE DATA									127	OLD-	127	AA
RSI	C									128	OLD-	128	AA
RSI	C-----ENTER CORRESPONDENCE DATA FOR CASE 2									129	OLD-	129	AA
RSI	C									130	OLD-	130	AA
RSI	FIG CASE2									131	OLD-	131	AA
RSI	1	= 1,11,22								132	OLD-	132	AA
RSI	2	= 2,25								133	OLD-	133	AA
RSI	3	= 3,13,24								134	OLD-	134	AA
RSI	4	= 4,14,21								135	OLD-	135	AA
RSI	5	= 5,15,26								136	OLD-	136	AA
RSI	12	= 12,23								137	OLD-	137	AA
RSI	C									138	OLD-	138	AA
RSI	C-----ENTER CORRESPONDENCE DATA FOR CASE 3 TO COMBINE FORM FACTORS									139	OLD-	139	AA
RSI	C									140	OLD-	140	AA
RSI	FIG CASE3,FF									141	OLD-	141	AA
RSI	1	= 1,11,22								142	OLD-	142	AA
RSI	2	= 2,25								143	OLD-	143	AA
RSI	3	= 3,13,24								144	OLD-	144	AA
RSI	4	= 4,14,21								145	OLD-	145	AA
RSI	5	= 5,15,26								146	OLD-	146	AA
RSI	12	= 12,23								147	OLD-	147	AA

DATE 062070 TIME 205319 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 10
 MODEL = SAMPLE SAMPLE CASE 3 - FFCAL/CMCAL/GSCAL/RCCAL/ORRGEN
 OPERATION DATA INPUT BLOCK (PASS 1)
 CARD ORIGIN 12345670 1 2345670 2 2345670 3 2345670 4 2345670 5 2345670 6 2345670 7 2345670 8 EDIT NO. OLD EDIT NO. LABEL
 RSI HEADER OPERATIONS DATA 140 OLD- 140 AA

+++++ OPERATIONS DATA BLOCK (PASS 1) COMPLETE +++++

DATE 062870 TIME 205323

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION

PAGE 11

MODEL = SAMPLE

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORRGEN

OPERATION DATA INPUT BLOCK (PASS 2)

CARD	ORIGIN	12345670 1	2345670 2	2345670 3	2345670 4	2345670 5	2345670 6	2345670 7	2345670 8	EDIT NO.	OLD	EDIT NO.	LABEL
RSI	C									149	OLD-	149	AA
RSI	C-----	BUILD THE CASE 1 CONFIGURATION FOR SFCAL/FFCAL/GBCAL RESTART								150	OLD-	150	AB
RSI	C									151	OLD-	151	AA
PROG	STEP	-1								0			
RSI	BUILD	CASE1,BOXINR,BOXINL,LIDINR,BOXOUT,LIDOUT								152	OLD-	152	AA
PROG		CALL BUILDG (BOXINR,6HCASE1)								0			
PROG		CALL ADD (BOXINL)								0			
PROG		CALL ADD (LIDINR)								0			
PROG		CALL ADD (BOXOUT)								0			
PROG		CALL ADD (LIDOUT)								0			
INPUT	C									153			AC
INPUT	C-----	SKIP THE SHADOW FACTOR TABLES ON RSI. THIS IS ACCOMPLISHED								154			AC
INPUT	C-----	BY REPLACING THE "L SFCAL" CARD WITH A "CALL RSTON" CARD								155			AC
INPUT	C-----	TO SET THE SKIP FLAG								156			AC
INPUT	C									157			AC
INPUT		CALL RSTON								158			AC
RSI		SFPRNT=YES								159	OLD-	157	AB
RSI	L	SFCAL								160	OLD-	158	AA
RSI	C									161	OLD-	159	AA
RSI	C-----	READ THE FORM FACTOR MATRIX FROM RSI								162	OLD-	160	AB
RSI	C									163	OLD-	161	AA
RSI	L	FFCAL								164	OLD-	162	AA
INPUT	C									165			AC
INPUT	C-----	COMBINE FORM FACTORS.								166			AC
INPUT	C									167			AC
INPUT		CALL RSTOFF								168			AC
INPUT		CALL CHDATA(0,5HCASE3,2HFF,0,0)								169			AC
INPUT	L	CNCAL								170			AC
INPUT	C									171			AC
INPUT	C-----	CALCULATE GRAY BODY MATRICES USING COMBINED FORM FACTORS.								172			AC
INPUT	C									173			AC
INPUT		CALL GBDATA(BOTH,0,CH)								174			AC
RSI	L	GBCAL								175	OLD-	167	AA
RSI	C									176	OLD-	168	AA
RSI	C-----	CALCULATE AND PUNCH RADKS WITH COMBINED NODES								177	OLD-	169	AB
RSI	C									178	OLD-	170	AB
INPUT		CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,0)								179			AC
RSI	L	RKCAL								180	OLD-	172	AA
RSI	C									181	OLD-	173	AB
RSI	C-----	DEFINE ORBIT AND VEHICLE ORIENTATION (CIRCULAR - PLANET ORIENTED)								182	OLD-	174	AB
RSI	C									183	OLD-	175	AB
RSI		CALL ORBIT2(EAR,0,60,0,0,0,100,6080,100,6080,)								184	OLD-	176	AB
RSI		CALL ORIENT(4HPLAN,1,2,3,300,270,0,)								185	OLD-	177	AB
RSI	C									186	OLD-	178	AB
PROG	C									0			
PROG	C*****	ORBIT GENERATION STARTS HERE *****								0			
RSI		CORRGEN CIRP,0,180,2,AQ								187	OLD-	179	AB
PROG	C									0			
PROG	STEP	10000								0			

PROG	TRUEAN	=	.000		0
PROG	TRUEANF	=	180.000		0
PROG	TRUEANI	=	.000		0
PROG	IAI	=	0		0
PROG	IAS	=	0		0
PROG	PLTYPE	=	6HPLSAVE		0
PROG	CALL DCOMP(0.0,0)				0
PROG	L DICAL				0
PROG	NSFFF	=	10000		0
PROG	PLTYPE	=	6HPLREAD		0
PROG	CALL AQDATA(IAI,IAS,0.0,0)				0
PROG	L AQCAL				0
PROG	STEP 10001				0
PROG	TRUEAN	=	90.000		0
PROG	CALL DCOMP(0.0,10000)				0
PROG	L DICAL				0
PROG	CALL AQDATA(IAI,IAS,0.0,0)				0
PROG	L AQCAL				0
PROG	STEP 10002				0
PROG	TRUEAN	=	180.000		0
PROG	CALL DCOMP(0.0,10000)				0
PROG	L DICAL				0
PROG	CALL AQDATA(IAI,IAS,0.0,0)				0
PROG	L AQCAL				0
PROG	STEP 10003				0
PROG	IF(SHADIN.LT.0.)			GO TO 90400	0
PROG	TRUEAN	=	SHADIN-0.1		0
PROG	IF(TRUEAN.LT.TRUEANI.OR.				0
PROG	TRUEAN.GT.TRUEANF)			GO TO 90000	0
PROG	CALL DCOMP(0.4HZERO,10000)				0
PROG	L DICAL				0
PROG	CALL AQDATA(IAI,IAS,0.0,0)				0
PROG	L AQCAL				0
PROG	90000 CONTINUE				0
PROG	STEP 10004				0
PROG	TRUEAN	=	SHADIN+0.1		0
PROG	IF(TRUEAN.LT.TRUEANI.OR.				0
PROG	TRUEAN.GT.TRUEANF)			GO TO 90100	0
PROG	CALL DCOMP(0.0,10000)				0
PROG	L DICAL				0
PROG	CALL AQDATA(IAI,IAS,0.0,0)				0
PROG	L AQCAL				0
PROG	90100 CONTINUE				0
PROG	STEP 10005				0
PROG	TRUEAN	=	SHAOUT+0.1		0
PROG	IF(TRUEAN.LT.TRUEANI.OR.				0
PROG	TRUEAN.GT.TRUEANF)			GO TO 90200	0
PROG	CALL DCOMP(0.4HZERO,10000)				0
PROG	L DICAL				0
PROG	CALL AQDATA(IAI,IAS,0.0,0)				0
PROG	L AQCAL				0
PROG	90200 CONTINUE				0
PROG	STEP 10006				0
PROG	TRUEAN	=	SHAOUT-0.1		0
PROG	IF(TRUEAN.LT.TRUEANI.OR.				0
PROG	TRUEAN.GT.TRUEANF)			GO TO 90300	0
PROG	CALL DCOMP(0.0,10000)				0

PROG	L	QICAL	.	0	
PROG		CALL AQDATA(1A1,1AS,0.0.0)	.	0	
PROG	L	AQCAL	.	0	
PROG	90300	CONTINUE	.	0	
PROG	90400	CONTINUE	.	0	
PROG		CALL QODATA(3HALL,0.0.0.0.0.0.0)	.	0	
PROG	L	QOCAL	.	0	
PROG	C		.	0	
PROG	C	***** ORBIT GENERATION ENDS HERE *****	.	0	
PROG	C		.	0	
RSI	C			180	OLD- 180 AB
RSI	C	-----THE CONFIGURATION NAME IS REDEFINED SO THE QO'S WILL USE		189	OLD- 181 AB
RSI	C	-----THE DESIRED(CASE2) CORRESPONDENCE DATA.		190	OLD- 182 AB
RSI	C			191	OLD- 183 AB
RSI		MODELN=5HCASE2		192	OLD- 184 AB
RSI		CALL QODATA(3HALL,0.0.0.0.0.0.0)		193	OLD- 185 AB
RSI	L	QOCAL		194	OLD- 186 AB
RSI		END OF DATA		195	OLD- 186 AA

MODEL = SAMPLE SAMPLE CASE 3 - FFCAL/CHCAL/GSCAL/RCCAL/ORBGEN
 PROCESSOR CORE ALLOCATION

THE FOLLOWING IS THE PROCESSOR CORE ALLOCATION FOR THOSE SEGMENTS WHICH WILL BE LOADED IN THIS EXECUTION (APPROX.) ...

OCTAL/DECIMAL

TRASYS (0) SEGMENT	121213/ 41611	
OPERATIONS DATA (NOT KNOWN AT THIS TIME).....	175000/ 64000	
INITIALIZATION SEGMENT	122300/ 42176	
FORM FACTOR SEGMENT	136100/ 48192	
SHADOW FACTOR SEGMENT	136000/ 48128	
DIRECT FLUX SEGMENT	150500/ 53568	
GRAY BODY SEGMENT	124000/ 43008	
ABSORBED Q-S SEGMENT	122500/ 42304	
-QO- SEGMENT	130600/ 45440	
RADIATION CONDUCTOR SEGMENT	125500/ 43840	
FORM FACTOR COMBINING SEGMENT	124500/ 43328	
GRAY BODY DYNAMIC COMMON	000276/ 190	
-QO- DYNAMIC COMMON	003554/ 1900	
RADIATION CONDUCTOR DYNAMIC COMMON	000574/ 380	
FORM FACTOR COMBINING DYNAMIC COMMON	000574/ 380	
GRAY BODY MINIMUM - MAXIMUM CORE	123566/ 42870 - 123716/ 42958	
-QO- MINIMUM - MAXIMUM CORE	125142/ 43618 - 130552/ 45418	
RADIATION CONDUCTOR MINIMUM - MAXIMUM CORE	125221/ 43665 - 125465/ 43829	
FORM FACTOR COMBINING MINIMUM - MAXIMUM CORE ...	124230/ 43160 - 124426/ 43286	
MINIMUM CORE NEEDED FOR PROCESSOR EXECUTION	150500/ 53568	
MAXIMUM CORE NEEDED FOR PROCESSOR EXECUTION	150500/ 53568	
AMOUNT OF CORE THAT WILL BE USED BY PROCESSOR .	150500/ 53568	

DATE 062870 TIME 205339

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION

PAGE 13

MODEL = SAMPLE
WRAP UP OF THE PRE-PROCESSOR

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORDGEN

PRE-PROCESSOR ACCOUNTING INFORMATION	CP-SEC	DYN-STORAGE
SOURCE EDITING	1.449	676
DOCUMENTATION DATA PRE-PROCESSING000	0
QUANTITIES DATA PRE-PROCESSING038	266
ARRAY DATA PRE-PROCESSING000	0
SURFACE DATA PRE-PROCESSING (PASS 1) ...	1.766	64
SURFACE DATA PRE-PROCESSING (PASS 2)660	1141
BCS DATA PRE-PROCESSING309	186
FORM FACTOR DATA PRE-PROCESSING000	0
SHADOW DATA PRE-PROCESSING000	0
FLUX DATA PRE-PROCESSING000	0
CORRESPONDENCE DATA PRE-PROCESSING268	101
OPERATIONS DATA PRE-PROCESSING	4.802	879
SUBROUTINE DATA PRE-PROCESSING368	0
SEQUENTIAL TAPE INITIALIZATION822	0
TOTAL CP TIME FOR PRE-PROCESSOR 10.392 DECIMAL SECONDS OR 000013 OCTAL SECONDS		
MINIMUM DYNAMIC STORAGE NEEDED BY PRE-PROCESSOR .. 1141 DECIMAL WORDS		
DYNAMIC STORAGE AVAILABLE TO PRE-PROCESSOR 10000 DECIMAL WORDS		

NORMAL TERMINATION BY PRE-PROCESSOR

#PHD.8LEP

#ASG.T/S RSO.,8C,RSO,92,RSO APPENDIX H, CASE 3.

#TEST TNE/1/53

#JUMP L3
INTERVENING STATEMENTS SKIPPED

#L3:FREE DATA1.

#FREE 14

NASA/MARTIN MARIETTA
THERMAL RADIATION ANALYSIS SYSTEM
UNIVAC 1110/EXEC 8

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TTTTTTTTTTTT
TTTTTTTTTTTT
TT  TTT  TT
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RRRRRRRRR
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RRRRRRRRR
RRR  RRR
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AAAAAAA
AAAAAAAAA
AAAAAAAAA
AAA  AAA
AAA  AAA
AAAAAAAAA
AAA  AAA
AAA  AAA
AAA  AAA
AAAAA  AAAA
  
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SSSSSSSSSS
SSSSSSSSSS
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YYYY  YYYY
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SSSSSSSSSS
SSSSSSSSSS
SSS  SS
SSS
SSSSSSSSSS
      SSS
SS  SSS
SSSSSSSSSS
SSSSSSSSSS
  
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TRASYS II

PROCESSOR EXECUTION

```

VERSION.MODIFICATION ... UL2E6
MODIFICATION DATE ..... 061978

DATE OF RUN ..... 062878
TIME OF RUN ..... 210523
JOB NUMBER ..... RVHH03
  
```

DATE 062670 TIME 210527

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 1

MODEL-SAMPLE CONFIG-CASE1 STEP--1
PROCESSING OPERATIONS DATA

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORRGEN

SEQUENCE	NODE	BCS	AREA	ALPH	ENISS	SURF. TYPE	ACTIVE	-----COMMENTS-----
1	1	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
2	2	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
3	3	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
4	4	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
5	11	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
6	12	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
7	13	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
8	14	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
9	5	LIDINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT LID
10	15	LIDINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER LEFT LID
11	21	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
12	22	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
13	23	BOXOUT	1.04040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
14	24	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
15	25	BOXOUT	1.04040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
16	26	LIDOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACE OF LID

NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE
BY -BUILD- (ACCESS NUMBER = 1)

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORDGEN

H-239

DATE 062870 TIME 210544

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 3

MODEL=SAMPLE CONFIG=CASE1 STEP=-1

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBCEN

SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																				
NODE		2	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR SHADOW TABLE																						CONE ANGLE
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.61	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.06	.17	.33	.44	.56	.59	.61	22.5
		.42	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.42	.64	.61	.59	.42	45.0
		.19	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.61	.42	.25	.22	.19	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

CLOCK ANGLE																				
NODE	2	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
INFRA RED SHADOW TABLE																				CONE ANGLE
	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
	.61	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.06	.17	.33	.44	.56	.59	.61 22.5
	.42	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.42	.64	.61	.59	.42 45.0
	.19	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.61	.42	.25	.22	.19 67.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00 90.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00 112.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00 135.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00 157.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00 180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBCEN

		CLOCK ANGLE																		CONE ANGLE
NODE	3	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
SOLAR SHADOW TABLE																				
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.06	.09	.03	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
	1.00	.81	.53	.31	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.33	.83	1.00	1.00	45.0
		.33	.42	.31	.25	.09	.00	.00	.00	.00	.00	.00	.00	.00	.25	.72	.50	.50	.33	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																		CONE ANGLE
NODE	3	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
INFRA RED SHADOW TABLE																				
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.06	.09	.03	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
	1.00	.81	.53	.31	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.33	.83	1.00	1.00	45.0
		.33	.42	.31	.25	.09	.00	.00	.00	.00	.00	.00	.00	.00	.25	.72	.50	.50	.33	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062070 TIME 210550

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION

PAGE 5

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CWCAL/GBCAL/RCCAL/ORBCEN

CLOCK ANGLE
NODE 4 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

SOLAR SHADOW TABLE																					CONE ANGLE
.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0	
.67	.56	.36	.39	.39	.28	.11	.00	.00	.00	.00	.00	.00	.00	.17	.33	.50	.50	.67	.67	22.5	
.00	.00	.06	.08	.00	.00	.06	.00	.00	.00	.00	.00	.00	.03	.28	.64	.50	.17	.00	.00	45.0	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

CLOCK ANGLE
NODE 4 0. 20. 40. 60. 80. 100. 120. 140. 160. 180. 200. 220. 240. 260. 280. 300. 320. 340. 360.

INFRA RED SHADOW TABLE																					CONE ANGLE
.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0	
.67	.56	.36	.39	.39	.28	.11	.00	.00	.00	.00	.00	.00	.00	.17	.33	.50	.50	.67	.67	22.5	
.00	.00	.06	.08	.00	.00	.06	.00	.00	.00	.00	.00	.00	.03	.28	.64	.50	.17	.00	.00	45.0	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN

		CLOCK ANGLE																				CONE ANGLE
NODE		11	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR SHADOW TABLE																						
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0	
		.00	.00	.00	.00	.00	1.00	.67	.17	.00	.00	.11	.33	.64	.81	.00	.00	.00	.00	.00	22.5	
		.00	.00	.00	.00	.00	1.00	.03	.00	.00	.00	.06	.19	.42	.58	.00	.00	.00	.00	.00	45.0	
		.00	.00	.00	.00	.00	.61	.17	.00	.00	.00	.08	.17	.25	.19	.00	.00	.00	.00	.00	67.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

		CLOCK ANGLE																				CONE ANGLE
NODE	11	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
INFRA RED SHADOW TABLE																						
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0	
		.00	.00	.00	.00	.00	1.00	.67	.17	.00	.00	.11	.33	.64	.81	.00	.00	.00	.00	.00	22.5	
		.00	.00	.00	.00	.00	1.00	.03	.00	.00	.00	.06	.19	.42	.58	.00	.00	.00	.00	.00	45.0	
		.00	.00	.00	.00	.00	.61	.17	.00	.00	.00	.08	.17	.25	.19	.00	.00	.00	.00	.00	67.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

DATE 062870 TIME 210557

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION

PAGE 7

MODEL=SAMPLE CONFIG=CASE1 STEP=-1

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORDGEN

SHADOW FACTOR GENERATOR LINK

C9

		CLOCK ANGLE																					
		12	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
SOLAR SHADOW TABLE		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	CONE	ANGLE
		.61	.59	.56	.44	.33	.17	.06	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.61	22.5	
		.42	.59	.61	.64	.42	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.42	45.0	
		.19	.22	.25	.42	.61	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.19	67.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

		CLOCK ANGLE																					
		12	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
INFRA RED SHADOW TABLE		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	CONE	ANGLE
		.61	.59	.56	.44	.33	.17	.06	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.61	22.5	
		.42	.59	.61	.64	.42	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.42	45.0	
		.19	.22	.25	.42	.61	.17	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.19	67.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

DATE 062878 TIME 210558

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE

8

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

		CLOCK ANGLE																			
NODE 13		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR SHADOW TABLE																				CONE ANGLE	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.03	.08	.08	.00	22.5
	1.00	1.00	.83	.33	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.31	.53	.81	1.00	45.0
	.33	.50	.50	.72	.25	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.25	.31	.42	.33	67.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE 13		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED SHADOW TABLE																				CONE ANGLE	
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.03	.08	.08	.00	22.5
	1.00	1.00	.83	.33	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.17	.31	.53	.81	1.00	45.0
	.33	.50	.50	.72	.25	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.08	.25	.31	.42	.33	67.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CHCAL/GDCAL/RCCAL/ORBGEN

		CLOCK ANGLE																				
NODE		14	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE	
SHADOW	TABLE	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	ANGLE
		.67	.67	.50	.50	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.28	.39	.39	.36	.56	.67	22.5
		.00	.00	.17	.50	.64	.28	.03	.00	.00	.00	.00	.00	.00	.06	.00	.00	.08	.06	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			
NODE	14	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED SHADOW TABLE																					CONE ANGLE
		.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33	.0
		.67	.67	.50	.50	.33	.17	.00	.00	.00	.00	.00	.00	.11	.28	.39	.39	.36	.56	.67	22.5
		.00	.00	.17	.50	.64	.28	.03	.00	.00	.00	.00	.00	.06	.00	.00	.08	.06	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062878 TIME 210606

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 10

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

		CLOCK ANGLE																			CONE ANGLE
NODE	5	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR SHADOW TABLE																					
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0
		1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
		.67	.56	.67	.67	.72	.72	.00	.00	.00	.00	.00	.00	.00	.14	.14	.33	.50	.50	.67	112.5
		.33	.39	.33	.31	.33	.33	.31	.22	.11	.00	.00	.00	.00	.00	.00	.00	.17	.33	.33	135.0
		.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

		CLOCK ANGLE																			CONE ANGLE
NODE	5	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED SHADOW TABLE																					
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0
		1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
		.67	.56	.67	.67	.72	.72	.00	.00	.00	.00	.00	.00	.00	.14	.14	.33	.50	.50	.67	112.5
		.33	.39	.33	.31	.33	.33	.31	.22	.11	.00	.00	.00	.00	.00	.00	.00	.17	.33	.33	135.0
		.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	157.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0

DATE 062878 TIME 210610 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 11

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

		CLOCK ANGLE																		CONE ANGLE	
NODE 15		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.		360.
SOLAR		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
SHADOW TABLE		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0
	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5
	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
	.67	.50	.50	.33	.14	.14	.00	.00	.00	.00	.00	.00	.00	.72	.72	.67	.67	.56	.67	112.5	
	.33	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.22	.31	.33	.33	.31	.33	.39	.33	135.0	
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	157.5	
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

		CLOCK ANGLE																		CONE ANGLE	
NODE 15		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.		360.
INFRA RED		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
SHADOW TABLE		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0
	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	67.5
	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
	.67	.50	.50	.33	.14	.14	.00	.00	.00	.00	.00	.00	.00	.72	.72	.67	.67	.56	.67	112.5	
	.33	.33	.17	.00	.00	.00	.00	.00	.00	.00	.11	.22	.31	.33	.33	.31	.33	.39	.33	135.0	
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.03	.08	.11	.14	.14	.11	.08	.03	.00	157.5	
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	180.0	

DATE 062978 TIME 210613 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 12

MODEL=SAWPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN

		CLOCK ANGLE																			
NODE	21	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

		CLOCK ANGLE																			
NODE	21	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW TABLE																					ANGLE
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	67.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

DATE 062070 TIME 210615

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN

SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																			
NODE	22	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW TABLE																					ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	22.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	45.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

		CLOCK ANGLE																			
NODE	22	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW TABLE																					ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	22.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	45.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	67.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

		CLOCK ANGLE																		CONE ANGLE
NODE	23	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
SOLAR SHADOW TABLE																				
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	45.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	67.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

		CLOCK ANGLE																		CONE ANGLE
NODE	23	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.
INFRA RED SHADOW TABLE																				
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	22.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	45.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	67.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	90.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	112.5
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	135.0
		1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

DATE 062878 TIME 210626

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1

SAMPLE CASE 3 - FFCAL/CHCAL/GSCAL/RCCAL/ORBGEN

SHADOW FACTOR GENERATOR LINK

		CLOCK ANGLE																			
NODE 24		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
SOLAR																					CONE
SHADOW	TABLE																				ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

		CLOCK ANGLE																			
NODE 24		0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.	
INFRA RED																					CONE
SHADOW	TABLE																				ANGLE
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	22.5
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	45.0
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	67.5
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	90.0
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	112.5
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	135.0
		.00	.00	.00	.00	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	157.5
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
SHADOW FACTOR GENERATOR LINK

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

		CLOCK ANGLE																				CONE ANGLE
NODE	25	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
SOLAR SHADOW TABLE																						
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	22.5	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	67.5	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	90.0	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	112.5	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	135.0	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	157.5	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0	

		CLOCK ANGLE																				CONE ANGLE
NODE	25	0.	20.	40.	60.	80.	100.	120.	140.	160.	180.	200.	220.	240.	260.	280.	300.	320.	340.	360.		
INFRA RED SHADOW TABLE																						
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	22.5	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	45.0	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	67.5	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	90.0	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	112.5	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	135.0	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.00	.00	.00	.00	.00	.00	.00	.00	1.00	157.5	
	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	180.0	

SOLAR SHADON TABLE

**CONE
ANGLE**

[illegible]

INFRA RED
SHADOW TABLE

**CONE
ANGLE**

[illegible]

SHADOW FACTORS FOR CONFIGURATION CASE1 HAVE BEEN STORED ON RSO.
LAST RECORD WRITTEN = 52

TOTAL TIME FOR SHADOW FACTOR TABLES 9.1

DATE 062878 TIME 210637

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORDGEN

FORM FACTORS AND COMBINED FORM FACTORS - USER INPUT AND DEFAULT PARAMETERS

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
FFACC	.0500	.0500	ORIENTATION ACCURACY PARAMETER	N/A
FFACCS	.1000	.1000	SHADOWING ACCURACY PARAMETER	N/A
FFHIN	.1-05	1.0E-06	PARAMETER TO ELIMINATE SMALL FORM FACTORS	N/A
FFNOSH	SHAD	SHAD	OVER RIDE SHADOWING PARAMETER	(SHAD,NOSH)
+FFPNCH	NO	NO	PARAMETER TO PUNCH FORM FACTORS	(YES,NO)
FFPRNT	YES	YES	FLAG FOR COMPREHENSIVE FF AND CH PRINT	(YES,NO,FF,CH,RP)
FFRATL	15.0	15.0	RATIO FOR USING SUB-NODE TECHNIQUE	N/A
FFCHB	NO	CORR	FLAG FOR COMBINING FORM FACTORS	(YES,NO,AUTO,CORR)

+ -FFPNCH WILL DEFAULT TO -YES- ON CALCULATED VALUES IF THE -RSO- FILE IS NOT SPECIFIED IN THE OPTIONS DATA BLOCK

RESTARTING - FFCAL - DATA FOR CONFIGURATION- CASE1 -FROM UNIT - 14

DATE 062078 TIME 210630

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/DRBGEN

SEQUENCE	NODE	AREA	ALPH	EMISS
1	1	1.00000	.900	.900
2	2	1.00000	.900	.900
3	3	1.00000	.900	.900
4	4	1.00000	.900	.900
5	11	1.00000	.900	.900
6	12	1.00000	.900	.900
7	13	1.00000	.900	.900
8	14	1.00000	.900	.900
9	5	1.00000	.900	.900
10	15	1.00000	.900	.900
11	21	2.06040	.200	.900
12	22	2.06040	.200	.900
13	23	1.04040	.200	.900
14	24	2.06040	.200	.900
15	25	1.04040	.200	.900
16	26	2.06040	.200	.900

NUMBER OF NODES = 16 NUMBER OF SURFACES = 16

(1 -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) M/SHAD	FIR(J,I) M/SHAD	FSOL(I,J) M/SHAD	FSOL(J,I) M/SHAD	FF(I,J) M/SHAD	SHAD:IR FACTOR	SHAD:SOL FACTOR	CP TIME (SEC)	NEI	NEJ	
1	2	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
1	3	RSI	.201522	.201522	.201522	.201522	.201522	1.000000	1.000000	.000	0	0	UN
1	4	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
1	12	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
1	13	RSI	.086058	.086058	.086058	.086058	.086058	1.000000	1.000000	.000	0	0	UN
1	14	RSI	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	.000	0	0	UN
1	5	RSI	.137203	.137203	.137203	.137203	.137203	1.000000	1.000000	.000	0	0	UN
1	15	RSI	.056006	.056006	.056006	.056006	.056006	1.000000	1.000000	.000	0	0	UN
1	FFSUM = .9690		ROW CP TIME = .137										
FORM FACTOR RESTART (RSI) RECORD = 56													
2	3	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN

DATE 062078 TIME 210639

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

(*) -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(*) -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(*) -INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(*) -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ	
2	4	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
2	11	RSI	.032922	.032922	.032922	.032922	.032922	.000000	.000000	.000	0	0	UN
2	12	RSI	.068832	.068832	.068832	.068832	.068832	1.000000	1.000000	.000	0	0	UN
2	13	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
2	14	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
2	5	RSI	.096343	.096343	.096343	.096343	.096343	1.000000	1.000000	.000	0	0	UN
2	15	RSI	.034262	.034262	.034262	.034262	.034262	1.000000	1.000000	.000	0	0	UN
2	FFSUM = .9203		ROW CP TIME = .157										
	FORM FACTOR RESTART (RSO) RECORD = 57												
3	4	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
3	11	RSI	.086059	.086059	.086059	.086059	.086059	.000000	.000000	.000	0	0	UN
3	12	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
3	14	RSI	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	.000	0	0	UN
3	5	RSI	.050426	.050426	.050426	.050426	.050426	1.000000	1.000000	.000	0	0	UN
3	15	RSI	.011660	.011660	.011660	.011660	.011660	1.000000	1.000000	.000	0	0	UN
3	FFSUM = .8378		ROW CP TIME = .080										
	FORM FACTOR RESTART (RSO) RECORD = 58												
4	11	RSI	.040501	.040501	.040501	.040501	.040501	.000000	.000000	.000	0	0	UN
4	12	RSI	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.000	0	0	UN
4	13	RSI	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	.000	0	0	UN
4	5	RSI	.107799	.107799	.107799	.107799	.107799	1.000000	1.000000	.000	0	0	UN
4	15	RSI	.056851	.056851	.056851	.056851	.056851	1.000000	1.000000	.000	0	0	UN
4	FFSUM = .9007		ROW CP TIME = .066										
	FORM FACTOR RESTART (RSO) RECORD = 59												
11	12	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0	UN
11	13	RSI	.201522	.201522	.201522	.201522	.201522	1.000000	1.000000	.000	0	0	UN

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBGEM
FORM FACTOR CALCULATION LINK.

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
11	14	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0 UN
11	5	RSI	.056006	.056006	.056006	.056006	.056006	1.000000	1.000000	.000	0	0 UN
11	15	RSI	.137203	.137203	.137203	.137203	.137203	1.000000	1.000000	.000	0	0 UN
11	FFSUM = .9690 ROW CP TIME = .119 FORM FACTOR RESTART (RSI) RECORD = 60											
12	13	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0 UN
12	14	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0 UN
12	5	RSI	.034262	.034262	.034262	.034262	.034262	1.000000	1.000000	.000	0	0 UN
12	15	RSI	.096343	.096343	.096343	.096343	.096343	1.000000	1.000000	.000	0	0 UN
12	FFSUM = .9203 ROW CP TIME = .052 FORM FACTOR RESTART (RSI) RECORD = 61											
13	14	RSI	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	.000	0	0 UN
13	5	RSI	.011660	.011660	.011660	.011660	.011660	1.000000	1.000000	.000	0	0 UN
13	15	RSI	.050426	.050426	.050426	.050426	.050426	1.000000	1.000000	.000	0	0 UN
13	FFSUM = .8378 ROW CP TIME = .047 FORM FACTOR RESTART (RSI) RECORD = 62											
14	5	RSI	.056051	.056051	.056051	.056051	.056051	1.000000	1.000000	.000	0	0 UN
14	15	RSI	.107790	.107790	.107790	.107790	.107790	1.000000	1.000000	.000	0	0 UN
14	FFSUM = .9007 ROW CP TIME = .029 FORM FACTOR RESTART (RSI) RECORD = 63											

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR CALCULATION LINK. SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBGEN

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RS1, RT1, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) M/SHAD	FIR(J,I) M/SHAD	FSOL(I,J) M/SHAD	FSOL(J,I) M/SHAD	FF(I,J) M/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
5		FFSUM = .5505 FORM FACTOR RESTART (RS0) RECORD =										
15		FFSUM = .5505 FORM FACTOR RESTART (RS0) RECORD =										
21		FFSUM = .0000 FORM FACTOR RESTART (RS0) RECORD =										
22		FFSUM = .0000 FORM FACTOR RESTART (RS0) RECORD =										
23		FFSUM = .0000 FORM FACTOR RESTART (RS0) RECORD =										
24		FFSUM = .0000 FORM FACTOR RESTART (RS0) RECORD =										

DATE 062070 TIME 210643 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 23

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORDGEN
FORM FACTOR CALCULATION LINK.

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION NODE BECAUES OF RSI, RTI, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) H/SHAD	FIR(J,I) H/SHAD	FSOL(I,J) H/SHAD	FSOL(J,I) H/SHAD	FF(I,J) HO/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
25		FFSUM = .0000										
		FORM FACTOR RESTART (RSO) RECORD =										
26		FFSUM = .0000										
		FORM FACTOR RESTART (RSO) RECORD =										

FF FORM FACTORS FOR CONFIGURATION CASE1 HAVE BEEN STORED ON RSO.
LAST RESTART RECORD WRITTEN = 71

DATE 062878 TIME 210644 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 24

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBGEN
FORM FACTOR CALCULATION LINK.

SUMMARY OF FORM FACTOR SUMS FOR ALL NODES

NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM
1- .9690	2- .9203	3- .8378	4- .9007	11- .9690	12- .9203
13- .8378	14- .9007	5- .5505	15- .5505	21- .0000	22- .0000
23- .0000	24- .0000	25- .0000	26- .0000		

TOTAL TIME FOR FORM FACTOR SEGMENT 1.517

TOTAL TIME SINCE START OF RUN 77.437

DATE 062870 TIME 210549

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR COMBINING LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/OBCAL/RCCAL/ORBGEM

NODE	AREA	ALPH	EMISS	TRANS(UV)	TRANS(IR)	SPECULAR REFL(UV)	SPECULAR REFL(IR)
1	4.06040	.545+00	.900+00	.000	.000	.000	.000
2	2.04040	.543+00	.900+00	.000	.000	.000	.000
3	4.06040	.545+00	.900+00	.000	.000	.000	.000
4	4.06040	.545+00	.900+00	.000	.000	.000	.000
12	2.04040	.543+00	.900+00	.000	.000	.000	.000
5	4.06040	.545+00	.900+00	.000	.000	.000	.000

NUMBER OF NODES AFTER COMBINING = 6

DATE 062070 TIME 210650

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR COMBINING LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORIGEN

NODE I	NODE J	COMPUTATION	FE(I,J) H/SHAD	FE(J,I) H/SHAD	FA(I,J) H/SHAD
1	2	COMB	.059102	.117772	.059102
1	3	COMB	.141651	.141651	.141651
1	4	COMB	.122096	.122096	.122096
1	12	COMB	.059102	.117772	.059102
1	5	COMB	.095167	.095167	.095167
1	FF SUM =		.4773		
2	3	COMB	.117772	.059102	.117772
2	4	COMB	.117772	.059102	.117772
2	12	COMB	.033734	.033734	.033734
2	5	COMB	.064010	.032166	.064010
2	FF SUM =		.4511		
3	4	COMB	.122096	.122096	.122096
3	12	COMB	.059102	.117772	.059102
3	5	COMB	.030501	.030501	.030501
3	FF SUM =		.4127		
4	12	COMB	.059102	.117772	.059102
4	5	COMB	.081100	.081100	.081100
4	FF SUM =		.4437		
12	5	COMB	.064010	.032166	.064010
12	FF SUM =		.4511		
5	FF SUM =		.2712		

DATE 062970 TIME 210651 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 27

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
FORM FACTOR COMBINING LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORDGEN

COMBINED FORM FACTOR SUMS FROM NODE 1

NODE 1 -	FFSUM NODE 1 -	FFSUM NODE 1 -	FFSUM NODE 1 -	FFSUM NODE 1 -	FFSUM NODE 1 -	FFSUM
1- .4772783	2- .4510588	3- .4126925	4- .4436561	12- .4510588	5- .2711795	

COMBINED NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE
BY THE FORM FACTOR COMBINING LINK. (ACCESS NUMBER = 2)

.....

CH FORM FACTORS FOR CONFIGURATION CASE1 HAVE BEEN STORED ON RSO.
LAST RESTART RECORD WRITTEN = 91

.....

DATE 062870 TIME 210653 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 28

MODEL=SAMPLE CONFIG=CASE1 STEP=-1 SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBCEN
GRAY BODIES COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
GBWBND	BOTH	BOTH	HAVEBAND DEFINITION PARAMETER	(2HIR,3HSOL,4HBOTH)

IR GRAY BODIES FOR CONFIGURATION CASE1 HAVE BEEN COMPUTED AND STORED ON RSO.
LAST RESTART RECORD WRITTEN = 99

SOL GRAY BODIES FOR CONFIGURATION CASE1 HAVE BEEN COMPUTED AND STORED ON RSO.
LAST RESTART RECORD WRITTEN = 107

TOTAL TIME TO COMPUTE GRAY BODIES .49

DATE 062878 TIME 210656

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 29

MODEL=SAHLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBGEN

VARIABLE NAME	CURRENT VALUE	DEFAULT	RADIATION CONDUCTORS DEFINITION	OPTIONS
RKPNCH	PUN	NO	PUNCH/NO PUNCH PARAMETER FOR RADKS	(YES,NO)
RKMIN	.0001	0.0001	PARAMETER TO ELIMINATE SMALL RADK S	N/A
IRKCN	1	1	INITIAL RADIATION CONDUCTOR ID NUMBER	N/A
RKSP	SPACE	NO	MNEMONIC FLAG FOR COMPUTATION OF RADKS TO SPACE	(SPACE,NO)
IRKNSP	999	32767	SPACE NODE ID NUMBER	N/A
SIGMA	.17-08	1.713E-9	STEFAN-BOLTZMANN CONSTANT	N/A
RKAMPF	1.00	1.0	AREA MULTIPLYING FACTOR	N/A
RKTAPE	NO	NO	PARAMETER TO OUTPUT TO BCD TAPE	(TAPE,NO)
RFRAC	.7+00	0.7	SIGNIFICANT RADIATION FRACTION	(0. TO 1.)
RTOL	.990	0.99	DECIMAL FRACTION OF LAST RADK SAVED	N/A
KERN	0	0	EFFECTIVE RADIATION NODE (ERN) NUMBER	N/A

DATE 062070 TIME 210657

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 30

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN

SPECIAL RADIATION NODES

NONE

MESS SPECIAL NODES

PRIMARY SECONDARY

NONE

DATE 062870 TIME 210657

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION

PAGE 31

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEM

RADIATION CONDUCTOR (RADKS) CARDS

AREA UNITS = INPUT UNITS * AMPF, WHERE AMPF = 1.00000

PUNCHED AND/OR BCD0U RADKS -	-	1.	1.	2.	.34560-09\$
PUNCHED AND/OR BCD0U RADKS -	-	2.	1.	3.	.81703-09\$
PUNCHED AND/OR BCD0U RADKS -	-	3.	1.	4.	.71086-09\$
PUNCHED AND/OR BCD0U RADKS -	-	4.	1.	12.	.34560-09\$
PUNCHED AND/OR BCD0U RADKS -	-	5.	1.	5.	.54917-09\$
PUNCHED AND/OR BCD0U RADKS -	-	6.	2.	3.	.34439-09\$
PUNCHED AND/OR BCD0U RADKS -	-	7.	2.	4.	.34467-09\$
PUNCHED AND/OR BCD0U RADKS -	-	8.	2.	12.	.10226-08\$
PUNCHED AND/OR BCD0U RADKS -	-	9.	2.	5.	.18906-09\$
PUNCHED AND/OR BCD0U RADKS -	-	10.	3.	4.	.70787-09\$
PUNCHED AND/OR BCD0U RADKS -	-	11.	3.	12.	.34439-09\$
PUNCHED AND/OR BCD0U RADKS -	-	12.	3.	5.	.19031-09\$
PUNCHED AND/OR BCD0U RADKS -	-	13.	4.	12.	.34467-09\$
PUNCHED AND/OR BCD0U RADKS -	-	14.	4.	5.	.47849-09\$
PUNCHED AND/OR BCD0U RADKS -	-	15.	12.	5.	.18906-09\$
PUNCHED AND/OR BCD0U RADKS -	-	16.	1.	999.	.34580-08\$
PUNCHED AND/OR BCD0U RADKS -	-	17.	2.	999.	.18126-08\$
PUNCHED AND/OR BCD0U RADKS -	-	18.	3.	999.	.38270-08\$
PUNCHED AND/OR BCD0U RADKS -	-	19.	4.	999.	.36521-08\$
PUNCHED AND/OR BCD0U RADKS -	-	20.	12.	999.	.18126-08\$
PUNCHED AND/OR BCD0U RADKS -	-	21.	5.	999.	.46598-08\$

DATE 062070 TIME 210703 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 32

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GSCAL/RCCAL/ORGEN

CONSERVATION CHECKS
RADIATION SUNS FOR EACH NODE BEFORE RKMIN SCREENING

1 - .10000+01	2 - .10000+01	3 - .10000+01	4 - .10000+01	12 - .10000+01	5 - .10000+01
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DATE 062878 TIME 210703 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 33

MODEL=SAMPLE CONFIG=CASE1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK. SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

CONSERVATION CHECKS
RADIATION SUNS FOR EACH NODE AFTER RKHM SCREENING

1 - .10000+01 2 - .10000+01 3 - .10000+01 4 - .10000+01 12 - .10000+01 5 - .10000+01

TOTAL TIME TO COMPUTE AND CONDENSE RADKS = .51

DATE 062878 TIME 210707

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 34

MODEL=SAMPLE CONFIG=CASE1 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD.NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
0	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.50800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.50800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX, IROTY, IROTZ		1 2 3	
.300+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.300+02	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCH POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062878 TIME 210708

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 35

MODEL=SAMPLE CONFIG=CASE1 STEP=10000

SAMPLE CASE 3 - PFCAL/CHCAL/GBCAL/RCCAL/ORSGEN

DIRECT IRRADIATION CALCULATION LINK.

+++++ NSTEP NO = 10000

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES	-	.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	HDS
.20900+08	PLANET RADIUS	PRAO		.75073+02	PLANET SS EMISS POWER	HSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062878 TIME 210712 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 36

MODEL=SANPLE CONFIG=CASE1 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GCCAL/RCCAL/ORDGEN

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10000 TRUE ANOMALY = .00000 TIME = .00000
++++ IN THE SUN +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	SFTAPE	.001	9	0
2	.94028+02	.18576+03	.5062	CALC	.183	81	5
3	.00000	.10725+03	.0000	CALC	.294	64	0
4	.18576+03	.37152+03	.5000	SFTAPE	.352	81	0
11	.00000	.00000	.0000	SFTAPE	.384	9	0
12	.00000	.00000	.0000	SFTAPE	.447	9	0
13	.10855+02	.10725+03	.0938	CALC	.566	64	6
14	.10664+03	.37152+03	.2870	SFTAPE	.628	81	0
5	.00000	.00000	.0000	SFTAPE	.677	9	0
15	.00000	.00000	.0000	SFTAPE	.725	9	0
21	.00000	.00000	.0000	SFTAPE	.774	8	0
22	.10725+03	.10725+03	1.0000	CALC	.948	66	10
23	.18576+03	.18576+03	1.0000	CALC	1.114	81	6
24	.00000	.00000	.0000	SFTAPE	1.160	8	0
25	.00000	.00000	.0000	SFTAPE	1.207	9	0
26	.18687+03	.18687+03	1.0000	CALC	1.411	78	10

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DIC

TOTAL ELAPSED TIME IN PROBLEM = 81.593 SECONDS

DATE 062878 TIME 210710 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 37

MODEL=SAMPLE CONFIG=CASE1 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORDGEN

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10000 TRUE ANOMALY = .00000 TIME = .00000
++++ IN THE SUN +++++

NODE NUMBER	COMPUT	---DIRECT ALBEDO	INCID. FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS--- ALBEDO PLAN	CP TIME (SECONDS)	---ELEMENTS--- PLAN SURF	SHAD SURF
1	SFTAPE	.000	.000	.391+02	.268+02	.000 .000	.000	66 9	9
2	SFTAPE	.000	.000	.400+02	.264+02	.000 .000	.289	66 9	9
3	SFTAPE	.000	.000	.402+02	.268+02	.000 .000	.523	61 9	9
4	SFTAPE	.000	.000	.000	.000	.000 .000	.623	52 9	9
11	SFTAPE	.000	.000	.391+02	.268+02	.000 .000	.848	66 9	9
12	SFTAPE	.000	.000	.382+02	.264+02	.000 .000	1.082	66 9	9
13	SFTAPE	.000	.000	.402+02	.268+02	.000 .000	1.313	61 9	9
14	SFTAPE	.000	.000	.000	.000	.000 .000	1.413	52 9	9
5	CALC	.231+02	.155+02	.834+02	.559+02	.277 .277	2.508	133 16	9
15	CALC	.233+02	.154+02	.834+02	.559+02	.279 .277	3.490	133 16	9
21	CALC	.110+03	.742+02	.110+03	.742+02	1.000 1.000	7.728	112 18	10
22	CALC	.402+02	.268+02	.402+02	.268+02	1.000 1.000	8.618	61 10	10
23	CALC	.400+02	.264+02	.400+02	.264+02	1.000 1.000	9.343	66 9	10
24	CALC	.391+02	.268+02	.391+02	.268+02	1.000 1.000	10.266	66 10	10
25	CALC	.382+02	.264+02	.382+02	.264+02	1.000 1.000	10.856	66 9	10
26	CALC	.659+01	.457+01	.659+01	.457+01	1.000 1.000	11.137	52 2	10

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RTI. THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DIC

TOTAL ELAPSED TIME IN PROBLEM = 92.987 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 120

DATE 062070 TIME 210017

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 30

MODEL=SAMPLE CONFIG=CASE1 STEP=10000
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/OROGEN

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSOS	10000	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10000	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10000	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10000

TOTAL TIME TO COMPUTE ABSORBED Q .14

MODEL=SAFPLE CONFIG=CASE1 STEP=10001 SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN
DIRECT IRRADIATION CALCULATION LINK.

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
90.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX, IROTY, IROTZ		1 2 3	
.000	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.900+02	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCH POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062870 TIME 210020 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 40
 MODEL=SAMPLE CONFIG=CASE1 STEP=10001 SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN
 DIRECT IRRADIATION CALCULATION LINK.

***** NSTEP NO = 10001

**** COMPUTED OR INPUT ORBIT DATA ****

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
50.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

**** PLANET --EARTH -- DATA ****

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	WSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062978 TIME 210021 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 41

MODEL=SAMPLE CONFIG=CASE1 STEP=10001
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORRGEN

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10001 TRUE ANOMALY = 90.00000 TIME = .36701
++++ IN THE SUN +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	SFTAPE	.001	9	0
2	.00000	.00000	.0000	SFTAPE	.065	9	0
3	.00000	.42900+03	.0000	SFTAPE	.104	81	0
4	.00000	.00000	.0000	SFTAPE	.139	9	0
11	.00000	.00000	.0000	SFTAPE	.172	9	0
12	.00000	.00000	.0000	SFTAPE	.206	9	0
13	.00000	.42900+03	.0000	SFTAPE	.250	81	0
14	.00000	.00000	.0000	SFTAPE	.285	9	0
5	.30335+03	.30335+03	1.0000	SFTAPE	.329	81	0
15	.30335+03	.30335+03	1.0000	SFTAPE	.375	81	0
21	.00000	.00000	.0000	SFTAPE	.409	8	0
22	.42900+03	.42900+03	1.0000	SFTAPE	.457	78	0
23	.00000	.00000	.0000	SFTAPE	.492	9	0
24	.00000	.00000	.0000	SFTAPE	.526	8	0
25	.00000	.00000	.0000	SFTAPE	.561	9	0
26	.00000	.00000	.0000	SFTAPE	.596	8	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DIC

TOTAL ELAPSED TIME IN PROBLEM = 94.280 SECONDS

MODEL=SAMPLE CONFIG=CASE1 STEP=10001
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORDGEN

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10001 TRUE ANOMALY = 90.00000 TIME = .36701
++++ IN THE SUN +++++

MODE NUMBER	COMPUT	---DIRECT ALBEDO	INCID. FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS--- ALBEDO PLAN	CP TIME (SECONDS)	---ELEMENTS--- PLAN SURF	SHAD SURF
1	SFTAPE	.000	.000	.000	.000	.000 .000	.001	66 9	9
2	SFTAPE	.000	.000	.638+00	.000	.000 .000	.235	66 9	9
3	SFTAPE	.000	.000	.206+01	.000	.000 .000	.432	61 9	9
4	SFTAPE	.000	.000	.000	.000	.000 .000	.520	52 9	9
11	SFTAPE	.000	.000	.000	.000	.000 .000	.714	66 9	9
12	SFTAPE	.000	.000	.634+00	.000	.000 .000	.913	66 9	9
13	SFTAPE	.000	.000	.206+01	.000	.000 .000	1.101	61 9	9
14	SFTAPE	.000	.000	.000	.000	.000 .000	1.187	52 9	9
5	CALC	.126+01	.155+02	.247+01	.000	.509 .000	2.034	133 16	9
15	CALC	.125+01	.154+02	.247+01	.000	.504 .000	2.802	133 16	9
21	CALC	.143+01	.742+02	.143+01	.000	1.000 .000	6.112	112 18	10
22	CALC	.206+01	.268+02	.206+01	.000	1.000 .000	6.818	61 10	10
23	CALC	.638+00	.264+02	.638+00	.000	1.000 .000	7.378	66 9	10
24	CALC	.000	.268+02	.000	.000	.000 .000	8.110	66 10	10
25	CALC	.634+00	.264+02	.634+00	.000	1.000 .000	8.670	66 9	10
26	CALC	.000	.457+01	.000	.000	.000 .000	8.938	52 2	10

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICO

TOTAL ELAPSED TIME IN PROBLEM = 103.420 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 139

DATE 062070 TIME 210040 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 43

MODEL=SAMPLE CONFIG=CASE1 STEP=10001

SAMPLE CASE 3 - FFCAL/CMCAL/GDCAL/RCCAL/ORBCEN

ABSORBED Q COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT VALUE	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10001	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10001	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10001	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10001

TOTAL TIME TO COMPUTE ABSORBED Q .15

DATE 062070 TIME 210043

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 44

MODEL=SANPLE CONFIG=CASE1 STEP=10002
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS ++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
100.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA ++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA ++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX, IROTY, IROTZ		1 2 3	
.300+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.150+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA ++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE - CCH POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062878 TIME 210843 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 45

MODEL=SAHPLE CONFIG=CASE1 STEP=10002 SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORDGEN
DIRECT IRRADIATION CALCULATION LINK.

+++++ NSTEP NO = 10002

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGHAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	WSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAY CONSTANT	GRAY		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062878 TIME 210844

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 46

MODEL=SAHLE CONFIG=CASE1 STEP=10002

SAMPLE CASE 3 - FFCAL/CHCAL/GDCAL/RCCAL/ORRGEN

DIRECT IRRADIATION CALCULATION LINK.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10002 TRUE ANOMALY = 100.00000 TIME = .73402
 ++++ IN THE SHADE ++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADON FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	+++++	.001	0	0
2	.00000	.00000	.0000	+++++	.053	0	0
3	.00000	.00000	.0000	+++++	.082	0	0
4	.00000	.00000	.0000	+++++	.106	0	0
11	.00000	.00000	.0000	+++++	.129	0	0
12	.00000	.00000	.0000	+++++	.156	0	0
13	.00000	.00000	.0000	+++++	.181	0	0
14	.00000	.00000	.0000	+++++	.208	0	0
5	.00000	.00000	.0000	+++++	.229	0	0
15	.00000	.00000	.0000	+++++	.258	0	0
21	.00000	.00000	.0000	+++++	.284	0	0
22	.00000	.00000	.0000	+++++	.308	0	0
23	.00000	.00000	.0000	+++++	.331	0	0
24	.00000	.00000	.0000	+++++	.356	0	0
25	.00000	.00000	.0000	+++++	.385	0	0
26	.00000	.00000	.0000	+++++	.411	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DIC

TOTAL ELAPSED TIME IN PROBLEM = 104.550 SECONDS

DATE 062878 TIME 210846 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 47

MODEL=SAMPLE CONFIG=CASE1 STEP=10002
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10002 TRUE ANOMALY = 180.00000 TIME = .73402
++++ IN THE SHADE +++++

NODE NUMBER	COMPUT	---DIRECT INCID. FLUX-- ALBEDO	PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS-- ALBEDO	PLAN	CP TIME (SECONDS)	---ELEMENTS-- PLAN	SURF	SHAD SURF
1	+++++	.000	.000	.000	.000	.000	.000	.000	0	0	0
2	+++++	.000	.000	.000	.000	.000	.000	.059	0	0	0
3	+++++	.000	.000	.000	.000	.000	.000	.086	0	0	0
4	+++++	.000	.000	.000	.000	.000	.000	.114	0	0	0
11	+++++	.000	.000	.000	.000	.000	.000	.138	0	0	0
12	+++++	.000	.000	.000	.000	.000	.000	.164	0	0	0
13	+++++	.000	.000	.000	.000	.000	.000	.191	0	0	0
14	+++++	.000	.000	.000	.000	.000	.000	.216	0	0	0
5	+++++	.000	.155+02	.000	.000	.000	.000	.239	0	0	0
15	+++++	.000	.154+02	.000	.000	.000	.000	.266	0	0	0
21	+++++	.000	.742+02	.000	.000	.000	.000	.292	0	0	0
22	+++++	.000	.268+02	.000	.000	.000	.000	.317	0	0	0
23	+++++	.000	.264+02	.000	.000	.000	.000	.341	0	0	0
24	+++++	.000	.268+02	.000	.000	.000	.000	.370	0	0	0
25	+++++	.000	.264+02	.000	.000	.000	.000	.401	0	0	0
26	+++++	.000	.457+01	.000	.000	.000	.000	.427	0	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 105.017 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 158

DATE 062878 TIME 210949 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 40

MODEL=SAMPLE CONFIG=CASE1 STEP=10002
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEM

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10002	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10002	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10002	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10002

TOTAL TIME TO COMPUTE ABSORBED Q .16

DATE 062070 TIME 210052

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 49

MODEL=SAMPLE CONFIG=CASE1 STEP=10003
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
105.720	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TINEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60000+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60000+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX,IROTY,IROTZ		1 2 3	
.359+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.104+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCH POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062970 TIME 210053 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 9 VERSION PAGE 50
 MODEL=SAFPLE CONFIG=CASE1 STEP=10003 SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBGEN
 DIRECT IRRADIATION CALCULATION LINK.

+++++ NSTEP NO = 10003

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	WSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062070 TIME 210054 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC'D VERSION PAGE 51

MODEL=SAMPLE CONFIG=CASE1 STEP=10003
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBGEN

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10003 TRUE ANOMALY = 105.71977 TIME = .43111
++++ IN THE SUN +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	SFTAPE	.001	9	0
2	.00000	.69478+01	.0000	SFTAPE	.068	9	0
3	.00000	.41697+03	.0000	SFTAPE	.109	01	0
4	.00000	.00000	.0000	SFTAPE	.146	9	0
11	.00000	.00000	.0000	SFTAPE	.180	9	0
12	.00000	.00000	.0000	SFTAPE	.216	9	0
13	.00000	.41697+03	.0000	SFTAPE	.258	01	0
14	.00000	.00000	.0000	SFTAPE	.298	9	0
5	.28468+03	.36602+03	.7778	CALC	.418	01	5
15	.28468+03	.36602+03	.7778	CALC	.542	01	5
21	.10066+03	.10066+03	1.0000	CALC	.670	55	10
22	.41696+03	.41696+03	1.0000	CALC	.834	78	10
23	.69478+01	.69478+01	1.0000	CALC	.884	9	5
24	.00000	.00000	.0000	SFTAPE	.919	9	0
25	.00000	.00000	.0000	SFTAPE	.955	9	0
26	.00000	.00000	.0000	SFTAPE	.990	9	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RTI, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DI

TOTAL ELAPSED TIME IN PROBLEM = 106.779 SECONDS

DATE 062978 TIME 210858

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 52

MODEL=SAMPLE CONFIG=CASE1 STEP=10003
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GSCAL/RCCAL/ORBGEN

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10003 TRUE ANOMALY = 105.71977 TIME = .43111
++++ IN THE SUN +++++

NODE NUMBER	COMPUT	---DIRECT INCID. ALBEDO	FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX-- PLANETARY	---SHADOW FACTORS-- ALBEDO	PLAN	CP TIME (SECONDS)	---ELEMENTS-- PLAN	SURF	SHAD SURF
1	+++++	.000	.000	.000	.000	.000	.000	.001	0	0	0
2	+++++	.000	.000	.000	.000	.000	.000	.059	0	0	0
3	+++++	.000	.000	.000	.000	.000	.000	.087	0	0	0
4	+++++	.000	.000	.000	.000	.000	.000	.115	0	0	0
11	+++++	.000	.000	.000	.000	.000	.000	.140	0	0	0
12	+++++	.000	.000	.000	.000	.000	.000	.169	0	0	0
13	+++++	.000	.000	.000	.000	.000	.000	.194	0	0	0
14	+++++	.000	.000	.000	.000	.000	.000	.222	0	0	0
5	+++++	.000	.155+02	.000	.000	.000	.000	.247	0	0	0
15	+++++	.000	.154+02	.000	.000	.000	.000	.276	0	0	0
21	+++++	.000	.742+02	.000	.000	.000	.000	.311	0	0	0
22	+++++	.000	.269+02	.000	.000	.000	.000	.341	0	0	0
23	+++++	.000	.264+02	.000	.000	.000	.000	.367	0	0	0
24	+++++	.000	.269+02	.000	.000	.000	.000	.402	0	0	0
25	+++++	.000	.264+02	.000	.000	.000	.000	.430	0	0	0
26	+++++	.000	.457+01	.000	.000	.000	.000	.457	0	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RTI, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DIC

TOTAL ELAPSED TIME IN PROBLEM = 107.279 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 177

DATE 062878 TIME 210900

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 53

MODEL=SAMPLE CONFIG=CASE1 STEP=10003
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 3 - FFCAL/CNCAL/OBCAL/RCCAL/ORDGEN

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10003	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10003	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSOP	10003	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED.Q STORED IN STEP 10003

TOTAL TIME TO COMPUTE ABSORBED Q .15

MODEL=SAMPLE CONFIG=CASE1 STEP=10004
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GEAL/RCCAL/ORDGEN

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS ++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
105.920	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA ++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA ++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX,IROTY,IROTZ		1 2 3	
.359+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.104+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA ++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCM=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCM POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMESP

DATE 062870 TIME 210903 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 55

MODEL=SAMPLE CONFIG=CASE1 STEP=10004 SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBOEN
DIRECT IRRADIATION CALCULATION LINK.

***** NSTEP NO * 10004

**** COMPUTED OR INPUT ORBIT DATA ****

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

**** PLANET --EARTH -- DATA ****

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	MDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	MSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAY CONSTANT	GRAY		.42900+03	SOLAR CONSTANT AT PSD	SOL

DIRECT INCIDENT FLUXES CALCULATED USING SHADOW FACTORS

DATE 062070 TIME 210904

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE1 STEP=10004
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GDCAL/RCCAL/ORBGEN

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10004 TRUE ANOMALY = 105.91977 TIME = .43193
++++ IN THE SHADE +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	+++++	.001	0	0
2	.00000	.00000	.0000	+++++	.056	0	0
3	.00000	.00000	.0000	+++++	.085	0	0
4	.00000	.00000	.0000	+++++	.110	0	0
11	.00000	.00000	.0000	+++++	.138	0	0
12	.00000	.00000	.0000	+++++	.164	0	0
13	.00000	.00000	.0000	+++++	.190	0	0
14	.00000	.00000	.0000	+++++	.220	0	0
5	.00000	.00000	.0000	+++++	.244	0	0
15	.00000	.00000	.0000	+++++	.270	0	0
21	.00000	.00000	.0000	+++++	.297	0	0
22	.00000	.00000	.0000	+++++	.322	0	0
23	.00000	.00000	.0000	+++++	.347	0	0
24	.00000	.00000	.0000	+++++	.372	0	0
25	.00000	.00000	.0000	+++++	.399	0	0
26	.00000	.00000	.0000	+++++	.429	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DIC

TOTAL ELAPSED TIME IN PROBLEM = 100.482 SECONDS

DATE 062070 TIME 210905 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 57

MODEL=SAHPLE CONFIG=CASE1 STEP=10004
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBOEN

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10004 TRUE ANOMALY = 105.91977 TIME = .43193
**** IN THE SHADE ****

MODE NUMBER	COMPUT	---DIRECT INCID. ALBEDO	FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADON FACTORS--- ALBEDO PLAN	CP TIME (SECONDS)	---ELEMENTS--- PLAN SURF	SHAD SURF
1	+++++	.000	.000	.000	.000	.000 .000	.001	0 0	0
2	+++++	.000	.000	.000	.000	.000 .000	.058	0 0	0
3	+++++	.000	.000	.000	.000	.000 .000	.087	0 0	0
4	+++++	.000	.000	.000	.000	.000 .000	.115	0 0	0
11	+++++	.000	.000	.000	.000	.000 .000	.138	0 0	0
12	+++++	.000	.000	.000	.000	.000 .000	.166	0 0	0
13	+++++	.000	.000	.000	.000	.000 .000	.194	0 0	0
14	+++++	.000	.000	.000	.000	.000 .000	.223	0 0	0
5	+++++	.000	.155+02	.000	.000	.000 .000	.246	0 0	0
15	+++++	.000	.154+02	.000	.000	.000 .000	.272	0 0	0
21	+++++	.000	.742+02	.000	.000	.000 .000	.298	0 0	0
22	+++++	.000	.268+02	.000	.000	.000 .000	.326	0 0	0
23	+++++	.000	.264+02	.000	.000	.000 .000	.352	0 0	0
24	+++++	.000	.268+02	.000	.000	.000 .000	.380	0 0	0
25	+++++	.000	.264+02	.000	.000	.000 .000	.409	0 0	0
26	+++++	.000	.457+01	.000	.000	.000 .000	.437	0 0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DIC

TOTAL ELAPSED TIME IN PROBLEM = 109.961 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 196

DATE 062070 TIME 210509 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 50

MODEL=SAMPLE CONFIG=CASE1 STEP=10004 SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORDGEN
ABSORBED Q COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10004	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10004	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10004	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

ABSORBED Q STORED IN STEP 10004

TOTAL TIME TO COMPUTE ABSORBED Q .20

DATE 062878 TIME 210911 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 59

MODEL=SAMPLE CONFIG=CASE1 STEP=10006 , SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORIGEN
 ABSORBED Q OUTPUT COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
IQOTHE	1	1	TIME ARRAY ID NUMBER FLUX TABLES START AT IQOTHE + 1	N/A
QOTAPE	NO	2HNO	PARAMETER TO OUTPUT TO BCD TAPE	(4HTAPE,2HNO)
QOPNCH	NO	2HNO	PUNCH/NO PUNCH PARAMETER FOR OUTPUT	(3HPUN,2HNO)
QOAMPF	1.0000	1.0	AREA MULTIPLYING FACTOR	N/A
QOFMPF	1.0000	1.0	FLUX MULTIPLYING FACTOR	N/A
QOTHPF	1.0000	1.0	TIME MULTIPLYING FACTOR	N/A
QOTYPE	BOTH	NONE	PARAMETER TO DETERMINE TYPE OF OUTPUT	(3HTAB,2HAV,4HBOTH)
IQOARY	ALL	NONE	STEP NO. ARRAY DIRECTIVE	(3HALL,ARRAY NAME)

DATE 062070 TIME 210912

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 60

MODEL=SAMPLE CONFIG=CASE1 STEP=10006
ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBCEN

ABSORBED HEAT RATE TABLES PUNCHED

Q = INPUT * RHPF WHERE RHPF = .10000+01
TIME = INPUT * THPF WHERE THPF = .10000+01
AREA IS ON SUBROUTINE CALL CARDS

1\$ TIME ARRAY
.000 .367+00. .431+00. .432+00. .734+00
END\$
2\$ HEAT RATE ARRAY
.268+03. .560+03. .551+03. .532+02. .532+02
END\$
3\$ HEAT RATE ARRAY
.122+03. .484+02. .507+02. .264+02. .264+02
END\$
4\$ HEAT RATE ARRAY
.151+03. .958+02. .101+03. .529+02. .529+02
END\$
5\$ HEAT RATE ARRAY
.464+03. .188+03. .299+03. .140+03. .140+03
END\$
6\$ HEAT RATE ARRAY
.177+03. .484+02. .546+02. .264+02. .264+02
END\$
7\$ HEAT RATE ARRAY
.311+03. .396+03. .378+03. .384+02. .384+02
END\$

DATE 062878 TIME 210913

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE

61

MODEL=SAMPLE CONFIG=CASE1 STEP=10006

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBGEM

ABSORBED & OUTPUT COMPUTATION LINK.

DAIINC SUBROUTINE CALL CARDS

AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000*01

DAIINC(1.46792175E 0.TIHEM,A1	.A2	.1.00000000E 0.01)\$
DAIINC(1.46792175E 0.TIHEM,A1	.A3	.1.00000000E 0.02)\$
DAIINC(1.46792175E 0.TIHEM,A1	.A4	.1.00000000E 0.03)\$
DAIINC(1.46792175E 0.TIHEM,A1	.A5	.1.00000000E 0.04)\$
DAIINC(1.46792175E 0.TIHEM,A1	.A6	.1.00000000E 0.012)\$
DAIINC(1.46792175E 0.TIHEM,A1	.A7	.1.00000000E 0.05)\$

DATE 062070 TIME 210913 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 62

MODEL=SAMPLE CONFIG=CASE1 STEP=10006
ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORSGEN

AVERAGE ORBITAL HEATING RATE AND AREA CARDS PUNCHED

VALUES ARE RATE = INPUT (UNITS) * RHPF WHERE RHPF = .10000+01
VALUES ARE AREA = INPUT (UNITS) * AHPF WHERE AHPF = .10000+01

Q1 =2.77859285E 2
Q2 =5.79530262E 1
Q3 =9.21390224E 1
Q4 =2.41824245E 2
Q12 =7.16434819E 1
Q5 =2.26533908E 2

TOTAL TIME TO COMPUTE ABSORBED Q OUT .39

DATE 062878 TIME 210913

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 63

MODEL=SAHPLE CONFIG=CASE2 STEP=10006
ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORBCEN

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
IQOTME	1	1	TIME ARRAY ID NUMBER FLUX TABLES START AT IQOTME + 1	N/A
QOTAPE	NO	2HNO	PARAMETER TO OUTPUT TO BCD TAPE	(4HTAPE,2HNO)
QOPNCH	NO	2HNO	PUNCH/NO PUNCH PARAMETER FOR OUTPUT	(3HPUN,2HNO)
QOAHMF	1.0000	1.0	AREA MULTIPLYING FACTOR	N/A
QOFMPF	1.0000	1.0	FLUX MULTIPLYING FACTOR	N/A
QOTHPF	1.0000	1.0	TIME MULTIPLYING FACTOR	N/A
QOTYPE	BOTH	NONE	PARAMETER TO DETERMINE TYPE OF OUTPUT	(3HTAB,2HAV,4HBOTH)
IQOARY	ALL	NONE	STEP NO. ARRAY DIRECTIVE	(3HALL,ARRAY NAME)

DATE 062078 TIME 210915

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION PAGE 64

MODEL=SAMPLE CONFIG=CASE2 STEP=10008
ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 3 - FFCAL/CHCAL/GBCAL/RCCAL/ORBGEN

ABSORBED HEAT RATE TABLES PUNCHED

Q = INPUT * RHPF WHERE RHPF = .10000+01
TIME = INPUT * THPF WHERE THPF = .10000+01
AREA IS ON SUBROUTINE CALL CARDS

18 TIME ARRAY
.000 , .367+00, .431+00, .432+00, .734+00
END\$
28 HEAT RATE ARRAY
.268+03, .560+03, .551+03, .532+02, .532+02
END\$
38 HEAT RATE ARRAY
.122+03, .484+02, .507+02, .264+02, .264+02
END\$
48 HEAT RATE ARRAY
.151+03, .956+02, .101+03, .529+02, .529+02
END\$
58 HEAT RATE ARRAY
.464+03, .188+03, .299+03, .140+03, .140+03
END\$
68 HEAT RATE ARRAY
.177+03, .484+02, .546+02, .264+02, .264+02
END\$
78 HEAT RATE ARRAY
.311+03, .396+03, .378+03, .384+02, .384+02
END\$

RRRRRRRRRR	VV	VV	PP	PP	MM	MM	0000	222222
RRRRRRRRRR	VV	VV	PPPP	PPPP	MM	MM	00000000	2222222222
RR	VV	VV	PPPPPP	PPPPPP	MM	MM	000	222
RR	VV	VV	PPPPPPPP	PPPPPPPP	MM	MM	000	222
RRRRRRRRRRRR	VV	VV	PPPPPPPPPP	PPPPPPPPPP	MM	MM	00	222
RRRRRRRRRRRR	VV	VV	PPPPPPPPPP	PPPPPPPPPP	MM	MM	00	222
RR	VV	VV	PPPP	PPPP	MM	MM	00	222
RR	VVVV	VVVV	PPPP	PPPP	MM	MM	000	222
RR	VVVV	VVVV	PPPP	PPPP	MM	MM	000	222
RR	VV	VV	PPPP	PPPP	MM	MM	00000000	222222222222
RR	VV	VV	PPPP	PPPP	MM	MM	0000	222222222222

00000000	00000000	XX	XX	PP	PP	MM	MM	0000
00000000	00000000	XX	XX	PPPP	PPPP	MM	MM	00000000
00	00	XX	XX	PPPPPP	PPPPPP	MM	MM	000
00	00	XX	XX	PPPPPPPP	PPPPPPPP	MM	MM	000
00	00	XXXX	XX	PPPPPPPP	PPPPPPPP	MM	MM	00
00	00	XX	XX	PPPPPPPP	PPPPPPPP	MM	MM	00
00	00	XXXX	XX	PPPP	PPPP	MM	MM	00
00	00	XX	XX	PPPP	PPPP	MM	MM	000
00	00	XX	XX	PPPP	PPPP	MM	MM	000
00000000	00000000	XX	XX	PPPP	PPPP	MM	MM	00000000
00000000	00000000	XX	XX	PPPP	PPPP	MM	MM	0000

0000	666666	222222	TTTTTTTTTTTT	TTTTTTTTTTTT	888888
00000000	6666666666	2222222222	TTTTTTTTTTTT	TTTTTTTTTTTT	88888888
000	666	222	TTT	TTT	88
000	66	222	TTT	TTT	88
00	66	222	TTT	TTT	88
00	66 666666	222	TTT	TTT	888888
00	6666666666	222	TTT	TTT	88888888
00	66	222	TTT	TTT	888
000	66	222	TTT	TTT	88
000	66	222	TTT	TTT	888
00000000	6666666666	222222222222	TTT	TTT	8888888888
0000	666666	222222222222	TTT	TTT	88888888

DATE 062678 TIME 210915

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 65

MODEL=SAMPLE CONFIG=CASE2 STEP=10000

SAMPLE CASE 3 - FFCAL/CNCAL/GBCAL/RCCAL/ORBGEN

ABSORBED Q OUTPUT COMPUTATION LINK.

DA11HC SUBROUTINE CALL CARDS

AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000*01

DA11HC(1.46792175E 0.TIMEH.A1	.A2	.1.00000000E 0.01	1\$
DA11HC(1.46792175E 0.TIMEH.A1	.A3	.1.00000000E 0.02	1\$
DA11HC(1.46792175E 0.TIMEH.A1	.A4	.1.00000000E 0.03	1\$
DA11HC(1.46792175E 0.TIMEH.A1	.A5	.1.00000000E 0.04	1\$
DA11HC(1.46792175E 0.TIMEH.A1	.A6	.1.00000000E 0.012	1\$
DA11HC(1.46792175E 0.TIMEH.A1	.A7	.1.00000000E 0.05	1\$

DATE 062070 TIME 210915 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 66

MODEL=SAMPLE CONFIG=CASE2 STEP=10006
ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 3 - FFCAL/CMCAL/GBCAL/RCCAL/ORDGEN

AVERAGE ORBITAL HEATING RATE AND AREA CARDS PUNCHED

VALUES ARE RATE = INPUT (UNITS) * RMPF WHERE RMPF = .10000+01
VALUES ARE AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000+01

Q1	=2.77859295E	2
Q2	=5.79538262E	1
Q3	=9.21390224E	1
Q4	=2.41824245E	2
Q12	=7.16434819E	1
Q5	=2.26533908E	2

TOTAL TIME TO COMPUTE ABSORBED Q OUT .39

NORMAL TERMINATION BY PROCESSOR

QPHD,PLED

QBRKPT PRINTS

SAMPLE CASE 4

SAMPLE CASE 4

SED,R VOGT0.CASE4
 FILE IN FIELD 1 DISABLED--ACCEPTED
 FILE IN FIELD 1 IN USE BY ANOTHER RUN
 READ-ONLY MODE
 CASE UPPER ASSUMED
 ED 14.02-06/20-20:44-(0.)
 EDIT

NO DECK VOGT

1:0RUN,R/R RVNH04.3240-F261-C.E53-N03711.05.150
 10:0ADD E53-TRASYS*TRASYS.STARTM
 11:0ASG,T RSI..0C,X04061
 12:0SETC 0100
 13:0ADD PREPRO
 14:HEADER OPTIONS DATA
 15:TITLE SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL
 16:C-----FORM TWO ENCLOSURES INSIDE THE BOX BY THE USE OF "MESS" NODES.
 17:C-----CLOSE THE BOX LID AND CALCULATE FORM FACTORS, GRAY BODY FACTORS,
 18:C-----AND RADK'S FOR EACH OF THE ENCLOSURES UTILIZING AN "ERN" NODE,
 19:C-----IN ENCLOSURE 2.
 20:C
 21: MODEL = SAMPLE
 22: RSI = RSTSAH
 23: RSD = RSTSAH4
 24:HEADER EDIT DATA
 25:0.1
 26:HEADER ARRAY DATA
 27: IPRIM1 = 101
 28: ISEC1 = 111
 29: IPRIM2 = 111
 30: ISEC2 = 101
 31:HEADER SURFACE DATA
 32:01,56
 33:BCS LIDINL
 34:01,121
 35:BCS LIDINL,0.,0.,1.,0.,-45.,0.
 36:01,171
 37:C
 38:C-----SPECIFY CALCULATION OF FORM FACTORS FOR ENCLOSURE 1 BY
 39:C-----THE USE OF UNIT-SPHERE LOGIC. (NO SHADOWING)
 40:C
 41:FIG ENCL1
 42:UNIT
 43:C
 44:C-----SPECIFY CALCULATION OF FORM FACTORS FOR ENCLOSURE 2 BY
 45:C-----THE USE OF UNIT SPHERE LOGIC. (NO SHADOWING)
 46:C
 47:FIG ENCL2
 48:UNIT
 49:01,193
 50:C
 51:C-----FINISHED WITH RSI, RELEASE TAPE DRIVE.
 52:C
 53: CALL RSTOFF
 54:0.194,222
 55:C
 56:C-----CLOSE BOX LID
 57:C
 58: CALL CHGBLK(LIDINR,0.,0.,1.,1,2,3,0.,0.,0.)


```

59:      CALL CHGBLK(LIDINL,0..0..1..1,2,3,0..0..0.)
60:C
61:C-----BUILD ENCL1 CONFIGURATION
62:C
63:BUILD   ENCL1,BOXINR,LIDINR,MESSR
64:C
65:C-----CALCULATE FORM FACTORS FOR ENCLOSURE 1
66:C
67:      CALL RSTOFF
68:L      FFCAL
69:C
70:C-----CHANGE EMITTANCES OF SURFACES FOR ENCL1
71:C
72:      CALL MODPR(1..9..5)
73:      CALL MODPR(2..9..5)
74:      CALL MODPR(3..9..5)
75:      CALL MODPR(4..9..5)
76:      CALL MODPR(5..9..5)
77:C
78:C-----PRINTOUT NODE DATA.
79:C
80:      CALL NOODAT
81:C
82:C-----CALCULATE GRAY BODY FACTORS FOR ENCLOSURE 1
83:C
84:      CALL GBDATA(1R,0,FF)
85:L      GBCAL
86:C
87:C-----CALCULATE RADK'S FOR ENCLOSURE 1
88:C
89:      CALL RCADATA(0,0,0,0,0,0,0,0,0,0,0,0,1PRIM1,1SEC1)
90:L      RCCAL
91:C
92:C-----BUILD ENCL2 CONFIGURATION
93:C
94:BUILD   ENCL2,BOXINL,LIDINL,MESSL
95:C
96:C-----CALCULATE FORM FACTORS FOR ENCLOSURE 2
97:C
98:L      FFCAL
99:C
100:C-----CHANGE EMITTANCES OF SURFACES FOR ENCL2
101:C
102:      CALL MODPR(11..9..5)
103:      CALL MODPR(12..9..5)
104:      CALL MODPR(13..9..5)
105:      CALL MODPR(14..9..5)
106:      CALL MODPR(15..9..5)
107:C
108:C-----PRINTOUT NODE DATA.
109:C
110:      CALL NOODAT
111:C
112:C-----CALCULATE GRAY BODY FACTORS FOR ENCLOSURE 2
113:C
114:      CALL GBDATA(1R,5HENCL2,FF)
115:L      GBCAL

```

116:C -
117:C-----CALCULATE RADK'S FOR ENCLOSURE 2 UTILIZING AN #ERN# NODE
118:C
119: CALL RCDATA(0.0.0.0.0.0.0.0.0.0.5,1.,555,1PRIM2,1SEC2)
120:L RCCAL
121:OPND,BLEP
122:QASG,T/S RSO..BC.RSO.92.RSO APPENDIX H, CASE 4.
123:QADD PROCSS
131:QFIN
NO CORRECTIONS APPLIED.

#FREE TPFS.

#ASG,T TPFS.,F4/D/TRK/400

QED ES3-TRASYS*TRASYS.PREPROH.TPFS.PREPRO
CASE UPPER ASSUMED
ED 14.02-06/20-20:44-(0,)
EDIT
LINES:57 FIELDATA

0ED ES3-TRASYS*TRASYS.PROCSSH,TPFS.PROCSS
CASE UPPER ASSUMED
ED 14.02-06/28-20:44-(1.)
EDIT
LINES:103 FIELDATA

0ASG,T RS1.,8C,X04061

0SETC 0100

0SETC,1

0ASG,AQ ES3-TRASYS*LIBRYN.
FAC WARNING 040200004000

0ASG,T 1.,F4/0/TRK/600

0ASG,T 2.,F4/0/TRK/600

0ASG,T 3.,F4/0/TRK/600

0ASG,T DIR.,F17/0/POS/5

0ASG,T FFR.,F17/0/POS/9

0ASG,T GBIRR.,F17/0/POS/5

0ASG,T RIO.,F17/0/POS/9

0ASG,T SQNTL.,F17/0/TRK/10

0ASG.T PLSR..F17/0/TRK/320

0ASG.T TQR..F17/0/TRK/320

0USE 0.R10

0USE 14.RS1

0USE 16.SQNTL

0USE 21.FFR

0USE 22.DIR

0USE 23.GB1RR

0USE 25.PLSR

0USE 26.TQR

0XQT ES3-TRASYS*LIBRYN.CHECK

0TEST TNE/1/S3

0JUMP L1
INTERVENING STATEMENTS SKIPPED

0L1:ASG.T R102..F17/0/POS/9

0ASG,T RIOS..F17/0/POS/20

0ASG,T DATA1..F17/0/POS/9

0ASG,T CMPL..F17/0/TRK/20

0ASG,T INFO

0ASG,T MAP.

0ASG,T MASS.F17/0/POS/20

0TEST TE/1/56
INTERVENING STATEMENTS SKIPPED

0ASG,T MASS1.F/0/POS/20

0USE 15,MASS1

0COPY.G 14.15
FURPUR 27R1 RL72-9 06/29/78 20:44:55
ES3-NO*MASS(0) COPIED ON 06/22/78 AT 20:30:00
3 BLOCKS COPIED.
EOF ENCOUNTERED ON INPUT TAPE

0ASG,T MASS2.F/0/POS/20

0MOVE RS1.7
FURPUR 27R1 RL72-9 06/29/78 20:46:08

0USE 4,MASS2

0XQT ES3-TRASYS*LIBRYN.LOAD
END OF FILE AFTER PHYSICAL RECORD 187

0L15:FREE 14

0USE 4,DATA1

0USE 9,R105

0USE 10,R102

0USE 11,INFO

0USE 12,CHERG

0USE 13,EMERG

0USE 14,MASS1

0USE 15,MASS

0USE 20,CHPL

0USE 27,MAP

0ASQ,AQ ES3-TRASYS*COMPLRN.
FAC WARNING 040200004000

0DATA.1 INFO.
DATA Y7 RL76-S 06/28-20:47:36
END DATA. IMAGE COUNT: 20

0XQT ES3-TRASYS°COMPLRN.ABS :

NASA/MARTIN MARIETTA
THERMAL RADIATION ANALYSIS SYSTEM
UNIVAC 1110/EXEC 0

TTTTTTTTTTTT
TTTTTTTTTTTT
TT TTT TT
TTT
TTT
TTT
TTT
TTT
TTTTTT

RRRRRRRR
RRRRRRRR
RRR RRR
RRR RRR
RRRRRRRR
RRR RRR
RRR RRR
RRR RRR
RRR RRR

AAAAAA
AAAAAA
AAAAAAAA
AAA AAA
AAA AAA
AAAAAAAA
AAA AAA
AAA AAA
AAA AAA
AAAAA AAAA

SSSSSSSS
SSSSSSSSSS
SSS SS
SSS
SSSSSSSS
SSS
SS SSS
SSSSSSSSSS
SSSSSSSSSS

TRASYS II

YYYY YYYY
YYY YYY
YYY YYY
YYY YYY
YYYY
YYY
YYY
YYYYYY

SSSSSSSS
SSSSSSSSSS
SSS SS
SSS
SSSSSSSS
SSS
SS SSS
SSSSSSSSSS
SSSSSSSSSS

PRE-PROCESSOR EXECUTION

VERSION.MODIFICATION ... UC2E3
MODIFICATION DATE 052678
DATE OF RUN 062878
TIME OF RUN 205211
JOB NUMBER RVMH04

DATE 062670 TIME 205212 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 1

MODEL = N/A

OPTION AND TITLE DATA BLOCKS

CARD ORIGIN 12345670 1 2345670 2 2345670 3 2345670 4 2345670 5 2345670 6 2345670 7 2345670 8 EDIT NO. OLD EDIT NO. LAB

INPUT HEADER OPTIONS DATA
INPUT TITLE SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL
INPUT C-----FORM TWO ENCLOSURES INSIDE THE BOX BY THE USE OF #MESS# NODES.
INPUT C-----CLOSE THE BOX LID AND CALCULATE FORM FACTORS, GRAY BODY FACTORS.
INPUT C-----AND RADK'S FOR EACH OF THE ENCLOSURES UTILIZING AN #ERN# NODE.
INPUT C-----IN ENCLOSURE 2.
INPUT C
INPUT MODEL = SAMPLE
INPUT RSI = RSTSAH
INPUT RSD = RSTSAH4

DATE 062670 TIME 205212

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION

PAGE 2

MODEL = SAMPLE

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

TRASYS INFORMATION TO USER

```
*****  
*  
*   A T T E N T I O N   T R A S Y S   U S E R S   *  
*  
*****
```

THIS SECTION OF THE TRASYS PRINTOUT WAS DEvised TO
INFORM THE TRASYS USERS OF THE STATUS OF THE TRASYS
PROGRAM WITHOUT HAVING TO PRINTOUT ALL THE STATUS
INFORMATION ON EVERY RUN. TO OBTAIN ADDITIONAL
INFORMATION ON HOW TO USE THIS SECTION OF THE TRASYS
PRINTOUT, PLACE A (INFO=INFO) IN THE OPTIONS DATA
BLOCK.

FOR TRASYS ASSISTANCE AND/OR POSSIBLE TRASYS PROGRAM
PROBLEMS, PLEASE CONTACT BOB VOGT AT JSC-2326.

NEWRL 08/29/77 DOCUMENTATION ADDITION

THE TRASYS -N- VERSION HAS BEEN UPDATED TO THE UC2E2
AND UL2E4 LEVEL.

SEE LATEST USERS MANUAL FOR INFORMATION ON USER-
CALLED SUBROUTINE ARGUMENT CHANGES AND NEW
CAPABILITIES.

END OF TRASYS INFORMATION FILE

DATE 062878 TIME 205213

INTERNAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC @ VERSION

PAGE 3

MODEL = SAMPLE
MODEL HISTORY

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

MODEL NAME SAMPLE

MODEL TITLE SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

MOD LABEL	RUN JOB NUMBER	RUN DATA	RUN TIME	RSI TAPE	RSO TAPE	RTI TAPE	RTD TAPE	CHRG TAPE	EMRG TAPE	BCDOU TAPE	TRAJ TAPE	USER1 TAPE	USER2 TAPE
AA	RVMH01	062278	202625										
AB	RVMH04	062878	205212	RSTSAM	RSTSAM								

MODEL = SAMPLE SOURCE DATA EDIT DIRECTIVES SAMPLE CASE 4 - FFCAL/GDCAL/RCCAL

CARD ORGIN 12345670 1 2345670 2 2345670 3 2345670 4 2345670 5 2345670 6 2345670 7 2345670 8 EDIT NO. OLD EDIT NO. LABEL

****	HEADER EDIT DATA			
D	*D,1		OLD-	1 AA
1	HEADER SURFACE DATA			AB
1	HEADER ARRAY DATA	1		AB
1	IPRIM1 = 101	2		AB
1	ISEC1 = 111	3		AB
1	IPRIM2 = 111	4		AB
1	ISEC2 = 101	5		AB
1	HEADER SURFACE DATA	6		AB
****	*I,56			
1	BCS LIDINL	62		AB
****	*I,121			
1	BCS LIDINL,0..0..1..0..-45..0.	128		AB
****	*I,171			
1	C	179		AB
1	C-----SPECIFY CALCULATION OF FORM FACTORS FOR ENCLOSURE 1 BY	180		AB
1	C-----THE USE OF UNIT-SPHERE LOGIC. (NO SHADOWING)	181		AB
1	C	182		AB
1	FIG ENCL1	183		AB
1	UNIT	184		AB
1	C	185		AB
1	C-----SPECIFY CALCULATION OF FORM FACTORS FOR ENCLOSURE 2 BY	186		AB
1	C-----THE USE OF UNIT SPHERE LOGIC. (NO SHADOWING)	187		AB
1	C	188		AB
1	FIG ENCL2	189		AB
1	UNIT	190		AB
****	*I,193			
1	C	213		AB
1	C-----FINISHED WITH RS1. RELEASE TAPE DRIVE.	214		AB
1	C	215		AB
1	CALL RSTOFF	216		AB
****	*D,194,222			
D	C		OLD-	194 AA
D	C-----BUILD THE CASE 1 CONFIGURATION		OLD-	195 AA
D	C		OLD-	196 AA
D	BUILD CASE1,BOXINR,BOXINL,LIDINR,BOXOUT,LIDOUT		OLD-	197 AA
D	C		OLD-	198 AA
D	C-----PLOT THE CASE 1 CONFIGURATION INDICATING THE ACTIVE		OLD-	199 AA
D	C-----SIDES OF THE NODES.		OLD-	200 AA
D	C		OLD-	201 AA
D	CALL NDATA(0,0,0,YES,0)		OLD-	202 AA
D	L NPLT		OLD-	203 AA
D	C		OLD-	204 AA
D	C-----CALCULATE SHADOW FACTOR TABLES FOR SUBSEQUENT USE		OLD-	205 AA
D	C-----SAMPLE CASE 2 IN THE CALCULATION OF DIRECT FLUXES.		OLD-	206 AA
D	C		OLD-	207 AA
D	L SFCAL		OLD-	208 AA

DATE 062878 TIME 205217 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 5

MODEL = SAMPLE SOURCE DATA EDIT DIRECTIVES SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CARD	ORIGIN	12345678 1	2345678 2	2345678 3	2345678 4	2345678 5	2345678 6	2345678 7	2345678 8	EDIT NO.	OLD EDIT NO.	LABEL
D	C										OLD-	209 AA
D	C	----	CALCULATE THE FORM FACTOR MATRIX.								OLD-	210 AA
D	C										OLD-	211 AA
D	L		FFCAL								OLD-	212 AA
D	C										OLD-	213 AA
D	C	----	CALCULATE THE GRAY BODY MATRIX.								OLD-	214 AA
D	C										OLD-	215 AA
D			CALL GBDATA(BOTH,0,FF)								OLD-	216 AA
D	L		GBCAL								OLD-	217 AA
D	C										OLD-	218 AA
D	C	----	CALCULATE AND PUNCH RADIATION CONDUCTORS.								OLD-	219 AA
D	C										OLD-	220 AA
D			CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,0)								OLD-	221 AA
D	L		RKCAL								OLD-	222 AA
I	C									217		AB
I	C	----	CLOSE BOX LID							218		AB
I	C									219		AB
I			CALL CHGBLK(LIDINR,0,0,1,1,2,3,0,0,0,0)							220		AB
I			CALL CHGBLK(LIDINL,0,0,1,1,2,3,0,0,0,0)							221		AB
I	C									222		AB
I	C	----	BUILD ENCL1 CONFIGURATION							223		AB
I	C									224		AB
I	BUILD		ENCL1,BOXINR,LIDINR,MESSR							225		AB
I	C									226		AB
I	C	----	CALCULATE FORM FACTORS FOR ENCLOSURE 1							227		AB
I	C									228		AB
I			CALL RSTOFF							229		AB
I	L		FFCAL							230		AB
I	C									231		AB
I	C	----	CHANGE EMITTANCES OF SURFACES FOR ENCL1							232		AB
I	C									233		AB
I			CALL MODPR(1,.9,.5)							234		AB
I			CALL MODPR(2,.9,.5)							235		AB
I			CALL MODPR(3,.9,.5)							236		AB
I			CALL MODPR(4,.9,.5)							237		AB
I			CALL MODPR(5,.9,.5)							238		AB
I	C									239		AB
I	C	----	PRINTOUT NODE DATA.							240		AB
I	C									241		AB
I			CALL NODDAT							242		AB
I	C									243		AB
I	C	----	CALCULATE GRAY BODY FACTORS FOR ENCLOSURE 1							244		AB
I	C									245		AB
I			CALL GBDATA(IR,0,FF)							246		AB
I	L		GBCAL							247		AB
I	C									248		AB
I	C	----	CALCULATE RADK'S FOR ENCLOSURE 1							249		AB

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DATE 062878 TIME 205220 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 7

MODEL = SAMPLE
ARRAY DATA INPUT BLOCK
SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

INPUT	HEADER ARRAY DATA			1	AD
INPUT	IPRIH1	= 101		2	AD
INPUT	ISEC1	= 111		3	AD
INPUT	IPRIH2	= 111		4	AD
INPUT	ISEC2	= 101		5	AD

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CARD ORIGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

INPUT	HEADER SURFACE DATA	6		AB
RSI	C	7	OLD-	2 AA
RSI	C-----THIS SURFACE DATA BLOCK IS USED IN SAMPLE CASES 1 THROUGH 5	8	OLD-	3 AA
RSI	C-----WITH VARIOUS PORTIONS OF IT BEING ACTIVATED FOR THE DIFFERENT	9	OLD-	4 AA
RSI	C-----CASES.	10	OLD-	5 AA
RSI	C	11	OLD-	6 AA
RSI	BCS BOXINR	12	OLD-	7 AA
RSI	S SURFN = 1	13	OLD-	8 AA
RSI	TYPE = RECT	14	OLD-	9 AA
RSI	ACTIVE = BOTTOM	15	OLD-	10 AA
RSI	PROP = 0.9,0.9	16	OLD-	11 AA
RSI	P1 = 1.0, 0.0, 1.0	17	OLD-	12 AA
RSI	P2 = 1.0, 0.0, 0.0	18	OLD-	13 AA
RSI	P3 = 1.0, 1.0, 0.0	19	OLD-	14 AA
RSI	COM = * INNER RIGHT FRONT *	20	OLD-	15 AA
RSI	S SURFN = 2	21	OLD-	16 AA
RSI	TYPE = RECT	22	OLD-	17 AA
RSI	ACTIVE = BOTTOM	23	OLD-	18 AA
RSI	PROP = 0.9,0.9	24	OLD-	19 AA
RSI	P1 = 1.0, 1.0, 1.0	25	OLD-	20 AA
RSI	P2 = 1.0, 1.0, 0.0	26	OLD-	21 AA
RSI	P3 = 0.0, 1.0, 0.0	27	OLD-	22 AA
RSI	COM = * INNER RIGHT SIDE *	28	OLD-	23 AA
RSI	S SURFN = 3	29	OLD-	24 AA
RSI	TYPE = RECT	30	OLD-	25 AA
RSI	ACTIVE = TOP	31	OLD-	26 AA
RSI	PROP = 0.9,0.9	32	OLD-	27 AA
RSI	P1 = 0.0, 0.0, 1.0	33	OLD-	28 AA
RSI	P2 = 0.0, 0.0, 0.0	34	OLD-	29 AA
RSI	P3 = 0.0, 1.0, 0.0	35	OLD-	30 AA
RSI	COM = * INNER RIGHT BACK *	36	OLD-	31 AA
RSI	S SURFN = 4	37	OLD-	32 AA
RSI	TYPE = RECT	38	OLD-	33 AA
RSI	ACTIVE = TOP	39	OLD-	34 AA
RSI	PROP = 0.9,0.9	40	OLD-	35 AA
RSI	P1 = 1.0, 1.0, 0.0	41	OLD-	36 AA
RSI	COM = * INNER RIGHT BOTTOM *	42	OLD-	37 AA
RSI	BCS BOXINL, INGBCS=BOXINR, NINC=10, IREFSF=1000	43	OLD-	38 AA
RSI	C	44	OLD-	39 AA
RSI	C-----THE FOREGOING CARD IMAGES BCS BOXINR IN REFERENCE PLANE 1000	45	OLD-	40 AA
RSI	C-----TO CREATE BCS BOXINL. THE INTERIOR OF THE BOX WAS INPUT IN	46	OLD-	41 AA
RSI	C-----THIS MANNER TO FACILITATE THE INPUT OF SAMPLE CASE 4 TO SHOW	47	OLD-	42 AA
RSI	C-----THE USE OF 'MESS' AND 'ERN' NODES.	48	OLD-	43 AA
RSI	C	49	OLD-	44 AA

IMAGING SURFACE (1) BCS (BOXINR), GENERATING SURFACE (11) BCS (BOXINL)
IMAGING SURFACE (2) BCS (BOXINR), GENERATING SURFACE (12) BCS (BOXINL)
IMAGING SURFACE (3) BCS (BOXINR), GENERATING SURFACE (13) BCS (BOXINL)

DATE 062870 TIME 205224 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 9

MODEL = SAMPLE SURFACE DATA INPUT BLOCK SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

		IMAGING SURFACE (4) BCS (BOXINR). GENERATING SURFACE (14) BCS (BOXINL)					
RSI	R	REFNO	= 1000	50	OLD-	45 AA	
RSI		P1	= 1.0, 0.0, 1.0	51	OLD-	46 AA	
RSI		P2	= 1.0, 0.0, 0.0	52	OLD-	47 AA	
RSI		P3	= 0.0, 0.0, 0.0	53	OLD-	48 AA	
RSI		CON	= * IMAGING PLANE *	54	OLD-	49 AA	
RSI	BCS	LIDINR		55	OLD-	50 AA	
RSI	S	SURFN	= 5	56	OLD-	51 AA	
RSI		TYPE	= RECT	57	OLD-	52 AA	
RSI		ACTIVE	= BOTTOM	58	OLD-	53 AA	
RSI		PROP	= 0.9,0.9	59	OLD-	54 AA	
RSI		P1	= 1.0, 1.0, 0.0	60	OLD-	55 AA	
RSI		CON	= * INNER RIGHT LID *	61	OLD-	56 AA	
INPUT	BCS	LIDINL		62		AB	
RSI	S	SURFN	= 15	63	OLD-	57 AA	
RSI		IMAGSF	= 5	64	OLD-	58 AA	
RSI		IREFSF	= 1000	65	OLD-	59 AA	
RSI		CON	= * INNER LEFT LID *	66	OLD-	60 AA	
RSI	BCS	BOXOUT		67	OLD-	61 AA	
RSI	S	SURFN	= 21	68	OLD-	62 AA	
RSI		TYPE	= BOX5	69	OLD-	63 AA	
RSI		ACTIVE	= OUT	70	OLD-	64 AA	
RSI		SHADE	= NO	71	OLD-	65 AA	
RSI		PROP	= 0.2,0.9	72	OLD-	66 AA	
RSI		P1	= 1.01,-1.01, 1.01	73	OLD-	67 AA	
RSI		P2	= 1.01, 1.01, 1.01	74	OLD-	68 AA	
RSI		P3	= -0.01, 1.01, 1.01	75	OLD-	69 AA	
RSI		P4	= -0.01, 1.01,-0.01	76	OLD-	70 AA	
RSI		CON	= * OUTER SURFACES *	77	OLD-	71 AA	
RSI	BCS	LIDOUT		78	OLD-	72 AA	
RSI	S	SURFN	= 26	79	OLD-	73 AA	
RSI		TYPE	= RECT	80	OLD-	74 AA	
RSI		ACTIVE	= TOP	81	OLD-	75 AA	
RSI		SHADE	= NO	82	OLD-	76 AA	
RSI		PROP	= 0.2,0.9	83	OLD-	77 AA	
RSI		P1	= 1.01,-1.01, 0.01	84	OLD-	78 AA	
RSI		P2	= 1.01, 1.01, 0.01	85	OLD-	79 AA	
RSI		P3	= -0.01, 1.01, 0.01	86	OLD-	80 AA	
RSI		CON	= * OUTER SURFACE OF LID *	87	OLD-	81 AA	
RSI	C			88	OLD-	82 AA	
RSI	C	-----THE NEXT TWO BCS'S (HESSR AND HESSL) ARE ACTIVATED IN SAMPLE			89	OLD-	83 AA
RSI	C	-----CASE 4 ONLY.			90	OLD-	84 AA
RSI	C			91	OLD-	85 AA	
RSI	BCS	HESSR		92	OLD-	86 AA	
RSI	S	SURFN	= 101	93	OLD-	87 AA	
RSI		TYPE	= RECT	94	OLD-	88 AA	
RSI		ACTIVE	= TOP	95	OLD-	89 AA	

DATE 062870 TIME 205225 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 10

MODEL = SAMPLE SURFACE DATA INPUT BLOCK SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CARD	ORIGIN	12345670	1	2345670	2	2345670	3	2345670	4	2345670	5	2345670	6	2345670	7	2345670	8	EDIT NO.	OLD EDIT NO.	LABEL	
RSI				PROP		=	1.0,1.0											96	OLD-	90	AA
RSI				P1		=	1.0, 0.0, 1.0											97	OLD-	91	AA
RSI				P2		=	1.0, 0.0, 0.0											98	OLD-	92	AA
RSI				P3		=	0.0, 0.0, 0.0											99	OLD-	93	AA
RSI				COM		=	* PRIMARY MESS NODE, RIGHT SIDE *											100	OLD-	94	AA
RSI	BCS			MESSL														101	OLD-	95	AA
RSI	S			SURFN		=	111											102	OLD-	96	AA
RSI				TYPE		=	RECT											103	OLD-	97	AA
RSI				ACTIVE		=	BOTTOM											104	OLD-	98	AA
RSI				PROP		=	1.0,1.0											105	OLD-	99	AA
RSI				P1		=	1.0, 0.0, 1.0											106	OLD-	100	AA
RSI				P2		=	1.0, 0.0, 0.0											107	OLD-	101	AA
RSI				P3		=	0.0, 0.0, 0.0											108	OLD-	102	AA
RSI				COM		=	* PRIMARY MESS NODE, LEFT SIDE *											109	OLD-	103	AA
RSI	C																	110	OLD-	104	AA
RSI	C			C-----THE FOLLOWING BCS (LIDSP) IS ACTIVATED IN SAMPLE CASE 3 ONLY.													111	OLD-	105	AA	
RSI	C																	112	OLD-	106	AA
RSI	BCS			LIDSP														113	OLD-	107	AA
RSI	S			SURFN		=	200											114	OLD-	108	AA
RSI				TYPE		=	RECT											115	OLD-	109	AA
RSI				ACTIVE		=	BOTTOM											116	OLD-	110	AA
RSI				PROP		=	0.1,0.1											117	OLD-	111	AA
RSI				SPR1		=	0.8											118	OLD-	112	AA
RSI				SPRS		=	0.8											119	OLD-	113	AA
RSI				P1		=	1.0,-1.0, 0.0											120	OLD-	114	AA
RSI				P2		=	1.0, 1.0, 0.0											121	OLD-	115	AA
RSI				P3		=	0.0, 1.0, 0.0											122	OLD-	116	AA
RSI				COM		=	* SPECULAR LID *											123	OLD-	117	AA

DATE 062070 TIME 205235 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 11

MODEL = SAMPLE SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL
BCS DATA INPUT BLOCK

CARD ORIGIN	12345670 1	2345670 2	2345670 3	2345670 4	2345670 5	2345670 6	2345670 7	2345670 8	EDIT NO.	OLD EDIT NO.	LABEL	
RSI	HEADER BCS DATA								124	OLD-	118	AA
RSI	BCS BOXINR								125	OLD-	119	AA
RSI	BCS BOXINL								126	OLD-	120	AA
RSI	BCS LIDINR .0..0..1..0..-45..0.								127	OLD-	121	AA
INPUT	BCS LIDINL .0..0..1..0..-45..0.								128			AB
RSI	BCS BOXOUT								129	OLD-	122	AA
RSI	BCS LIDOUT .0..0..1..0..-45..0.								130	OLD-	123	AA
RSI	BCS MESSR								131	OLD-	124	AA
RSI	BCS MESSL								132	OLD-	125	AA
RSI	BCS LIDSP .0..0..1..0..-45..0.								133	OLD-	126	AA

DATE 062078 TIME 205239

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION

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MODEL = SAMPLE
FORM FACTOR DATA INPUT BLOCK

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CARD	ORIGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL	
RSI																		134	OLD-	127	AA
RSI																		135	OLD-	128	AA
RSI																		136	OLD-	129	AA
RSI																		137	OLD-	130	AA
RSI																		138	OLD-	131	AA
RSI																		139	OLD-	132	AA
RSI																		140	OLD-	133	AA
RSI																		141	OLD-	134	AA
RSI																		142	OLD-	135	AA
RSI																		143	OLD-	136	AA
RSI																		144	OLD-	137	AA
RSI																		145	OLD-	138	AA
RSI																		146	OLD-	139	AA
RSI																		147	OLD-	140	AA
RSI																		148	OLD-	141	AA
RSI																		149	OLD-	142	AA
RSI																		150	OLD-	143	AA
RSI																		151	OLD-	144	AA
RSI																		152	OLD-	145	AA
RSI																		153	OLD-	146	AA
RSI																		154	OLD-	147	AA
RSI																		155	OLD-	148	AA
RSI																		156	OLD-	149	AA
RSI																		157	OLD-	150	AA
RSI																		158	OLD-	151	AA
RSI																		159	OLD-	152	AA
RSI																		160	OLD-	153	AA
RSI																		161	OLD-	154	AA
RSI																		162	OLD-	155	AA
RSI																		163	OLD-	156	AA
RSI																		164	OLD-	157	AA
RSI																		165	OLD-	158	AA
RSI																		166	OLD-	159	AA
RSI																		167	OLD-	160	AA
RSI																		168	OLD-	161	AA
RSI																		169	OLD-	162	AA
RSI																		170	OLD-	163	AA
RSI																		171	OLD-	164	AA
RSI																		172	OLD-	165	AA
RSI																		173	OLD-	166	AA
RSI																		174	OLD-	167	AA
RSI																		175	OLD-	168	AA
RSI																		176	OLD-	169	AA
RSI																		177	OLD-	170	AA
RSI																		178	OLD-	171	AA
INPUT																		179			AB
INPUT																		180			AB

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DATE 062870 TIME 205240 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 13

MODEL = SAMPLE SAMPLE CASE 4 - FFCAL/ODCAL/RCCAL
FORM FACTOR DATA INPUT BLOCK

CARD ORIGIN	12345678 1	2345678 2	2345678 3	2345678 4	2345678 5	2345678 6	2345678 7	2345678 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	C-----THE USE OF UNIT-SPHERE LOGIC. (NO SHADOWING)								181		AD
INPUT	C								182		AD
INPUT	FIG ENCL1								183		AD
INPUT	UNIT								184		AD
INPUT	C								185		AD
INPUT	C-----SPECIFY CALCULATION OF FORM FACTORS FOR ENCLOSURE 2 BY								186		AD
INPUT	C-----THE USE OF UNIT SPHERE LOGIC. (NO SHADOWING)								187		AD
INPUT	C								188		AD
INPUT	FIG ENCL2								189		AD
INPUT	UNIT								190		AD

DATE 062070 TIME 205247 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 14

MODEL = SAMPLE
CORRESPONDENCE DATA INPUT BLOCK SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CARD ORIGIN	12345678 1	2345678 2	2345678 3	2345678 4	2345678 5	2345678 6	2345678 7	2345678 8	EDIT NO.	OLD EDIT NO.	LABEL	
RSI	HEADER CORRESPONDENCE DATA								191	OLD-	172	AA
RSI	C								192	OLD-	173	AA
RSI	C-----ENTER CORRESPONDENCE DATA FOR CASE 2								193	OLD-	174	AA
RSI	C								194	OLD-	175	AA
RSI	FIG	CASE2							195	OLD-	176	AA
RSI		1	= 1,11,22						196	OLD-	177	AA
RSI		2	= 2,25						197	OLD-	178	AA
RSI		3	= 3,13,24						198	OLD-	179	AA
RSI		4	= 4,14,21						199	OLD-	180	AA
RSI		5	= 5,15,26						200	OLD-	181	AA
RSI		12	= 12,23						201	OLD-	182	AA
RSI	C								202	OLD-	183	AA
RSI	C-----ENTER CORRESPONDENCE DATA FOR CASE 3 TO COMBINE FORM FACTORS								203	OLD-	184	AA
RSI	C								204	OLD-	185	AA
RSI	FIG	CASE3,FF							205	OLD-	186	AA
RSI		1	= 1,11,22						206	OLD-	187	AA
RSI		2	= 2,25						207	OLD-	188	AA
RSI		3	= 3,13,24						208	OLD-	189	AA
RSI		4	= 4,14,21						209	OLD-	190	AA
RSI		5	= 5,15,26						210	OLD-	191	AA
RSI		12	= 12,23						211	OLD-	192	AA

DATE 062878 TIME 205249 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 15

MODEL = SAMPLE SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL
OPERATION DATA INPUT BLOCK (PASS 1)

CARD ORIGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL
RSI																	212	OLD-	193 AA

+++++ OPERATIONS DATA BLOCK (PASS 1) COMPLETE +++++

H-331

H-332

DATE 062878 TIME 205254 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 17

MODEL = SAMPLE
PROCESSOR CORE ALLOCATION

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

THE FOLLOWING IS THE PROCESSOR CORE ALLOCATION FOR THOSE SEGMENTS WHICH WILL BE LOADED IN THIS EXECUTION (APPROX.) ...

OCTAL/DECIMAL

TRASYS (0) SEGMENT	121222/ 41618
OPERATIONS DATA (NOT KNOWN AT THIS TIME).....	175000/ 64000
INITIALIZATION SEGMENT	122300/ 42176
FORM FACTOR SEGMENT	136100/ 48192
GRAY BODY SEGMENT	124000/ 43008
RADIATION CONDUCTOR SEGMENT	125500/ 43840
GRAY BODY DYNAMIC COMMON	000276/ 190
RADIATION CONDUCTOR DYNAMIC COMMON	000574/ 380
GRAY BODY MINIMUM - MAXIMUM CORE	123575/ 42877 - 123725/ 42965
RADIATION CONDUCTOR MINIMUM - MAXIMUM CORE	125230/ 43672 - 125474/ 43836
MINIMUM CORE NEEDED FOR PROCESSOR EXECUTION	136100/ 48192
MAXIMUM CORE NEEDED FOR PROCESSOR EXECUTION	136100/ 48192
AMOUNT OF CORE THAT WILL BE USED BY PROCESSOR .	136100/ 48192

MODEL = SAMPLE
 WRAP UP OF THE PRE-PROCESSOR SAMPLE CASE 4 - FFCAL/GBCAL/BCCAL

PRE-PROCESSOR ACCOUNTING INFORMATION	CP-SEC	DYN-STORAGE
SOURCE EDITING	1.534	676
DOCUMENTATION DATA PRE-PROCESSING000	0
QUANTITIES DATA PRE-PROCESSING027	266
ARRAY DATA PRE-PROCESSING082	20
SURFACE DATA PRE-PROCESSING (PASS 1) ...	1.090	64
SURFACE DATA PRE-PROCESSING (PASS 2)489	1141
BCS DATA PRE-PROCESSING172	201
FORM FACTOR DATA PRE-PROCESSING763	1169
SHADOW DATA PRE-PROCESSING000	0
FLUX DATA PRE-PROCESSING000	0
CORRESPONDENCE DATA PRE-PROCESSING211	101
OPERATIONS DATA PRE-PROCESSING	2.038	892
SUBROUTINE DATA PRE-PROCESSING147	0
SEQUENTIAL TAPE INITIALIZATION022	0
TOTAL CP TIME FOR PRE-PROCESSOR	0.963 DECIMAL SECONDS OR 000007 OCTAL SECONDS	
MINIMUM DYNAMIC STORAGE NEEDED BY PRE-PROCESSOR ..	1169 DECIMAL WORDS	
DYNAMIC STORAGE AVAILABLE TO PRE-PROCESSOR	10000 DECIMAL WORDS	

NORMAL TERMINATION BY PRE-PROCESSOR

@PHD,BLEP

@ASG,T/5 RSO.,BC.RSO.92.RSO APPENDIX H, CASE 4.

@TEST TNE/1/53

@JUMP L3
 INTERVENING STATEMENTS SKIPPED

@L3:FREE DATA1.

@FREE 14

M A S A / M A R T I N M A R I E T T A
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P R O C E S S O R E X E C U T I O N

VERSION.MODIFICATION ... UL2E6
MODIFICATION DATE 061970

DATE OF RUN 062070
TIME OF RUN 205915
JOB NUMBER RVMH04

DATE 062878 TIME 205919

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 1

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
PROCESSING OPERATIONS DATA

SAMPLE CASE 4 - FFCAL/GBCAL/BCAL

SEQUENCE	NODE	BCS	AREA	ALPH	EMISS	SURF. TYPE	ACTIVE	-----COMMENTS-----
1	1	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
2	2	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
3	3	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
4	4	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
5	5	LIDINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT LID
6	101	HESSR	1.00000	1.000	1.000	RECTANGLE	TOP	PRIMARY HESS NODE, RIGHT SIDE

NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE
BY -BUILDC- (ACCESS NUMBER = 1)

DATE 062070 TIME 205924

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 9 VERSION

PAGE 2

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

FORM FACTORS AND COMBINED FORM FACTORS - USER INPUT AND DEFAULT PARAMETERS

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
FFACC	.0500	.0500	ORIENTATION ACCURACY PARAMETER	N/A
FFACCS	.1000	.1000	SHADOWING ACCURACY PARAMETER	N/A
FFHIN	.1-05	1.0E-06	PARAMETER TO ELIMINATE SMALL FORM FACTORS	N/A
FFNOSH	SHAD	SHAD	OVER RIDE SHADOWING PARAMETER	(SHAD,NOSH)
*FFPNCH	NO	NO	PARAMETER TO PUNCH FORM FACTORS	(YES,NO)
FFPRNT	YES	YES	FLAG FOR COMPREHENSIVE FF AND CH PRINT	(YES,NO,FF,CH,RR)
FFRATL	15.0	15.0	RATIO FOR USING SUB-NODE TECHNIQUE	N/A
FFCHB	CORR	CORR	FLAG FOR COMBINING FORM FACTORS	(YES,NO,AUTO,CORR)

* -FFPNCH WILL DEFAULT TO -YES- ON CALCULATED VALUES IF THE -RSD- FILE IS NOT SPECIFIED IN THE OPTIONS DATA BLOCK

DATE 062870 TIME 205924

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 3

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

SEQUENCE	NODE	AREA	ALPH	EMISS
1	1	1.00000	.900	.900
2	2	1.00000	.900	.900
3	3	1.00000	.900	.900
4	4	1.00000	.900	.900
5	5	1.00000	.900	.900
6	101	1.00000	1.000	1.000

NUMBER OF NODES = 6 NUMBER OF SURFACES = 6

DATE 062870 TIME 205925

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION

PAGE 4

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

(*) -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) H/SHAD	FIR(J,I) H/SHAD	FSOL(I,J) H/SHAD	FSOL(J,I) H/SHAD	FF(I,J) H0/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
1	2	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.109	36	1
1	3	CAL	.200672	.200672	.200672	.200672	.200672	1.000000	1.000000	.066	36	1
1	4	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.064	36	1
1	5	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.067	36	1
1	101	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.065	36	1
1	FF SUM = 1.0000		ROW CP TIME =		.437							
1	FORM FACTOR RESTART (RSO) RECORD =		21									
2	3	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.065	36	1
2	4	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.064	36	1
2	5	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.064	36	1
2	101	CAL	.200672	.200672	.200672	.200672	.200672	1.000000	1.000000	.067	36	1
2	FF SUM = 1.0000		ROW CP TIME =		.311							
2	FORM FACTOR RESTART (RSO) RECORD =		22									
3	4	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.066	36	1
3	5	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.066	36	1
3	101	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.065	36	1
3	FF SUM = 1.0000		ROW CP TIME =		.232							
3	FORM FACTOR RESTART (RSO) RECORD =		23									
4	5	CAL	.200672	.200672	.200672	.200672	.200672	1.000000	1.000000	.062	36	1
4	101	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.062	36	1
4	FF SUM = 1.0000		ROW CP TIME =		.151							
4	FORM FACTOR RESTART (RSO) RECORD =		24									

DATE 062878 TIME 205929 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 5

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1 SAMPLE CASE 4 - FFCAL/OBCAL/RCCAL
FORM FACTOR CALCULATION LINK.

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUES OF RSI, RTI, OR CARD INPUT)
19.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W0/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
5	101	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.064	36	1
5		FF SUM = 1.0000	ROW CP TIME = .126									
		FORM FACTOR RESTART (RSO) RECORD = 25										
101		FF SUM = 1.0000	ROW CP TIME = .009									
		FORM FACTOR RESTART (RSO) RECORD = 26										

FF FORM FACTORS FOR CONFIGURATION ENCL1 HAVE BEEN STORED ON RSO.
LAST RESTART RECORD WRITTEN = 26

DATE 062878 TIME 205930 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 6

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/OBCAL/RCCAL

SUMMARY OF FORM FACTOR SUMS FOR ALL NODES

NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM
1- 1.0000	2- 1.0000	3- 1.0000	4- 1.0000	5- 1.0000	101- 1.0000
TOTAL TIME FOR FORM FACTOR SEGMENT		1.640			
TOTAL TIME SINCE START OF RUN		35.717			

DATE 062078 TIME 205931

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 7

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
PROCESSING OPERATIONS DATA

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

NODE DATA--

NODE	AREA	ALPH	EMISS	TRAN(SOL)	TRAN(IR)	SPECULAR REFL(SOL)	SPECULAR REFL(IR)
1	1.00000	.900+00	.500+00	.000	.000	.000	.000
2	1.00000	.900+00	.500+00	.000	.000	.000	.000
3	1.00000	.900+00	.500+00	.000	.000	.000	.000
4	1.00000	.900+00	.500+00	.000	.000	.000	.000
5	1.00000	.900+00	.500+00	.000	.000	.000	.000
101	1.00000	.100+01	.100+01	.000	.000	.000	.000

NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE
BY -TRASYS- FOLLOWING MODIFICATION(S). (ACCESS NUMBER = 2)

DATE 062070 TIME 205932 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 8

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1 SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL
GRAY BODIES COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
GBH8ND	IR	BOTH	HAVEBAND DEFINITION PARAMETER	(2H1R.3HSOL.4HBOTH)

.....
IR GRAY BODIES FOR CONFIGURATION ENCL1 HAVE BEEN COMPUTED AND STORED ON R50.
LAST RESTART RECORD WRITTEN = 44
.....

TOTAL TIME TO COMPUTE GRAY BODIES .21

DATE 062070 TIME 205934

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION

PAGE 9

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

VARIABLE NAME	CURRENT VALUE	DEFAULT	RADIATION CONDUCTORS DEFINITION	OPTIONS
RKPNCH	PUN	NO	PUNCH/NO PUNCH PARAMETER FOR RADKS	(YES,NO)
RKHIN	.0001	0.0001	PARAMETER TO ELIMINATE SMALL RADK S	N/A
IRKCN	1	1	INITIAL RADIATION CONDUCTOR ID NUMBER	N/A
RKSP	NO	NO	MNEMONIC FLAG FOR COMPUTATION OF RADKS TO SPACE	(SPACE,NO)
IRKNSP	32767	32767	SPACE NODE ID NUMBER	N/A
SIGMA	.17-08	1.713E-9	STEFAN-BOLTZMANN CONSTANT	N/A
RKAMPF	1.00	1.0	AREA MULTIPLYING FACTOR	N/A
RKTAPE	NO	NO	PARAMETER TO OUTPUT TO BCD TAPE	(TAPE,NO)
RFRAC	.7+00	0.7	SIGNIFICANT RADIATION FRACTION	(0. TO 1.)
RTOL	.990	0.99	DECIMAL FRACTION OF LAST RADK SAVED	N/A
NERN	0	0	EFFECTIVE RADIATION NODE (ERN) NUMBER	N/A

DATE 062070 TIME 205935 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 10

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

SPECIAL RADIATION NODES

NONE

MESS SPECIAL NODES

PRIMARY SECONDARY

101 111

DATE 062070 TIME 205935

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 11

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

RADIATION CONDUCTOR (RADKS) CARDS

AREA UNITS = INPUT UNITS * AMPF. WHERE AMPF = 1.00000

PUNCHED AND/OR BCD0U RADKS -	-	1.	1.	2.	.12969-09\$
PUNCHED AND/OR BCD0U RADKS -	-	2.	1.	3.	.13003-09\$
PUNCHED AND/OR BCD0U RADKS -	-	3.	1.	4.	.12974-09\$
PUNCHED AND/OR BCD0U RADKS -	-	4.	1.	5.	.12974-09\$
PUNCHED AND/OR BCD0U RADKS -	-	5.	-1.	101.	.28540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	6.	-111.	1.	.28540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	7.	2.	3.	.12969-09\$
PUNCHED AND/OR BCD0U RADKS -	-	8.	2.	4.	.12969-09\$
PUNCHED AND/OR BCD0U RADKS -	-	9.	2.	5.	.12969-09\$
PUNCHED AND/OR BCD0U RADKS -	-	10.	-2.	101.	.28594-09\$
PUNCHED AND/OR BCD0U RADKS -	-	11.	-111.	2.	.28594-09\$
PUNCHED AND/OR BCD0U RADKS -	-	12.	3.	4.	.12974-09\$
PUNCHED AND/OR BCD0U RADKS -	-	13.	3.	5.	.12974-09\$
PUNCHED AND/OR BCD0U RADKS -	-	14.	-3.	101.	.28540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	15.	-111.	3.	.28540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	16.	4.	5.	.13003-09\$
PUNCHED AND/OR BCD0U RADKS -	-	17.	-4.	101.	.28540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	18.	-111.	4.	.28540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	19.	-5.	101.	.28540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	20.	-111.	5.	.28540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	21.	-101.	111.	.17868-09\$

DATE 062970 TIME 205541

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 12

MODEL=SAMPLE CONFIG=ENCL1 STEP=1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE BEFORE RK4IN SCREENING

1 - .10000+01	2 - .10000+01	3 - .10000+01	4 - .10000+01	5 - .10000+01	-101 - .93767+00
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DATE 062070 TIME 205042 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 13

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE AFTER RKHIN SCREENING

1 -	.10000+01	2 -	.10000+01	3 -	.10000+01	4 -	.10000+01	5 -	.10000+01	-101 -	.93767+00
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DATE 062070 TIME 205943

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION

PAGE 14

MODEL=SAMPLE CONFIG=ENCL1 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

THE INPUT SIGNIFICANT RADIATION FRACTION = .700

THE NUMBER OF CONDUCTORS INPUT = 21

THE NUMBER OF CONDUCTORS OUTPUT = 21

WHICH IS A .0 PERCENT REDUCTION IN THE NUMBER OF CONDUCTORS.

100.0 PERCENT OF THE TOTAL EMISSIVE POWER IS EXACTLY COUPLED.

TOTAL TIME TO COMPUTE AND CONDENSE RADKS = .51

DATE 062070 TIME 205945

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 15

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
PROCESSING OPERATIONS DATA

SAMPLE CASE 4 - FFCAL/GBCAL/BCCAL

SEQUENCE	NODE	BCS	AREA	ALPH	EMISS	SURF. TYPE	ACTIVE	-----COMMENTS-----
1	11	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
2	12	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
3	13	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
4	14	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
5	15	LIDINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER LEFT LID
6	111	HESSL	1.00000	1.000	1.000	RECTANGLE	BOTTOM	PRIMARY HESS NODE. LEFT SIDE

NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE
BY -BUILDG- (ACCESS NUMBER = 3)

DATE 062870 TIME 205949

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 16

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

FORM FACTORS AND COMBINED FORM FACTORS - USER INPUT AND DEFAULT PARAMETERS

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
FFACC	.0500	.0500	ORIENTATION ACCURACY PARAMETER	N/A
FFACCS	.1000	.1000	SHADOWING ACCURACY PARAMETER	N/A
FFMIN	.1-05	1.0E-06	PARAMETER TO ELIMINATE SMALL FORM FACTORS	N/A
FFNOSH	SHAD	SHAD	OVER RIDE SHADOWING PARAMETER	(SHAD,NOSH)
+FFPNCH	NO	NO	PARAMETER TO PUNCH FORM FACTORS	(YES,NO)
FFPRNT	YES	YES	FLAG FOR COMPREHENSIVE FF AND CM PRINT	(YES,NO,FF,CM,RB)
FFRATL	15.0	15.0	RATIO FOR USING SUB-NODE TECHNIQUE	N/A
FFCMB	NO	CORR	FLAG FOR COMBINING FORM FACTORS	(YES,NO,AUTO,CORR)

* -FFPNCH WILL DEFAULT TO -YES- ON CALCULATED VALUES IF THE -RSD- FILE IS NOT SPECIFIED IN THE OPTIONS DATA BLOCK

DATE 062878 TIME 205950

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION PAGE 17

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/GDCAL/RCCAL

SEQUENCE	NODE	AREA	ALPH	EMISS
1	11	1.00000	.900	.900
2	12	1.00000	.900	.900
3	13	1.00000	.900	.900
4	14	1.00000	.900	.900
5	15	1.00000	.900	.900
6	111	1.00000	1.000	1.000

NUMBER OF NODES = 6 NUMBER OF SURFACES = 6

DATE 062070 TIME 205950

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 10

MODEL=SAHLE CONFIG=ENCL2 STEP=-2
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) H/SHAD	FIR(J,I) H/SHAD	FSOL(I,J) H/SHAD	FSOL(J,I) H/SHAD	FF(I,J) H0/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
11	12	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.116	36	1
11	13	CAL	.200672	.200672	.200672	.200672	.200672	1.000000	1.000000	.065	36	1
11	14	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.070	36	1
11	15	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.072	36	1
11	111	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.070	36	1
11	FF SUM = 1.0000		ROW CP TIME =		.464							
	FORM FACTOR RESTART (RSO) RECORD =		58									
12	13	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.071	36	1
12	14	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.071	36	1
12	15	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.070	36	1
12	111	CAL	.200672	.200672	.200672	.200672	.200672	1.000000	1.000000	.071	36	1
12	FF SUM = 1.0000		ROW CP TIME =		.330							
	FORM FACTOR RESTART (RSO) RECORD =		59									
13	14	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.069	36	1
13	15	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.070	36	1
13	111	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.072	36	1
13	FF SUM = 1.0000		ROW CP TIME =		.251							
	FORM FACTOR RESTART (RSO) RECORD =		60									
14	15	CAL	.200672	.200672	.200672	.200672	.200672	1.000000	1.000000	.066	36	1
14	111	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.066	36	1
14	FF SUM = 1.0000		ROW CP TIME =		.160							
	FORM FACTOR RESTART (RSO) RECORD =		61									

DATE 082870 TIME 205954 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 15

MODEL=SANPLE CONFIG=ENCL2 STEP=-2
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWNM CALCULATION MODE BECAUES OF RSI, RTI, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWNM DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
15	111	CAL	.199837	.199837	.199837	.199837	.199837	1.000000	1.000000	.063	36	1
15	FF SUM = 1.0000 ROW CP TIME = .127											
	FORM FACTOR RESTART (RSO) RECORD = 62											
111	FF SUM = 1.0000 ROW CP TIME = .009											
	FORM FACTOR RESTART (RSO) RECORD = 63											

FF FORM FACTORS FOR CONFIGURATION ENCL2 HAVE BEEN STORED ON RSO.
LAST RESTART RECORD WRITTEN = 63

DATE 062870 TIME 205955

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC D VERSION

PAGE 20

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

SUMMARY OF FORM FACTOR SUMS FOR ALL NODES

NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM
11- 1.0000	12- 1.0000	13- 1.0000	14- 1.0000	15- 1.0000	111- 1.0000
TOTAL TIME FOR FORM FACTOR SEGMENT		1.731			
TOTAL TIME SINCE START OF RUN		38.778			

DATE 062070 TIME 205956 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 21

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2 SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL
PROCESSING OPERATIONS DATA

NODE DATA--

NODE	AREA	ALPH	EMISS	TRAN(SOL)	TRAN(IR)	SPECULAR REFL(SOL)	SPECULAR REFL(IR)
11	1.00000	.900+00	.500+00	.000	.000	.000	.000
12	1.00000	.900+00	.500+00	.000	.000	.000	.000
13	1.00000	.900+00	.500+00	.000	.000	.000	.000
14	1.00000	.900+00	.500+00	.000	.000	.000	.000
15	1.00000	.900+00	.500+00	.000	.000	.000	.000
111	1.00000	.100+01	.100+01	.000	.000	.000	.000

NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE
BY -TRASYS- FOLLOWING MODIFICATION(S). (ACCESS NUMBER = 4)

DATE 062878 TIME 205957 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION PAGE 22

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
GRAY BODIES COMPUTATION LINK.

SAMPLE CASE 4 - FFCAL/GDCAL/RCCAL

VARIABLE NAME	CURRENT VALUE	DEFAULT	GREY BODIES DEFINITION	OPTIONS
G8HBND	IR	BOTH	WAVEBAND DEFINITION PARAMETER	(2HIR,3HSOL,4HBOTH)

.....

IR GRAY BODIES FOR CONFIGURATION ENCL2 HAVE BEEN COMPUTED AND STORED ON RSO.
LAST RESTART RECORD WRITTEN = 81

.....

TOTAL TIME TO COMPUTE GRAY BODIES .22

DATE 062878 TIME 210000

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 23

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
RKPNCH	PUN	NO	PUNCH/NO PUNCH PARAMETER FOR RADKS	(YES,NO)
RKHIN	.0001	0.0001	PARAMETER TO ELIMINATE SMALL RADK S	N/A
IRKCN	1	1	INITIAL RADIATION CONDUCTOR ID NUMBER	N/A
RKSP	NO	NO	MNEMONIC FLAG FOR COMPUTATION OF RADKS TO SPACE	(SPACE,NO)
IRKNSP	32767	32767	SPACE NODE ID NUMBER	N/A
SIGMA	.17-08	1.713E-9	STEFAN-BOLTZMANN CONSTANT	N/A
RKAMPF	1.00	1.0	AREA MULTIPLYING FACTOR	N/A
RKTAPE	NO	NO	PARAMETER TO OUTPUT TO BCD TAPE	(TAPE,NO)
RFRAC	.5+00	0.7	SIGNIFICANT RADIATION FRACTION	(0. TO 1.)
RTOL	1.00	0.99	DECIMAL FRACTION OF LAST RADK SAVED	N/A
NERN	555	0	EFFECTIVE RADIATION NODE (ERN) NUMBER	N/A

DATE 062070 TIME 210000

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 24

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

SPECIAL RADIATION NODES

NONE

MESS SPECIAL NODES

PRIMARY SECONDARY

111 101

MODEL=SAHPLE CONFIG=ENCL2 STEP=-2
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

RADIATION CONDUCTOR (RADKS) CARDS

AREA UNITS = INPUT UNITS * AMPF, WHERE AMPF = 1.00000

****	11.	11.	.1713000-08*	.3031613-01
PUNCHED AND/OR BCD0U RADKS -	-	1. 11.	13.	.13003-09\$
PUNCHED AND/OR BCD0U RADKS -	-	2. -11.	111.	.20540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	3. -101.	11.	.20540-09\$
	11.	12.	.1713000-08*	.7570016-01
	11.	14.	.1713000-08*	.7573692-01
	11.	15.	.1713000-08*	.7573692-01

PUNCHED AND/OR BCD0U RADKS -	-	4. 11.	555.	.38916-09\$
****	12.	12.	.1713000-08*	.3025055-01
PUNCHED AND/OR BCD0U RADKS -	-	5. 12.	15.	.12969-09\$
PUNCHED AND/OR BCD0U RADKS -	-	6. -12.	111.	.20594-09\$
PUNCHED AND/OR BCD0U RADKS -	-	7. -101.	12.	.20594-09\$
	12.	11.	.1713000-08*	.7570016-01
	12.	13.	.1713000-08*	.7570016-01
	12.	14.	.1713000-08*	.7570015-01

PUNCHED AND/OR BCD0U RADKS -	-	8. 12.	555.	.38906-09\$
****	13.	13.	.1713000-08*	.3031613-01
PUNCHED AND/OR BCD0U RADKS -	-	9. -13.	111.	.20540-09\$
PUNCHED AND/OR BCD0U RADKS -	-	10. -101.	13.	.20540-09\$
	13.	12.	.1713000-08*	.7570016-01
	13.	14.	.1713000-08*	.7573692-01
	13.	15.	.1713000-08*	.7573692-01

PUNCHED AND/OR BCD0U RADKS -	-	11. 13.	555.	.38916-09\$
****	14.	14.	.1713000-08*	.3031613-01
PUNCHED AND/OR BCD0U RADKS -	-	12. 14.	15.	.13003-09\$
PUNCHED AND/OR BCD0U RADKS -	-	13. -14.	111.	.20540-09\$

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
 RADIATION CONDUCTOR GENERATION LINK. SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

RADIATION CONDUCTOR (RADK) CARDS

AREA UNITS = INPUT UNITS * AMPF, WHERE AMPF = 1.00000

PUNCHED AND/OR BCD0U RADKS -	-	14, -101, 14,	.28540-09\$	
		14, 11,	.1713000-08*	.7573692-01
		14, 12,	.1713000-08*	.7570815-01
		14, 13,	.1713000-08*	.7573692-01
<hr/>				
PUNCHED AND/OR BCD0U RADKS -	-	15, 14, 555,	.38916-09\$	
		15, 15,	.1713000-08*	.3031614-01
PUNCHED AND/OR BCD0U RADKS -	-	16, -15, 111,	.28540-09\$	
PUNCHED AND/OR BCD0U RADKS -	-	17, -101, 15,	.28540-09\$	
		15, 11,	.1713000-08*	.7573692-01
		15, 13,	.1713000-08*	.7573692-01
<hr/>				
PUNCHED AND/OR BCD0U RADKS -	-	18, 15, 555,	.25947-09\$	
PUNCHED AND/OR BCD0U RADKS -	-	19, -111, 101,	.17868-09\$	

DATE 082870 TIME 210011 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 27

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE BEFORE RKHIN SCREENING

11 - .10000+01	12 - .10000+01	13 - .10000+01	14 - .10000+01	15 - .10000+01	-111 - .93767+00
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DATE 062878 TIME 210012 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 28

MODEL=SAMPLE CONFIG=ENCL2 STEP=-2 SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL
RADIATION CONDUCTOR GENERATION LINK.

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE AFTER RKNIN SCREENING

11 - .10000+01 12 - .10000+01 13 - .10000+01 14 - .10000+01 15 - .10000+01 -111 - .93767+00

DATE 062878 TIME 210014 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION , PAGE 29

MODEL=SAFPLE CONFIG=ENCL2 STEP=-2 SAMPLE CASE 4 - FFCAL/GBCAL/RCCAL
RADIATION CONDUCTOR GENERATION LINK.

THE INPUT SIGNIFICANT RADIATION FRACTION = .500

THE NUMBER OF CONDUCTORS INPUT = 21

THE NUMBER OF CONDUCTORS OUTPUT = 19

WHICH IS A 9.5 PERCENT REDUCTION IN THE NUMBER OF CONDUCTORS.

69.7 PERCENT OF THE TOTAL EMISSIVE POWER IS EXACTLY COUPLED.

TOTAL TIME TO COMPUTE AND CONDENSE RADKS = .69

NORMAL TERMINATION BY PROCESSOR

8PMD,PLEB

8BRKPT PRINTS

SAMPLE CASE 5

QED,R V00TB.CASES
 FILE IN FIELD 1 DISABLED--ACCEPTED
 FILE IN FIELD 1 IN USE BY ANOTHER RUN
 READ-ONLY MODE
 CASE UPPER ASSUMED
 ED 14.02-06/20-01:48-(0.)
 EDIT

NO DECK V00T

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1:RUN,R/R RVHM05.3240-F261-C,ES3-N03711.09.150
10:0ASG,A ES3-TRASYS*TRASYS.
11:0ADD ES3-TRASYS*TRASYS.STARTH
12:0SETC 0100
13:0ADD PREPRO
14:HEADER OPTIONS DATA
15:TITLE SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
16:  MODEL      = SAMPLE
17:  RSO        = RSTSAM5
18:HEADER SURFACE DATA
19:C
20:C-----THIS SURFACE DATA BLOCK IS USED IN SAMPLE CASES 1 THROUGH 5
21:C-----WITH VARIOUS PORTIONS OF IT BEING ACTIVATED FOR THE DIFFERENT
22:C-----CASES.
23:C
24:BCS  BOXINR
25:S    SURFN      = 1
26:      TYPE       = RECT
27:      ACTIVE      = BOTTOM
28:      PROP        = 0.9,0.9
29:      P1          = 1.0, 0.0, 1.0
30:      P2          = 1.0, 0.0, 0.0
31:      P3          = 1.0, 1.0, 0.0
32:      COM         = * INNER RIGHT FRONT *
33:S    SURFN      = 2
34:      TYPE       = RECT
35:      ACTIVE      = BOTTOM
36:      PROP        = 0.9,0.9
37:      P1          = 1.0, 1.0, 1.0
38:      P2          = 1.0, 1.0, 0.0
39:      P3          = 0.0, 1.0, 0.0
40:      COM         = * INNER RIGHT SIDE *
41:S    SURFN      = 3
42:      TYPE       = RECT
43:      ACTIVE      = TOP
44:      PROP        = 0.9,0.9
45:      P1          = 0.0, 0.0, 1.0
46:      P2          = 0.0, 0.0, 0.0
47:      P3          = 0.0, 1.0, 0.0
48:      COM         = * INNER RIGHT BACK *
49:S    SURFN      = 4
50:      TYPE       = RECT
51:      ACTIVE      = TOP
52:      PROP        = 0.9,0.9
53:      P1          = 1.0, 1.0, 0.0
54:      COM         = * INNER RIGHT BOTTOM *
55:BCS  BOXINL,IM0BCS=BOXINR,NINC=10,IREFSF=1000
56:C
57:C-----THE FOREGOING CARD IMAGES BCS BOXINR IN REFERENCE PLANE 1000
58:C-----TO CREATE BCS BOXINL. THE INTERIOR OF THE BOX WAS INPUT IN

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59:C-----THIS-MANNER TO FACILITATE THE INPUT OF SAMPLE CASE 4 TO SHOW -
60:C-----THE USE OF 'MESS' AND 'ERN' NODES.
61:C
62:R      REFNO      = 1000
63:      P1          = 1.0, 0.0, 1.0
64:      P2          = 1.0, 0.0, 0.0
65:      P3          = 0.0, 0.0, 0.0
66:      COM         = * IMAGING PLANE *
67:BCS    LIDINR
68:S      SURFN      = 5
69:      TYPE        = RECT
70:      ACTIVE      = BOTTOM
71:      PROP        = 0.9,0.9
72:      P1          = 1.0, 1.0, 0.0
73:      COM         = * INNER RIGHT LID *
74:S      SURFN      = 15
75:      IMAGSF      = 5
76:      IREFSF      = 1000
77:      COM         = * INNER LEFT LID *
78:BCS    BOXOUT
79:S      SURFN      = 21
80:      TYPE        = BOXS
81:      ACTIVE      = OUT
82:      SHADE       = NO
83:      PROP        = 0.2,0.9
84:      P1          = 1.01,-1.01, 1.01
85:      P2          = 1.01, 1.01, 1.01
86:      P3          = -0.01, 1.01, 1.01
87:      P4          = -0.01, 1.01,-0.01
88:      COM         = * OUTER SURFACES *
89:BCS    LIDOUT
90:S      SURFN      = 28
91:      TYPE        = RECT
92:      ACTIVE      = TOP
93:      SHADE       = NO
94:      PROP        = 0.2,0.9
95:      P1          = 1.01,-1.01, 0.01
96:      P2          = 1.01, 1.01, 0.01
97:      P3          = -0.01, 1.01, 0.01
98:      COM         = * OUTER SURFACE OF LID *
99:C
100:C-----THE NEXT TWO BCSIS (MESSR AND MESSL) ARE ACTIVATED IN SAMPLE
101:C-----CASE 4 ONLY.
102:C
103:BCS    MESSR
104:S      SURFN      = 101
105:      TYPE        = RECT
106:      ACTIVE      = TOP
107:      PROP        = 1.0,1.0
108:      P1          = 1.0, 0.0, 1.0
109:      P2          = 1.0, 0.0, 0.0
110:      P3          = 0.0, 0.0, 0.0
111:      COM         = * PRIMARY MESS NODE, RIGHT SIDE *
112:BCS    MESSL
113:S      SURFN      = 111
114:      TYPE        = RECT
115:      ACTIVE      = BOTTOM

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116:      PROP      = 1.0,1.0
117:      P1         = 1.0, 0.0, 1.0
118:      P2         = 1.0, 0.0, 0.0
119:      P3         = 0.0, 0.0, 0.0
120:      COM        = * PRIMARY MESS NODE, LEFT SIDE *
121:C
122:C-----THE FOLLOWING BCS (LIDSP) IS ACTIVATED IN SAMPLE CASE 5 ONLY.
123:C
124:BCS      LIDSP
125:S      SURFN      = 200
126:      TYPE      = RECT
127:      ACTIVE     = BOTTON
128:      PROP      = 0.1,0.1
129:      SPRI      = 0.8
130:      SPRS      = 0.8
131:      P1         = 1.0,-1.0, 0.0
132:      P2         = 1.0, 1.0, 0.0
133:      P3         = 0.0, 1.0, 0.0
134:      COM        = * SPECULAR LID *
135:HEADER BCS DATA
136:BCS      BOXINR
137:BCS      BOXIML
138:BCS      LIDINR ,0.,0.,1.,0.,-45.,0.
139:BCS      BOXOUT
140:BCS      LIDOUT ,0.,0.,1.,0.,-45.,0.
141:BCS      MESSR
142:BCS      MESSL
143:BCS      LIDSP ,0.,0.,1.,0.,-45.,0.
144:HEADER FORM FACTOR DATA
145:C
146:C-----ENTER KNOWN ZERO FORM FACTORS AND EQUIVALENT FORM FACTORS FOR
147:C-----CASE5.
148:C
149:F10      CASE1
150:NODEA    1,2,3,4,11,12,13,14,200,21,22,23,24,25,26,END
151:BOTH     21,ZERO
152:      22,ZERO
153:      23,ZERO
154:      24,ZERO
155:      25,ZERO
156:      26,ZERO
157:      1,1,0.
158:      11,12,1,2
159:      11,13,1,3
160:      11,14,1,4
161:      11,200,1,200
162:      1,11,0.
163:      11,2,1,12
164:      11,3,1,13
165:      11,4,1,14
166:      2,2,0.
167:      2,3,1,2
168:      2,4,1,4
169:      12,13,2,3
170:      12,14,2,4
171:      12,200,2,200
172:      12,3,2,13

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173:      12,4,2,14
174:      3,3,0.
175:      3,4,1,4
176:      13,14,3,4
177:      13,200,3,200
178:      3,13,0.
179:      13,4,3,14
180:      4,4,0.
181:      14,200,4,200
182:      4,14,0.
183:      200,200,0.
184:HEADER CORRESPONDENCE DATA
185:C
186:C-----ENTER CORRESPONDENCE DATA FOR CASE 2
187:C
188:F10      CASE2
189:      1          = 1,11,22
190:      2          = 2,25
191:      3          = 3,13,24
192:      4          = 4,14,21
193:      5          = 5,15,26
194:      12         = 12,23
195:C
196:C-----ENTER CORRESPONDENCE DATA FOR CASE 3 TO COMBINE FORM FACTORS
197:C
198:F10      CASE3,FF
199:      1          = 1,11,22
200:      2          = 2,25
201:      3          = 3,13,24
202:      4          = 4,14,21
203:      5          = 5,15,26
204:      12         = 12,23
205:HEADER OPERATIONS DATA
206:C
207:C-----BUILD THE CASE 5 CONFIGURATION
208:C
209:BUILD CASE5,BOXINR,BOXINL,LIDSP,BOXOUT,LIDOUT
210:C
211:C-----CALCULATE THE FORM FACTOR MATRIX.
212:C
213:L      FFCAL
214:C
215:C-----CALCULATE IMAGE FACTORS
216:C
217:      CALL RBDATA(0,0,0,0,0)
218:L      RBCAL
219:C
220:C-----CALCULATE THE GRAY BODY MATRIX USING IMAGE FACTORS.
221:C
222:      CALL GBDATA(BOTH,0,RB)
223:L      GBCAL
224:C
225:C-----CALCULATE AND PUNCH RADIATION CONDUCTORS.
226:C
227:      CALL RKDATA(0,0,0,0,SPACE,999,0,0,0,0)
228:L      RKCAL
229:C

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230:C-----DEFINE ORBIT AND VEHICLE ORIENTATION (CIRCULAR-PLANET-ORIENTED)
231:C
232:      CALL ORBIT2(EAR,0.00,0.0,0.100,0000,100,0000.)
233:      CALL ORIENT(4MPLAN,1,2,3,300,270,0.)
234:C
235:C-----SET BACPRINT TO PRINT THE COMPONENT VALUES OF ABSORBED Q'S.
236:C
237:      BACPRINT      =YES
238:C
239:C-----CALCULATE INCIDENT FLUXES PLUS SPECULAR REFLECTIONS.
240:C
241:ORBGEN CIRP,0,180,2,01
242:STEP 10010
243:      CALL DRDATA(10000,0)
244:L      DRCAL
245:      CALL AQDATA(0,0,0,0,0)
246:L      AQCAL
247:C
248:STEP 10011
249:      CALL DRDATA(10001,0)
250:L      DRCAL
251:      CALL AQDATA(0,0,0,0,0)
252:L      AQCAL
253:C
254:STEP 10012
255:      CALL DRDATA(10002,0)
256:L      DRCAL
257:      CALL AQDATA(0,0,0,0,0)
258:L      AQCAL
259:C
260:STEP 10013
261:      CALL DRDATA(10003,0)
262:L      DRCAL
263:      CALL AQDATA(0,0,0,0,0)
264:L      AQCAL
265:C
266:STEP 10014
267:      CALL DRDATA(10004,0)
268:L      DRCAL
269:      CALL AQDATA(0,0,0,0,0)
270:L      AQCAL
271:C
272:      CALL QODATA(3HALL,0,0,0,0,0,0,0)
273:L      QOCAL
274:END OF DATA
275:8PHD,8LEP
276:8ASQ,T/S R50,8C,R50,92,R50 APPENDIX H, CASE 5.
277:8ADD PROCSS
285:8FIN
NO CORRECTIONS APPLIED.

```

H-370

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8ASQ,A ES3-TRASYS*TRASYS.
FAC WARNING      040000100200

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M A S A / M A R T I N M A R I E T T A
T H E R M A L R A D I A T I O N A N A L Y S I S S Y S T E M
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P R E - P R O C E S S O R E X E C U T I O N

VERSION.MODIFICATION ... UC2E3
MODIFICATION DATE 052678
DATE OF RUN 062878
TIME OF RUN 014922
JOB NUMBER RVMH05

DATE 002070 TIME 014024 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 1
 MODEL = N/A
 OPTION AND TITLE DATA BLOCKS
 CARD ORIGIN 12345670 1 2345670 2 2345670 3 2345670 4 2345670 5 2345670 6 2345670 7 2345670 8 EDIT NO. OLD EDIT NO. LABEL
 INPUT HEADER OPTIONS DATA
 INPUT TITLE SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
 INPUT MODEL = SAMPLE
 INPUT RSO = RSTSAH5

DATE 062070 TIME 014824 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC B VERSION PAGE 2

MODEL = SAMPLE SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
TRASYS INFORMATION TO USER

*
* ATTENTION TRASYS USERS *
*

THIS SECTION OF THE TRASYS PRINTOUT WAS DEVISED TO
INFORM THE TRASYS USERS OF THE STATUS OF THE TRASYS
PROGRAM WITHOUT HAVING TO PRINTOUT ALL THE STATUS
INFORMATION ON EVERY RUN. TO OBTAIN ADDITIONAL
INFORMATION ON HOW TO USE THIS SECTION OF THE TRASYS
PRINTOUT, PLACE A (INFO=INFO) IN THE OPTIONS DATA
BLOCK.

FOR TRASYS ASSISTANCE AND/OR POSSIBLE TRASYS PROGRAM
PROBLEMS, PLEASE CONTACT BOB VOOT AT JSC-2326.

NEHRL 08/29/77 DOCUMENTATION ADDITION

THE TRASYS -N- VERSION HAS BEEN UPDATED TO THE UC2E2
AND UL2E4 LEVEL.
SEE LATEST USERS MANUAL FOR INFORMATION ON USER-
CALLED SUBROUTINE ARGUMENT CHANGES AND NEW
CAPABILITIES.

END OF TRASYS INFORMATION FILE

++NOTE++ DATA ORIGINATION FROM INPUT FILE. NO -RSI- SOURCE EDITING

DATE 062878 TIME 014827 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC @ VERSION PAGE 3

MODEL = SAMPLE SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QOCAL
MODEL HISTORY

MODEL NAME SAMPLE

MODEL TITLE SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QOCAL

MOD	RUN	JOB	RUN	RUN	RSI	RSO	RTI	RTO	CMERG	EMERG	BCDOU	TRAJ	USER1	USER2
LABEL	NUMBER		DATA	TIME	TAPE	TAPE	TAPE	TAPE	TAPE	TAPE	TAPE	TAPE	TAPE	TAPE
AA	RVHM05	062878	014924		RSTSAH									

DATE 062878 TIME 014827 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 4
MODEL = SAMPLE SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QOCAL
SOURCE DATA EDIT DIRECTIVES
CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

INPUT	HEADER SURFACE DATA	1	AA
INPUT	C	2	AA
INPUT	C-----THIS SURFACE DATA BLOCK IS USED IN SAMPLE CASES 1 THROUGH 5	3	AA
INPUT	C-----WITH VARIOUS PORTIONS OF IT BEING ACTIVATED FOR THE DIFFERENT	4	AA
INPUT	C-----CASES.	5	AA
INPUT	C	6	AA
INPUT	BCS BOXINR	7	AA
INPUT	S SURFN = 1	8	AA
INPUT	TYPE = RECT	9	AA
INPUT	ACTIVE = BOTTOM	10	AA
INPUT	PROP = 0.9,0.9	11	AA
INPUT	P1 = 1.0, 0.0, 1.0	12	AA
INPUT	P2 = 1.0, 0.0, 0.0	13	AA
INPUT	P3 = 1.0, 1.0, 0.0	14	AA
INPUT	COM = * INNER RIGHT FRONT *	15	AA
INPUT	S SURFN = 2	16	AA
INPUT	TYPE = RECT	17	AA
INPUT	ACTIVE = BOTTOM	18	AA
INPUT	PROP = 0.9,0.9	19	AA
INPUT	P1 = 1.0, 1.0, 1.0	20	AA
INPUT	P2 = 1.0, 1.0, 0.0	21	AA
INPUT	P3 = 0.0, 1.0, 0.0	22	AA
INPUT	COM = * INNER RIGHT SIDE *	23	AA
INPUT	S SURFN = 3	24	AA
INPUT	TYPE = RECT	25	AA
INPUT	ACTIVE = TOP	26	AA
INPUT	PROP = 0.9,0.9	27	AA
INPUT	P1 = 0.0, 0.0, 1.0	28	AA
INPUT	P2 = 0.0, 0.0, 0.0	29	AA
INPUT	P3 = 0.0, 1.0, 0.0	30	AA
INPUT	COM = * INNER RIGHT BACK *	31	AA
INPUT	S SURFN = 4	32	AA
INPUT	TYPE = RECT	33	AA
INPUT	ACTIVE = TOP	34	AA
INPUT	PROP = 0.9,0.9	35	AA
INPUT	P1 = 1.0, 1.0, 0.0	36	AA
INPUT	COM = * INNER RIGHT BOTTOM *	37	AA
INPUT	BCS BOXINL,IMGBCS=BOXINR,NINC=10,IREFSF=1000	38	AA
INPUT	C	39	AA
INPUT	C-----THE FOREGOING CARD IMACES BCS BOXINR IN REFERENCE PLANE 1000	40	AA
INPUT	C-----TO CREATE BCS BOXINL. THE INTERIOR OF THE BOX WAS INPUT IN	41	AA
INPUT	C-----THIS MANNER TO FACILITATE THE INPUT OF SAMPLE CASE 4 TO SHOW	42	AA
INPUT	C-----THE USE OF 'MESS' AND 'ERN' NODES.	43	AA
INPUT	C	44	AA

IMAGING SURFACE (1) BCS (BOXINR), GENERATING SURFACE (11) BCS (BOXINL)
IMAGING SURFACE (2) BCS (BOXINR), GENERATING SURFACE (12) BCS (BOXINL)
IMAGING SURFACE (3) BCS (BOXINR), GENERATING SURFACE (13) BCS (BOXINL)

MODEL = SAMPLE
SURFACE DATA INPUT BLOCK

SAMPLE CASE 5 - FFCAL/RBCAL/GDCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

		IMAGING SURFACE (4) BCS (BOXINR). GENERATING SURFACE (14) BCS (BOXINL)		
INPUT	R	REFNO = 1000	45	AA
INPUT		P1 = 1.0, 0.0, 1.0	46	AA
INPUT		P2 = 1.0, 0.0, 0.0	47	AA
INPUT		P3 = 0.0, 0.0, 0.0	48	AA
INPUT		COM = * IMAGING PLANE *	49	AA
INPUT	BCS	LIDINR	50	AA
INPUT	S	SURFN = 5	51	AA
INPUT		TYPE = RECT	52	AA
INPUT		ACTIVE = BOTTOM	53	AA
INPUT		PROP = 0.9,0.9	54	AA
INPUT		P1 = 1.0, 1.0, 0.0	55	AA
INPUT		COM = * INNER RIGHT LID *	56	AA
INPUT	S	SURFN = 15	57	AA
INPUT		IMAGSF = 5	58	AA
INPUT		IREFSF = 1000	59	AA
INPUT		COM = * INNER LEFT LID *	60	AA
INPUT	BCS	BOXOUT	61	AA
INPUT	S	SURFN = 21	62	AA
INPUT		TYPE = BOX3	63	AA
INPUT		ACTIVE = OUT	64	AA
INPUT		SHADE = NO	65	AA
INPUT		PROP = 0.2,0.9	66	AA
INPUT		P1 = 1.01,-1.01, 1.01	67	AA
INPUT		P2 = 1.01, 1.01, 1.01	68	AA
INPUT		P3 = -0.01, 1.01, 1.01	69	AA
INPUT		P4 = -0.01, 1.01,-0.01	70	AA
INPUT		COM = * OUTER SURFACES *	71	AA
INPUT	BCS	LIDOUT	72	AA
INPUT	S	SURFN = 26	73	AA
INPUT		TYPE = RECT	74	AA
INPUT		ACTIVE = TOP	75	AA
INPUT		SHADE = NO	76	AA
INPUT		PROP = 0.2,0.9	77	AA
INPUT		P1 = 1.01,-1.01, 0.01	78	AA
INPUT		P2 = 1.01, 1.01, 0.01	79	AA
INPUT		P3 = -0.01, 1.01, 0.01	80	AA
INPUT		COM = * OUTER SURFACE OF LID *	81	AA
INPUT	C		82	AA
INPUT		C-----THE NEXT TWO BCS'S (MESSR AND MESSL) ARE ACTIVATED IN SAMPLE	83	AA
INPUT		C-----CASE 4 ONLY.	84	AA
INPUT	C		85	AA
INPUT	BCS	MESSR	86	AA
INPUT	S	SURFN = 101	87	AA
INPUT		TYPE = RECT	88	AA
INPUT		ACTIVE = TOP	89	AA
INPUT		PROP = 1.0,1.0	90	AA

DATE 062870 TIME 014544 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 6 VERSION PAGE 7

MODEL = SAMPLE SURFACE DATA INPUT BLOCK SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/DRBCEN/DRCAL/AGCAL/QOCAL

CARD	ORIGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT			P1	=	1.0, 0.0, 1.0													91		AA
INPUT			P2	=	1.0, 0.0, 0.0													92		AA
INPUT			P3	=	0.0, 0.0, 0.0													93		AA
INPUT			COM	=	* PRIMARY MESS NODE, RIGHT SIDE *													94		AA
INPUT	BCS		MESSL															95		AA
INPUT	S		SURFN	=	111													96		AA
INPUT			TYPE	=	RECT													97		AA
INPUT			ACTIVE	=	BOTTOM													98		AA
INPUT			PROP	=	1.0, 1.0													99		AA
INPUT			P1	=	1.0, 0.0, 1.0													100		AA
INPUT			P2	=	1.0, 0.0, 0.0													101		AA
INPUT			P3	=	0.0, 0.0, 0.0													102		AA
INPUT			COM	=	* PRIMARY MESS NODE, LEFT SIDE *													103		AA
INPUT	C																	104		AA
INPUT	C		C-----THE FOLLOWING BCS (LIDSP) IS ACTIVATED IN SAMPLE CASE 5 ONLY.															105		AA
INPUT	C																	106		AA
INPUT	BCS		LIDSP															107		AA
INPUT	S		SURFN	=	200													108		AA
INPUT			TYPE	=	RECT													109		AA
INPUT			ACTIVE	=	BOTTOM													110		AA
INPUT			PROP	=	0.1, 0.1													111		AA
INPUT			SPRI	=	0.8													112		AA
INPUT			SPRS	=	0.8													113		AA
INPUT			P1	=	1.0, -1.0, 0.0													114		AA
INPUT			P2	=	1.0, 1.0, 0.0													115		AA
INPUT			P3	=	0.0, 1.0, 0.0													116		AA
INPUT			COM	=	* SPECULAR LID *													117		AA

DATE 062878 TIME 014958 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 8

MODEL = SAMPLE
BCS DATA INPUT BLOCK SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

CARD	ORIGIN	12345678	1	2345678	2	2345678	3	2345678	4	2345678	5	2345678	6	2345678	7	2345678	8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	HEADER	BCS DATA																118		AA
INPUT	BCS	BOXINR																119		AA
INPUT	BCS	BOXIML																120		AA
INPUT	BCS	LIDIMR	.0..0..1..0..-43..0.															121		AA
INPUT	BCS	BOXOUT																122		AA
INPUT	BCS	LIDOUT	.0..0..1..0..-45..0.															123		AA
INPUT	BCS	MESSR																124		AA
INPUT	BCS	MESSL																125		AA
INPUT	BCS	LIDSP	.0..0..1..0..-45..0.															126		AA

DATE 062878 TIME 015000 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 9

MODEL = SAMPLE SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
FORM FACTOR DATA INPUT BLOCK

CARD ORGIN 12345678 1 2345678 2 2345678 3 2345678 4 2345678 5 2345678 6 2345678 7 2345678 8 EDIT NO. OLD EDIT NO. LABEL

INPUT	HEADER FORM FACTOR DATA	127	AA
INPUT	C	128	AA
INPUT	C-----ENTER KNOWN ZERO FORM FACTORS AND EQUIVALENT FORM FACTORS FOR	129	AA
INPUT	C-----CASE5.	130	AA
INPUT	C	131	AA
INPUT	FIG CASE1	132	AA
INPUT	NODEA 1,2,3,4,11,12,13,14,200,21,22,23,24,25,26,END	133	AA
INPUT	BOTH 21,ZERO	134	AA
INPUT	22,ZERO	135	AA
INPUT	23,ZERO	136	AA
INPUT	24,ZERO	137	AA
INPUT	25,ZERO	138	AA
INPUT	26,ZERO	139	AA
INPUT	1,1,0.	140	AA
INPUT	11,12,1,2	141	AA
INPUT	11,13,1,3	142	AA
INPUT	11,14,1,4	143	AA
INPUT	11,200,1,200	144	AA
INPUT	1,11,0.	145	AA
INPUT	11,2,1,12	146	AA
INPUT	11,3,1,13	147	AA
INPUT	11,4,1,14	148	AA
INPUT	2,2,0.	149	AA
INPUT	2,3,1,2	150	AA
INPUT	2,4,1,4	151	AA
INPUT	12,13,2,3	152	AA
INPUT	12,14,2,4	153	AA
INPUT	12,200,2,200	154	AA
INPUT	12,3,2,13	155	AA
INPUT	12,4,2,14	156	AA
INPUT	3,3,0.	157	AA
INPUT	3,4,1,4	158	AA
INPUT	13,14,3,4	159	AA
INPUT	13,200,3,200	160	AA
INPUT	3,13,0.	161	AA
INPUT	13,4,3,14	162	AA
INPUT	4,4,0.	163	AA
INPUT	14,200,4,200	164	AA
INPUT	4,14,0.	165	AA
INPUT	200,200,0.	166	AA

DATE 062070 TIME 015003 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 0 VERSION PAGE 10

MODEL = SAMPLE CORRESPONDENCE DATA INPUT BLOCK SAMPLE CASE 5 - FFCAL/RBCAL/QBCAL/RKCAL/ORDGEN/DRCAL/QOCAL/QOCAL

CARD ORIGIN	12345670 1 2345670 2 2345670 3 2345670 4 2345670 5 2345670 6 2345670 7 2345670 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	HEADER CORRESPONDENCE DATA			167 AA
INPUT	C			168 AA
INPUT	C-----ENTER CORRESPONDENCE DATA FOR CASE 2			169 AA
INPUT	C			170 AA
INPUT	F10 CASE2			171 AA
INPUT	1 = 1,11,22			172 AA
INPUT	2 = 2,25			173 AA
INPUT	3 = 3,13,24			174 AA
INPUT	4 = 4,14,21			175 AA
INPUT	5 = 5,15,26			176 AA
INPUT	12 = 12,23			177 AA
INPUT	C			178 AA
INPUT	C-----ENTER CORRESPONDENCE DATA FOR CASE 3 TO COMBINE FORM FACTORS			179 AA
INPUT	C			180 AA
INPUT	F10 CASE3,FF			181 AA
INPUT	1 = 1,11,22			182 AA
INPUT	2 = 2,25			183 AA
INPUT	3 = 3,13,24			184 AA
INPUT	4 = 4,14,21			185 AA
INPUT	5 = 5,15,26			186 AA
INPUT	12 = 12,23			187 AA

DATE 082870 TIME 015005 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 11

MODEL = SAMPLE SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORDGEN/DRCAL/AQCAL/QOCAL
OPERATION DATA INPUT BLOCK (PASS 1)

CARD ORIGIN	12345670 1	2345670 2	2345670 3	2345670 4	2345670 5	2345670 6	2345670 7	2345670 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	HEADER OPERATIONS DATA									188	AA

+++++ OPERATIONS DATA BLOCK (PASS 1) COMPLETE +++++

MODEL = SAMPLE
OPERATION DATA INPUT BLOCK (PASS 2) SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBOEN/DRCAL/AQCAL/QOCAL

CARD	ORIGIN	12345678 1	2345678 2	2345678 3	2345678 4	2345678 5	2345678 6	2345678 7	2345678 8	EDIT NO.	OLD EDIT NO.	LABEL
INPUT	C									180		AA
INPUT	C	----	BUILD THE CASE 5 CONFIGURATION							190		AA
INPUT	C									191		AA
PROG	STEP	-1								0		
INPUT	BUILD	CASE5,BOXINR,BOXINL,LIDSP,BOXOUT,LIDOUT								192		AA
PROG		CALL BUILDG (BOXINR,6HCASE5)								0		
PROG		CALL ADD (BOXINL)								0		
PROG		CALL ADD (LIDSP)								0		
PROG		CALL ADD (BOXOUT)								0		
PROG		CALL ADD (LIDOUT)								0		
INPUT	C									193		AA
INPUT	C	----	CALCULATE THE FORM FACTOR MATRIX.							194		AA
INPUT	C									195		AA
INPUT	L	FFCAL								196		AA
INPUT	C									197		AA
INPUT	C	----	CALCULATE IMAGE FACTORS							198		AA
INPUT	C									199		AA
INPUT		CALL RBDATA(0.0,0.0,0)								200		AA
INPUT	L	RBCAL								201		AA
INPUT	C									202		AA
INPUT	C	----	CALCULATE THE GRAY BODY MATRIX USING IMAGE FACTORS.							203		AA
INPUT	C									204		AA
INPUT		CALL GBDATA(BOTH,0,RB)								205		AA
INPUT	L	GBCAL								206		AA
INPUT	C									207		AA
INPUT	C	----	CALCULATE AND PUNCH RADIATION CONDUCTORS.							208		AA
INPUT	C									209		AA
INPUT		CALL RKDATA(0.0,0.0,SPACE,999,0.0,0.0)								210		AA
INPUT	L	RKCAL								211		AA
INPUT	C									212		AA
INPUT	C	----	DEFINE ORBIT AND VEHICLE ORIENTATION (CIRCULAR-PLANET-ORIENTED)							213		AA
INPUT	C									214		AA
INPUT		CALL ORBIT2(EAR,0.60,0.0,0.0,100.*6080.,100.*6080.)								215		AA
INPUT		CALL ORIENT(4HPLAN,1,2,3,300.,270.,0.)								216		AA
INPUT	C									217		AA
INPUT	C	----	SET AQPRNT TO PRINT THE COMPONENT VALUES OF ABSORBED Q'S.							218		AA
INPUT	C									219		AA
INPUT		AQPRNT = YES								220		AA
INPUT	C									221		AA
INPUT	C	----	CALCULATE INCIDENT FLUXES PLUS SPECULAR REFLECTIONS.							222		AA
INPUT	C									223		AA
PROG	C									0		
PROG		ORBIT GENERATION STARTS HERE								0		
INPUT		CORBOEN CIRP,0.,100.,2,DI								224		AA
PROG	C									0		
PROG	STEP	10000								0		
PROG		TRUEAN = .000								0		
PROG		TRUEANF = 100.000								0		
PROG		TRUEANI = .000								0		

PROG	90300	CONTINUE	•	0	
PROG	90400	CONTINUE	•	0	
PROG	C		•	0	
PROG	C	***** ORBIT GENERATION ENDS HERE *****	•	0	
PROG	C		•	0	
INPUT	STEP	10010		225	AA
INPUT		CALL DRDATA(10000.0)		226	AA
INPUT	L	DRCAL		227	AA
INPUT		CALL AQDATA(0.0,0.0,0)		228	AA
INPUT	L	AQCAL		229	AA
INPUT	C			230	AA
INPUT	STEP	10011		231	AA
INPUT		CALL DRDATA(10001.0)		232	AA
INPUT	L	DRCAL		233	AA
INPUT		CALL AQDATA(0.0,0.0,0)		234	AA
INPUT	L	AQCAL		235	AA
INPUT	C			236	AA
INPUT	STEP	10012		237	AA
INPUT		CALL DRDATA(10002.0)		238	AA
INPUT	L	DRCAL		239	AA
INPUT		CALL AQDATA(0.0,0.0,0)		240	AA
INPUT	L	AQCAL		241	AA
INPUT	C			242	AA
INPUT	STEP	10013		243	AA
INPUT		CALL DRDATA(10003.0)		244	AA
INPUT	L	DRCAL		245	AA
INPUT		CALL AQDATA(0.0,0.0,0)		246	AA
INPUT	L	AQCAL		247	AA
INPUT	C			248	AA
INPUT	STEP	10014		249	AA
INPUT		CALL DRDATA(10004.0)		250	AA
INPUT	L	DRCAL		251	AA
INPUT		CALL AQDATA(0.0,0.0,0)		252	AA
INPUT	L	AQCAL		253	AA
INPUT	C			254	AA
INPUT		CALL QODATA(3HALL,0.0,0.0,0.0,0)		255	AA
INPUT	L	QOCAL		256	AA
INPUT		END OF DATA		257	AA

DATE 062878 TIME 019012 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC/EXC 8 VERSION PAGE 13

MODEL = SAMPLE SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBOEN/DRCAL/AQCAL/QOCAL
PROCESSOR CORE ALLOCATION

THE FOLLOWING IS THE PROCESSOR CORE ALLOCATION FOR THOSE SEGMENTS WHICH WILL BE LOADED IN THIS EXECUTION (APPROX.) ...

OCTAL/DECIMAL

TRASYS (0) SEGMENT	121220/	41618	
OPERATIONS DATA (NOT KNOWN AT THIS TIME).....	175000/	64000	
INITIALIZATION SEGMENT	122300/	42176	
FORM FACTOR SEGMENT	138100/	48192	
DIRECT FLUX SEGMENT	150500/	53568	
GRAY BODY SEGMENT	124000/	43008	
ABSORBED Q-S SEGMENT	122500/	42304	
-QO- SEGMENT	130600/	45440	
REAL BODY SEGMENT	142600/	50560	
RADIATION CONDUCTOR SEGMENT	125300/	43840	
DIRECT FLUX REAL BODY SEGMENT	126000/	44032	
GRAY BODY DYNAMIC COMMON	000276/	180	
-QO- DYNAMIC COMMON	003554/	1900	
RADIATION CONDUCTOR DYNAMIC COMMON	000574/	380	
GRAY BODY MINIMUM - MAXIMUM CORE	123573/	42875 - 123723/	42983
-QO- MINIMUM - MAXIMUM CORE	125147/	43623 - 130557/	45423
RADIATION CONDUCTOR MINIMUM - MAXIMUM CORE	125228/	43870 - 125472/	43834
MINIMUM CORE NEEDED FOR PROCESSOR EXECUTION	150500/	53568	
MAXIMUM CORE NEEDED FOR PROCESSOR EXECUTION	150500/	53568	
AMOUNT OF CORE THAT WILL BE USED BY PROCESSOR .	150500/	53568	

MODEL = SAMPLE SAMPLE CASE 3 - FFCAL/RBCAL/QBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
 WRAP UP OF THE PRE-PROCESSOR

PRE-PROCESSOR ACCOUNTING INFORMATION	CP-SEC	DYN-STORAGE
SOURCE EDITING	1.900	676
DOCUMENTATION DATA PRE-PROCESSING000	0
QUANTITIES DATA PRE-PROCESSING034	268
ARRAY DATA PRE-PROCESSING000	0
SURFACE DATA PRE-PROCESSING (PASS 1) ...	1.832	84
SURFACE DATA PRE-PROCESSING (PASS 2)579	1141
BCS DATA PRE-PROCESSING210	188
FORM FACTOR DATA PRE-PROCESSING665	1038
SHADOW DATA PRE-PROCESSING000	0
FLUX DATA PRE-PROCESSING000	0
CORRESPONDENCE DATA PRE-PROCESSING252	101
OPERATIONS DATA PRE-PROCESSING	4.177	884
SUBROUTINE DATA PRE-PROCESSING302	0
SEQUENTIAL TAPE INITIALIZATION025	0
TOTAL CP TIME FOR PRE-PROCESSOR 10.655 DECIMAL SECONDS OR 000013 OCTAL SECONDS		
MINIMUM DYNAMIC STORAGE NEEDED BY PRE-PROCESSOR .. 1141 DECIMAL WORDS		
DYNAMIC STORAGE AVAILABLE TO PRE-PROCESSOR 10000 DECIMAL WORDS		

NORMAL TERMINATION BY PRE-PROCESSOR

0PHD,BLEP

0AS0.T/S RS0.,8C,RS0,92,RS0 APPENDIX H, CASE 5.

0TEST TNE/1/S3

0JUMP L3
 INTERVENING STATEMENTS SKIPPED

0L3:FREE DATA1.

0FREE 14

NASA/HARTIN HARIETTA
THERMAL RADIATION ANALYSIS SYSTEM
UNIVAC 1110/EXEC 8

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PROCESSOR EXECUTION

VERSION/MODIFICATION ... UL2E6
MODIFICATION DATE 061978
DATE OF RUN 062878
TIME OF RUN 022222
JOB NUMBER RVMH05

DATE 062070 TIME 022228 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 1

MODEL=SAMPLE CONFIG=CASE5 STEP=-1
PROCESSING OPERATIONS DATA

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORDGEN/DRCAL/AQCAL/QOCAL

SEQUENCE	NODE	BCS	AREA	ALPH	ENISS	SURF. TYPE	ACTIVE	-----COMMENTS-----
1	1	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
2	2	BOXINR	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
3	3	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
4	4	BOXINR	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
5	11	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT FRONT
6	12	BOXINL	1.00000	.900	.900	RECTANGLE	BOTTOM	INNER RIGHT SIDE
7	13	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BACK
8	14	BOXINL	1.00000	.900	.900	RECTANGLE	TOP	INNER RIGHT BOTTOM
9	200	LIDSP	2.00000	.100	.100	RECTANGLE	BOTTOM	SPECULAR LID
10	21	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
11	22	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
12	23	BOXOUT	1.04040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
13	24	BOXOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
14	25	BOXOUT	1.04040	.200	.900	RECTANGLE	TOP	OUTER SURFACES
15	26	LIDOUT	2.06040	.200	.900	RECTANGLE	TOP	OUTER SURFACE OF LID

NODE, AREA, AND PROPERTIES ARRAYS HAVE BEEN WRITTEN ON THE -RSO- TAPE
BY -BUILDG- (ACCESS NUMBER = 1)

DATE 062070 TIME 022233

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 2

MODEL=SAMPLE CONFIG=CASE3 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RXCAL/ORBGEN/DRCAL/AQCAL/QOCAL

FORM FACTORS AND COMBINED FORM FACTORS - USER INPUT AND DEFAULT PARAMETERS

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
FFACC	.0500	.0500	ORIENTATION ACCURACY PARAMETER	N/A
FFACCS	.1000	.1000	SHADOWING ACCURACY PARAMETER	N/A
FFMIN	.1-05	1.0E-06	PARAMETER TO ELIMINATE SMALL FORM FACTORS	N/A
FFNOSH	SHAD	SHAD	OVER RIDE SHADOWING PARAMETER	(SHAD,NOSH)
*FFPNCH	NO	NO	PARAMETER TO PUNCH FORM FACTORS	(YES,NO)
FFPRNT	YES	YES	FLAG FOR COMPREHENSIVE FF AND CH PRINT	(YES,NO,FF,CH,RB)
FFRATL	15.0	15.0	RATIO FOR USING SUB-NODE TECHNIQUE	N/A
FFCMB	CORR	CORR	FLAG FOR COMBINING FORM FACTORS	(YES,NO,AUTO,CORR)

* -FFPNCH WILL DEFAULT TO -YES- ON CALCULATED VALUES IF THE -RSO- FILE IS NOT SPECIFIED IN THE OPTIONS DATA BLOCK

DATE 062978 TIME 022234

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 3

MODEL=SAMPLE CONFIG=CASE5 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

SEQUENCE	NODE	AREA	ALPH	ENISS
1	1	1.00000	.900	.900
2	2	1.00000	.900	.900
3	3	1.00000	.900	.900
4	4	1.00000	.900	.900
5	11	1.00000	.900	.900
6	12	1.00000	.900	.900
7	13	1.00000	.900	.900
8	14	1.00000	.900	.900
9	200	2.00000	.100	.100
10	21	2.06040	.200	.900
11	22	2.06040	.200	.900
12	23	1.04040	.200	.900
13	24	2.06040	.200	.900
14	25	1.04040	.200	.900
15	26	2.06040	.200	.900

NUMBER OF NODES = 15 NUMBER OF SURFACES = 9

DATE 062870 TIME 022300

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION

PAGE 4

MODEL=SAMPLE CONFIG=CASE3 STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 3 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(*R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(*UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(*9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) H/SHAD	FIR(J,I) H/SHAD	FSOL(I,J) H/SHAD	FSOL(J,I) H/SHAD	FF(I,J) H/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ	
1	2	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	22.033	1108	1108	*
1	3	CAL	.201522	.201522	.201522	.201522	.201522	1.000000	1.000000	.534	36	36	
1	4	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	22.051	1108	1108	*
1	12	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.300	36	36	
1	13	CAL	.086058	.086058	.086058	.086058	.086058	1.000000	1.000000	.367	36	36	
1	14	CAL	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	21.722	1024	1024	*
1	200	CAL	.193994	.096997	.193994	.096997	.193994	1.000000	1.000000	.407	36	32	
1	FF SUM = .9690		ROW CP TIME = 68.579										
1	FORM FACTOR RESTART (RSO) RECORD = 21												
2	3	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	21.730	1108	1108	*
2	4	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	21.476	1108	1108	*
2	11	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.302	36	36	
2	12	CAL	.068832	.068832	.068832	.068832	.068832	1.000000	1.000000	.366	36	36	
2	13	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.288	36	36	
2	14	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.298	36	36	
2	200	CAL	.132107	.066054	.132107	.066054	.132107	1.000000	1.000000	10.647	657	642	*
2	FF SUM = .9218		ROW CP TIME = 56.148										
2	FORM FACTOR RESTART (RSO) RECORD = 22												
3	4	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	21.903	1108	1108	*
3	11	CAL	.086058	.086058	.086058	.086058	.086058	1.000000	1.000000	.362	36	36	
3	12	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.289	36	36	
3	14	CAL	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	20.978	1024	1024	*
3	200	CAL	.060738	.030369	.060738	.030369	.060738	1.000000	1.000000	10.654	650	640	*
3	FF SUM = .8365		ROW CP TIME = 55.291										
3	FORM FACTOR RESTART (RSO) RECORD = 23												
4	11	CAL	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	20.992	1024	1024	*

DATE 062670 TIME 022702

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC @ VERSION

PAGE

5

MODEL=SAFPLE CONFIO=CASES STEP=-1
FORM FACTOR CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/DRBGEN/DRCAL/AQCAL/QOCAL

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)

(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)

(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) M/SHAD	FIR(J,I) M/SHAD	FSOL(I,J) M/SHAD	FSOL(J,I) M/SHAD	FF(I,J) M/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
4	12	CAL	.032922	.032922	.032922	.032922	.032922	1.000000	1.000000	.282	38	38
4	13	CAL	.040501	.040501	.040501	.040501	.040501	1.000000	1.000000	21.150	1024	1024
4	200	CAL	.164809	.082404	.164809	.082404	.164809	1.000000	1.000000	.392	36	32
4	FF SUM = .9009 ROW CP TIME = 43.989 FORM FACTOR RESTART (RSO) RECORD = 24											
11	12	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	17.885	1108	1108
11	13	CAL	.201522	.201522	.201522	.201522	.201522	1.000000	1.000000	.427	36	36
11	14	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	16.517	1108	1108
11	200	CAL	.193994	.096997	.193994	.096997	.193994	1.000000	1.000000	.343	38	32
11	FF SUM = .9698 ROW CP TIME = 35.989 FORM FACTOR RESTART (RSO) RECORD = 25											
12	13	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	16.572	1108	1108
12	14	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	16.400	1108	1108
12	200	CAL	.132107	.066054	.132107	.066054	.132107	1.000000	1.000000	7.993	657	642
12	FF SUM = .9218 ROW CP TIME = 41.774 FORM FACTOR RESTART (RSO) RECORD = 26											
13	14	CAL	.207379	.207379	.207379	.207379	.207379	1.000000	1.000000	16.951	1108	1108
13	200	CAL	.060738	.030369	.060738	.030369	.060738	1.000000	1.000000	8.294	650	640
13	FF SUM = .8365 ROW CP TIME = 26.056 FORM FACTOR RESTART (RSO) RECORD = 27											
14	200	CAL	.164809	.082404	.164809	.082404	.164809	1.000000	1.000000	.324	36	32

DATE 062070 TIME 023059 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 8

MODEL=SAFPLE CONFIG=CASE5 STEP=-1 SAMPLE CASE 5 - FFCAL/RSCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
FORM FACTOR CALCULATION LINK.

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUES OF RSI, RTI, OR CARD INPUT)
(9.999999 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
14		FF SUM = .9009 FORM FACTOR RESTART										
			ROW CP TIME =		1.115							
			(RSO) RECORD =	28								
200		FF SUM = .5518 FORM FACTOR RESTART										
			ROW CP TIME =	.654								
			(RSO) RECORD =	29								
21		FF SUM = .0000 FORM FACTOR RESTART										
			ROW CP TIME =	.502								
			(RSO) RECORD =	30								
22		FF SUM = .0000 FORM FACTOR RESTART										
			ROW CP TIME =	.386								
			(RSO) RECORD =	31								
23		FF SUM = .0000 FORM FACTOR RESTART										
			ROW CP TIME =	.334								
			(RSO) RECORD =	32								
24		FF SUM = .0000 FORM FACTOR RESTART										
			ROW CP TIME =	.201								
			(RSO) RECORD =	33								

DATE 062970 TIME 023105 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 7

MODEL=SAMPLE CONFIG=CASE5 STEP=-1 SAMPLE CASE 5 - FFCAL/RBCAL/QBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
FORM FACTOR CALCULATION LINK.

(* -INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R -INDICATES FF CALCULATED FROM NODE J TO NODE I BECAUSE NODE J HAS SMALLEST AREA)
(UN-INDICATES UNKNOWN CALCULATION MODE BECAUSE OF RSI, RTI, OR CARD INPUT)
(0.000000 -INDICATES UNKNOWN DATA VALUE BECAUSE OF INSUFFICIENT CARD INPUT)

NODE I	NODE J	COMPUTATION	FIR(I,J) W/SHAD	FIR(J,I) W/SHAD	FSOL(I,J) W/SHAD	FSOL(J,I) W/SHAD	FF(I,J) W/SHAD	SHAD.IR FACTOR	SHAD.SOL FACTOR	CP TIME (SEC)	NEI	NEJ
25		FF SUM = .0000 FORM FACTOR RESTART (RSO) RECORD =								.145 34		
28		FF SUM = .0000 FORM FACTOR RESTART (RSO) RECORD =								.000 35		

FF FORM FACTORS FOR CONFIGURATION CASE5 HAVE BEEN STORED ON RSO.
LAST RESTART RECORD WRITTEN = 35

DATE 062870 TIME 023105 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 0

MODEL=SAMPLE CONFIG=CASE5 STEP=-1 SAMPLE CASE 5 - FFCAL/RSCAL/0BCAL/RACAL/0R0GEN/0R0CAL/AQCAL/Q0CAL
FORM FACTOR CALCULATION LINK.

SUMMARY OF FORM FACTOR SUMS FOR ALL NODES

NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM	NODE 1- FF SUM
1- .9698	2- .9218	3- .8365	4- .9009	11- .9698	12- .9218
13- .8365	14- .9009	200- .5518	21- .0000	22- .0000	23- .0000
24- .0000	25- .0000	26- .0000			

TOTAL TIME FOR FORM FACTOR SEGMENT 331.794

TOTAL TIME SINCE START OF RUN 395.910

DATE 062070 TIME 023106

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 9

MODEL=SAMPLE CONFIG=CASE5 STEP=-1
IMAGE FACTOR CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

NODE	AREA	ALPH	ENISS	SPECULAR REFL(SOL)	SPECULAR REFL(IR)
1	1.00000	.900+00	.900+00	.000	.000
2	1.00000	.900+00	.900+00	.000	.000
3	1.00000	.900+00	.900+00	.000	.000
4	1.00000	.900+00	.900+00	.000	.000
11	1.00000	.900+00	.900+00	.000	.000
12	1.00000	.900+00	.900+00	.000	.000
13	1.00000	.900+00	.900+00	.000	.000
14	1.00000	.900+00	.900+00	.000	.000
200	2.00000	.100+00	.100+00	.800+00	.800+00
21	2.06040	.200+00	.900+00	.000	.000
22	2.06040	.200+00	.900+00	.000	.000
23	1.04040	.200+00	.900+00	.000	.000
24	2.06040	.200+00	.900+00	.000	.000
25	1.04040	.200+00	.900+00	.000	.000
26	2.06040	.200+00	.900+00	.000	.000

NUMBER OF NODES = 15 NUMBER OF SURFACES = 9

DATE 062070 TIME 023106

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION

PAGE 10

MODEL=SAMPLE CONFIG=CASE5 STEP=-1

SAMPLE CASE 5 - FFCAL/RBCAL/QBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

IMAGE FACTOR CALCULATION LINK.

(0 INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
 (R INDICATES FF CALCULATED FROM J TO I)

NODE I	NODE J	COMPUTATION	IFE(I,J) W/SHAD	IFE(J,I) W/SHAD	IFA(I,J) W/SHAD	CP TIME (SEC)
1	1	CAL.	.053297	.053297	.053297	.166
1	2	CAL.	.221283	.221283	.221283	.292
1	3	CAL.	.201522	.201522	.201522	.366
1	4	CAL.	.217091	.217091	.217091	.472
1	11	CAL.	.037057	.037057	.037057	.617
1	12	CAL.	.049448	.049448	.049448	.737
1	13	CAL.	.086058	.086058	.086058	.805
1	14	CAL.	.047559	.047559	.047559	.929
1	200	CAL.	.193994	.096997	.193994	.937
1		ROW CP TIME =	.988	-	RECT	INNER RIGHT FRONT
1		ROW RESTART RECORD =	37.			HAS BEEN WRITTEN TO THE RSO FILE
1		ROW CP TIME =	1.007	+	RECT	INNER RIGHT FRONT
1		ROW RESTART RECORD =	39.			HAS BEEN WRITTEN TO THE RSO FILE
2	3	CAL.	.207379	.207379	.207379	.131
2	4	CAL.	.208765	.208765	.208765	.243
2	11	CAL.	.049448	.049448	.049448	.373
2	12	CAL.	.077642	.077642	.077642	.481
2	13	CAL.	.032922	.032922	.032922	.557
2	14	CAL.	.034983	.034983	.034983	.651
2	200	CAL.	.132107	.066054	.132107	.659
2		ROW CP TIME =	.711	-	RECT	INNER RIGHT SIDE
2		ROW RESTART RECORD =	38.			HAS BEEN WRITTEN TO THE RSO FILE
2		ROW CP TIME =	.734	+	RECT	INNER RIGHT SIDE
2		ROW RESTART RECORD =	39.			HAS BEEN WRITTEN TO THE RSO FILE
3	4	CAL.	.207379	.207379	.207379	.106
3	11	CAL.	.086058	.086058	.086058	.171
3	12	CAL.	.032922	.032922	.032922	.217
3	14	CAL.	.040501	.040501	.040501	.309
3	200	CAL.	.060738	.030369	.060738	.317
3		ROW CP TIME =	.364	+	RECT	INNER RIGHT BACK
3		ROW RESTART RECORD =	39.			HAS BEEN WRITTEN TO THE RSO FILE
3		ROW CP TIME =	.383	+	RECT	INNER RIGHT BACK
3		ROW RESTART RECORD =	40.			HAS BEEN WRITTEN TO THE RSO FILE

DATE 062070 TIME 023113

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 11

MODEL=SAMPLE CONFIG=CASE3 STEP=-1
IMAGE FACTOR CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

(* INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R INDICATES FF CALCULATED FROM J TO I)

NODE I	NODE J	COMPUTATION	IFE(I,J) M/SHAD	IFE(J,I) M/SHAD	IFA(I,J) W/SHAD	CP TIME (SEC)
4	11	CAL.	.047559	.047559	.047559	.204
4	12	CAL.	.034983	.034983	.034983	.328
4	13	CAL.	.040501	.040501	.040501	.394
4	200	CAL.	.164809	.082404	.164809	.498
4		ROW CP TIME =	.546	+	RECT	INNER RIGHT BOTTOM
4		ROW RESTART RECORD =	40, HAS BEEN WRITTEN TO THE RSO FILE			
4		ROW CP TIME =	.563	+	RECT	INNER RIGHT BOTTOM
4		ROW RESTART RECORD =	41, HAS BEEN WRITTEN TO THE RSO FILE			
11	11	CAL.	.053297	.053297	.053297	.137
11	12	CAL.	.221283	.221283	.221283	.254
11	13	CAL.	.201522	.201522	.201522	.323
11	14	CAL.	.217091	.217091	.217091	.441
11	200	CAL.	.193994	.096997	.193994	.448
11		ROW CP TIME =	.482	-	RECT	INNER RIGHT FRONT
11		ROW RESTART RECORD =	41, HAS BEEN WRITTEN TO THE RSO FILE			
11		ROW CP TIME =	.499	+	RECT	INNER RIGHT FRONT
11		ROW RESTART RECORD =	42, HAS BEEN WRITTEN TO THE RSO FILE			
12	13	CAL.	.207379	.207379	.207379	.137
12	14	CAL.	.208765	.208765	.208765	.247
12	200	CAL.	.132107	.066054	.132107	.259
12		ROW CP TIME =	.310	-	RECT	INNER RIGHT SIDE
12		ROW RESTART RECORD =	42, HAS BEEN WRITTEN TO THE RSO FILE			
12		ROW CP TIME =	.331	+	RECT	INNER RIGHT SIDE
12		ROW RESTART RECORD =	43, HAS BEEN WRITTEN TO THE RSO FILE			
13	14	CAL.	.207379	.207379	.207379	.101
13	200	CAL.	.060738	.030369	.060738	.109
13		ROW CP TIME =	.160	+	RECT	INNER RIGHT BACK
13		ROW RESTART RECORD =	43, HAS BEEN WRITTEN TO THE RSO FILE			

DATE 062878 TIME 023118

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 12

MODEL=SAFPLE CONFIO=CASE5 STEP=-1
IMAGE FACTOR CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

(* INDICATES NODE PAIR HAS BEEN SUBDIVIDED)
(R INDICATES FF CALCULATED FROM J TO I)

NODE I	NODE J	COMPUTATION	IFE(I,J) W/SHAD	IFE(J,I) W/SHAD	IFA(I,J) W/SHAD	CP TIME (SEC)
13		ROW CP TIME =	.199	+	RECT	INNER RIGHT BACK
13		ROW RESTART RECORD =	44.	HAS BEEN WRITTEN TO THE RSO FILE		
14	200	CAL.	.164809	.082404	.164809	.119
14		ROW CP TIME =	.170	+	RECT	INNER RIGHT BOTTOM
14		ROW RESTART RECORD =	44.	HAS BEEN WRITTEN TO THE RSO FILE		
14		ROW CP TIME =	.188	+	RECT	INNER RIGHT BOTTOM
14		ROW RESTART RECORD =	45.	HAS BEEN WRITTEN TO THE RSO FILE		
200		ROW CP TIME =	.067	-	RECT	SPECULAR LID
200		ROW RESTART RECORD =	45.	HAS BEEN WRITTEN TO THE RSO FILE		
200		ROW CP TIME =	.087	+	RECT	SPECULAR LID
200		ROW RESTART RECORD =	46.	HAS BEEN WRITTEN TO THE RSO FILE		
21		ROW CP TIME =	.054	+	RECT	OUTER SURFACES
21		ROW RESTART RECORD =	46.	HAS BEEN WRITTEN TO THE RSO FILE		
21		ROW CP TIME =	.076	+	RECT	OUTER SURFACES
21		ROW RESTART RECORD =	47.	HAS BEEN WRITTEN TO THE RSO FILE		
22		ROW CP TIME =	.054	+	RECT	OUTER SURFACES
22		ROW RESTART RECORD =	47.	HAS BEEN WRITTEN TO THE RSO FILE		
22		ROW CP TIME =	.071	+	RECT	OUTER SURFACES
22		ROW RESTART RECORD =	48.	HAS BEEN WRITTEN TO THE RSO FILE		

DATE 062070 TIME 023120

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 13

MODEL=SAMPLE CONFIG=CASE5 STEP=1
IMAGE FACTOR CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

(0 INDICATES NODE PAIR HAS BEEN SUBDIVIDED)

(R INDICATES FF CALCULATED FROM J TO I)

NODE I	NODE J	COMPUTATION	IFE(I,J) W/SHAD	IFE(J,I) W/SHAD	IFA(I,J) W/SHAD	CP TIME (SEC)
23		ROW CP TIME =	.088	+	RECT	OUTER SURFACES
23		ROW RESTART RECORD =	48			HAS BEEN WRITTEN TO THE RSO FILE
23		ROW CP TIME =	.088	+	RECT	OUTER SURFACES
23		ROW RESTART RECORD =	49			HAS BEEN WRITTEN TO THE RSO FILE
24		ROW CP TIME =	.021	+	RECT	OUTER SURFACES
24		ROW RESTART RECORD =	49			HAS BEEN WRITTEN TO THE RSO FILE
24		ROW CP TIME =	.038	+	RECT	OUTER SURFACES
24		ROW RESTART RECORD =	50			HAS BEEN WRITTEN TO THE RSO FILE
25		ROW CP TIME =	.023	+	RECT	OUTER SURFACES
25		ROW RESTART RECORD =	50			HAS BEEN WRITTEN TO THE RSO FILE
25		ROW CP TIME =	.042	+	RECT	OUTER SURFACES
25		ROW RESTART RECORD =	51			HAS BEEN WRITTEN TO THE RSO FILE
26		ROW CP TIME =	.013	+	RECT	OUTER SURFACE OF LID
26		ROW RESTART RECORD =	51			HAS BEEN WRITTEN TO THE RSO FILE
26		ROW CP TIME =	.037	+	RECT	OUTER SURFACE OF LID
26		ROW RESTART RECORD =	52			HAS BEEN WRITTEN TO THE RSO FILE

TOTAL CP TIME (SEC) FOR PROBLEM = 4.712

DATE 062878 TIME 023122 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 14

MODEL=SAMPLE CONFIG=CASE5 STEP=-1 SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
GRAY BODIES COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	GREY BODIES DEFINITION	OPTIONS
GBWBND	BOTH	BOTH	WAVEBAND DEFINITION PARAMETER	(2HIR,3HSOL,4HBOTH)

.....

IR GRAY BODIES FOR CONFIGURATION CASE5 HAVE BEEN COMPUTED AND STORED ON RSO.
LAST RESTART RECORD WRITTEN = 69

.....

.....

SOL GRAY BODIES FOR CONFIGURATION CASE5 HAVE BEEN COMPUTED AND STORED ON RSO.
LAST RESTART RECORD WRITTEN = 88

.....

TOTAL TIME TO COMPUTE GRAY BODIES .83

DATE 062079 TIME 023133

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 15

MODEL=SAMPLE CONFIG=CASE5 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 5 - FFCAL/RDCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

VARIABLE NAME	CURRENT VALUE	DEFAULT	RADIATION CONDUCTORS DEFINITION	OPTIONS
RKPRCH	PUN	NO	PUNCH/NO PUNCH PARAMETER FOR RADKS	(YES.NO)
RKHIN	.0001	0.0001	PARAMETER TO ELIMINATE SMALL RADK S	N/A
IRKCN	1	1	INITIAL RADIATION CONDUCTOR ID NUMBER	N/A
RKSP	SPACE	NO	MNEMONIC FLAG FOR COMPUTATION OF RADKS TO SPACE	(SPACE.NO)
IRKNSP	999	32767	SPACE NODE ID NUMBER	N/A
SIGMA	.17-08	1.713E-9	STEFAN-BOLTZMANN CONSTANT	N/A
RKAMPF	1.00	1.0	AREA MULTIPLYING FACTOR	N/A
RKTAPE	NO	NO	PARAMETER TO OUTPUT TO BCD TAPE	(TAPE.NO)
RFRAC	.7+00	0.7	SIGNIFICANT RADIATION FRACTION	(0. TO 1.)
RTOL	.990	0.99	DECIMAL FRACTION OF LAST RADK SAVED	N/A
NERN	0	0	EFFECTIVE RADIATION NODE (ERN) NUMBER	N/A

DATE 062078 TIME 023133 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 18

MODEL=SAMPLE CONFIG=CASE5 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

SPECIAL RADIATION NODES

NONE

MESS SPECIAL NODES

PRIMARY SECONDARY

NONE

MODEL=SAMPLE CONFIG=CASE5 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

RADIATION CONDUCTOR (RADKS) CARDS

AREA UNITS = INPUT UNITS * AHPP, WHERE AHPP = 1.00000

PUNCHED AND/OR BCD0U RADKS -	-	1.	1.	2.	.32562-09\$
PUNCHED AND/OR BCD0U RADKS -	-	2.	1.	3.	.29703-09\$
PUNCHED AND/OR BCD0U RADKS -	-	3.	1.	4.	.31982-09\$
PUNCHED AND/OR BCD0U RADKS -	-	4.	1.	11.	.66666-10\$
PUNCHED AND/OR BCD0U RADKS -	-	5.	1.	12.	.81362-10\$
PUNCHED AND/OR BCD0U RADKS -	-	6.	1.	13.	.12813-09\$
PUNCHED AND/OR BCD0U RADKS -	-	7.	1.	14.	.76972-10\$
PUNCHED AND/OR BCD0U RADKS -	-	8.	1.	200.	.31877-10\$
PUNCHED AND/OR BCD0U RADKS -	-	9.	2.	3.	.30306-09\$
PUNCHED AND/OR BCD0U RADKS -	-	10.	2.	4.	.30618-09\$
PUNCHED AND/OR BCD0U RADKS -	-	11.	2.	11.	.81362-10\$
PUNCHED AND/OR BCD0U RADKS -	-	12.	2.	12.	.11709-09\$
PUNCHED AND/OR BCD0U RADKS -	-	13.	2.	13.	.55689-10\$
PUNCHED AND/OR BCD0U RADKS -	-	14.	2.	14.	.58420-10\$
PUNCHED AND/OR BCD0U RADKS -	-	15.	2.	200.	.22359-10\$
PUNCHED AND/OR BCD0U RADKS -	-	16.	3.	4.	.30264-09\$
PUNCHED AND/OR BCD0U RADKS -	-	17.	3.	11.	.12813-09\$
PUNCHED AND/OR BCD0U RADKS -	-	18.	3.	12.	.55689-10\$
PUNCHED AND/OR BCD0U RADKS -	-	19.	3.	13.	.10153-10\$
PUNCHED AND/OR BCD0U RADKS -	-	20.	3.	14.	.63760-10\$
PUNCHED AND/OR BCD0U RADKS -	-	21.	3.	200.	.11499-10\$
PUNCHED AND/OR BCD0U RADKS -	-	22.	4.	11.	.76972-10\$
PUNCHED AND/OR BCD0U RADKS -	-	23.	4.	12.	.58420-10\$
PUNCHED AND/OR BCD0U RADKS -	-	24.	4.	13.	.63760-10\$
PUNCHED AND/OR BCD0U RADKS -	-	25.	4.	14.	.10041-10\$
PUNCHED AND/OR BCD0U RADKS -	-	26.	4.	200.	.27106-10\$
PUNCHED AND/OR BCD0U RADKS -	-	27.	11.	12.	.32562-09\$
PUNCHED AND/OR BCD0U RADKS -	-	28.	11.	13.	.29703-09\$
PUNCHED AND/OR BCD0U RADKS -	-	29.	11.	14.	.31982-09\$
PUNCHED AND/OR BCD0U RADKS -	-	30.	11.	200.	.31877-10\$
PUNCHED AND/OR BCD0U RADKS -	-	31.	12.	13.	.30306-09\$
PUNCHED AND/OR BCD0U RADKS -	-	32.	12.	14.	.30618-09\$
PUNCHED AND/OR BCD0U RADKS -	-	33.	12.	200.	.22359-10\$
PUNCHED AND/OR BCD0U RADKS -	-	34.	13.	14.	.30264-09\$
PUNCHED AND/OR BCD0U RADKS -	-	35.	13.	200.	.11499-10\$
PUNCHED AND/OR BCD0U RADKS -	-	36.	14.	200.	.27106-10\$
PUNCHED AND/OR BCD0U RADKS -	-	37.	1.	999.	.11470-09\$
PUNCHED AND/OR BCD0U RADKS -	-	38.	2.	999.	.24900-09\$
PUNCHED AND/OR BCD0U RADKS -	-	39.	3.	999.	.34933-09\$
PUNCHED AND/OR BCD0U RADKS -	-	40.	4.	999.	.35431-09\$

DATE 062878 TIME 023134

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS), UNIVAC EXEC D VERSION PAGE 10

MODEL=SAMPLE CONFIG=CASE5 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

RADIATION CONDUCTOR (RADK) CARDS

AREA UNITS = INPUT UNITS * AMPF, WHERE AMPF = 1.00000

PUNCHED AND/OR BCD0U RADKS -	-	41,	11,	999,	.11470-09\$
PUNCHED AND/OR BCD0U RADKS -	-	42,	12,	999,	.24900-09\$
PUNCHED AND/OR BCD0U RADKS -	-	43,	13,	999,	.34933-09\$
PUNCHED AND/OR BCD0U RADKS -	-	44,	14,	999,	.35431-09\$
PUNCHED AND/OR BCD0U RADKS -	-	45,	200,	999,	.15660-09\$
PUNCHED AND/OR BCD0U RADKS -	-	46,	21,	999,	.31765-08\$
PUNCHED AND/OR BCD0U RADKS -	-	47,	22,	999,	.31765-08\$
PUNCHED AND/OR BCD0U RADKS -	-	48,	23,	999,	.16040-08\$
PUNCHED AND/OR BCD0U RADKS -	-	49,	24,	999,	.31765-08\$
PUNCHED AND/OR BCD0U RADKS -	-	50,	25,	999,	.16040-08\$
PUNCHED AND/OR BCD0U RADKS -	-	51,	26,	999,	.31765-08\$

DATE 062678 TIME 023135

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 19

MODEL=SAMPLE CONFIG=CASE5 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE BEFORE RKM IN SCREENING

1 - .10000+01	2 - .10000+01	3 - .10000+01	4 - .10000+01	11 - .10000+01	12 - .10000+01
13 - .10000+01	14 - .10000+01	200 - .10000+01	21 - .10000+01	22 - .10000+01	23 - .10000+01
24 - .10000+01	25 - .10000+01	26 - .10000+01			

DATE 062079 TIME 023135

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION 1 PAGE 20

MODEL=SAHPLE CONFIG=CASE5 STEP=-1
RADIATION CONDUCTOR GENERATION LINK.

SAMPLE CASE 5 - FFCAL/RDCAL/OBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

CONSERVATION CHECKS
RADIATION SUMS FOR EACH NODE AFTER RKHIN SCREENING

1 - .10000+01	2 - .10000+01	3 - .10000+01	4 - .10000+01	11 - .10000+01	12 - .10000+01
13 - .10000+01	14 - .10000+01	200 - .10000+01	21 - .10000+01	22 - .10000+01	23 - .10000+01
24 - .10000+01	25 - .10000+01	26 - .10000+01			

TOTAL TIME TO COMPUTE AND CONDENSE RADKS = .57

MODEL=SAMPLE CONFIG=CASE5 STEP=10000 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
DIRECT IRRADIATION CALCULATION LINK.

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
0	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX,IROTY,IROTZ		1 2 3	
.300+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.300+02	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCW=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCW POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062070 TIME 023137

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE5 STEP=10000

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

DIRECT IRRADIATION CALCULATION LINK.

+++++ NSTEP NO = 10000

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	HSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DATE 062870 TIME 023130

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 23

MODEL=SAMPLE CONFIG=CASE5 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10000 TRUE ANOMALY = .00000 TIME = .00000
++++ IN THE SUM +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	CALC	.001	9	0
2	.94028+02	.18576+03	.5062	CALC	.089	81	4
3	.00000	.10725+03	.0000	CALC	.130	64	7
4	.16512+03	.37152+03	.4444	CALC	.199	81	8
11	.00000	.00000	.0000	CALC	.209	9	0
12	.00000	.00000	.0000	CALC	.219	9	0
13	.10055+02	.10725+03	.0938	CALC	.266	64	6
14	.91734+02	.37152+03	.2489	CALC	.330	81	7
200	.00000	.00000	.0000	CALC	.340	8	0
21	.00000	.00000	.0000	CALC	.350	8	0
22	.10725+03	.10725+03	1.0000	CALC	.429	66	9
23	.18576+03	.18576+03	1.0000	CALC	.503	81	6
24	.00000	.00000	.0000	CALC	.514	8	0
25	.00000	.00000	.0000	CALC	.525	9	0
26	.18687+03	.18687+03	1.0000	CALC	.633	78	9

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RTI, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 403.015 SECONDS
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 91

DATE 062070 TIME 023140

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 24

MODEL=SAMPLE CONFIG=CASE5 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10000 TRUE ANOMALY = .00000 TIME = .00000
++++ IN THE SUN +++++

NODE NUMBER	COMPUT	---DIRECT INCID. ALBEDO	FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	--SHADOW FACTORS-- ALBEDO PLAN	CP TIME (SECONDS)	--ELEMENTS-- PLAN SURF	SHAD SURF
1	CALC	.000	.000	.391+02	.268+02	.000 .000	.000	66 9	7
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 93									
2	CALC	.000	.000	.400+02	.264+02	.000 .000	.470	66 9	5
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 95									
3	CALC	.000	.000	.402+02	.268+02	.000 .000	.895	61 9	7
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 97									
4	CALC	.000	.000	.000	.000	.000 .000	.975	1 9	7
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 99									
11	CALC	.000	.000	.391+02	.268+02	.000 .000	1.389	66 9	7
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 101									
12	CALC	.000	.000	.382+02	.264+02	.000 .000	1.821	66 9	5
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 103									
13	CALC	.000	.000	.402+02	.268+02	.000 .000	2.280	61 9	7
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 105									
14	CALC	.000	.000	.000	.000	.000 .000	2.361	1 9	7
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 107									
200	CALC	.215+02	.144+02	.834+02	.559+02	.258 .257	4.078	133 18	8
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 109									
21	CALC	.110+03	.742+02	.110+03	.742+02	1.000 1.000	6.497	112 18	9
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 111									
22	CALC	.402+02	.268+02	.402+02	.268+02	1.000 1.000	7.070	61 10	9
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 113									
23	CALC	.400+02	.264+02	.400+02	.264+02	1.000 1.000	7.593	66 9	7
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 115									
24	CALC	.391+02	.268+02	.391+02	.268+02	1.000 1.000	8.204	66 10	9
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 117									

DATE 062070 TIME 023156

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION

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MODEL=SAMPLE CONFIG=CASE5 STEP=10000
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RDCAL/OSCAL/RKCAL/ORSGEN/DRCAL/AQCAL/QOCAL

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10000 TRUE ANOMALY = .00000 TIME = .00000
++++ IN THE SUN +++++

MODE NUMBER	COMPUT	---DIRECT INCID. FLUX-- ALBEDO	PLANETARY	---UNSHADOWED FLUX--- ALBEDO	PLANETARY	---SHADOW FACTORS--- ALBEDO	FLAN	CP TIME (SECONDS)	---ELEMENTS--- PLAN	SURF	SHAD SURF
25	CALC	.382+02	.264+02	.382+02	.264+02	1.000	1.000	9.703	66	9	7
PLANETARY FF HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 119											
26	CALC	.659+01	.457+01	.659+01	.457+01	1.000	1.000	0.973	52	2	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 412.485 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE. LAST RESTART RECORD WRITTEN = 129

DATE 062878 TIME 023159

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 26

MODEL=SAMPLE CONFIG=CASE5 STEP=10001
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS ++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
90.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA ++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA ++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX,IROTY,IROTZ		1 2 3	
.000	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.900+02	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA ++++				
.000	CLOCK ANGLE, DEGREES(ABOUT CCS Z-AXIS CCM=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCM POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062670 TIME 023200 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 27

MODEL=SAMPLE CONFIG=CASE5 STEP=10001 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBOEN/DRCAL/AQCAL/QOCAL
DIRECT IRRADIATION CALCULATION LINK.

***** NSTEP NO = 10001

**** COMPUTED OR INPUT ORBIT DATA ****

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

**** PLANET --EARTH -- DATA ****

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	HDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	HSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DATE 062878 TIME 023201 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 28

MODEL=SAMPLE CONFIG=CASE5 STEP=10001 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/OROGEN/DRCAL/AQCAL/QOCAL
DIRECT IRRADIATION CALCULATION LINK.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10001 TRUE ANOMALY = 90.00000 TIME = .36701
++++ IN THE SUN +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	CALC	.001	9	0
2	.00000	.00000	.0000	CALC	.037	9	0
3	.00000	.42900+03	.0000	CALC	.086	81	7
4	.00000	.00000	.0000	CALC	.097	9	0
11	.00000	.00000	.0000	CALC	.107	9	0
12	.00000	.00000	.0000	CALC	.118	9	0
13	.00000	.42900+03	.0000	CALC	.179	81	7
14	.00000	.00000	.0000	CALC	.189	9	0
200	.30335+03	.30335+03	1.0000	CALC	.283	78	8
21	.00000	.00000	.0000	CALC	.296	8	0
22	.42900+03	.42900+03	1.0000	CALC	.388	78	9
23	.00000	.00000	.0000	CALC	.400	9	0
24	.00000	.00000	.0000	CALC	.411	8	0
25	.00000	.00000	.0000	CALC	.422	9	0
26	.00000	.00000	.0000	CALC	.431	8	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 413.370 SECONDS

DATE 062070 TIME 023203 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 29

MODEL=SAMPLE CONFIG=CASE5 STEP=10001 SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QOCAL
DIRECT IRRADIATION CALCULATION LINK.

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10001 TRUE ANOMALY = 90.00000 TIME = .36701
++++ IN THE SUN +++++

NODE NUMBER	COMPUT	---DIRECT INCID. ALBEDO	FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS-- ALBEDO	PLAN	CP TIME (SECONDS)	---ELEMENTS-- PLAN	SURF	SHAD SURF
1	CALC	.000	.000	.000	.000	.000	.000	.000	66	0	0
2	CALC	.000	.000	.000	.000	.000	.000	.061	66	0	0
3	CALC	.000	.000	.000	.000	.000	.000	.094	81	0	0
4	CALC	.000	.000	.000	.000	.000	.000	.109	1	0	0
11	CALC	.000	.000	.000	.000	.000	.000	.147	66	0	0
12	CALC	.000	.000	.000	.000	.000	.000	.191	66	0	0
13	CALC	.000	.000	.000	.000	.000	.000	.229	61	0	0
14	CALC	.000	.000	.000	.000	.000	.000	.249	1	0	0
200	CALC	.120+01	.144+02	.465+01	.559+02	.258	.257	.325	133	0	0
21	CALC	.143+01	.742+02	.143+01	.742+02	1.000	1.000	.383	112	0	0
22	CALC	.206+01	.268+02	.206+01	.268+02	1.000	1.000	.423	81	0	0
23	CALC	.638+00	.264+02	.638+00	.264+02	1.000	1.000	.465	66	0	0
24	CALC	.000	.268+02	.000	.268+02	1.000	1.000	.503	66	0	0
25	CALC	.634+00	.264+02	.634+00	.264+02	1.000	1.000	.544	66	0	0
26	CALC	.000	.457+01	.000	.457+01	1.000	1.000	.579	52	0	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 413.997 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 142

DATE 062878 TIME 023207

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 30

MODEL=SAMPLE CONFIG=CASE5 STEP=10002
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RDCAL/OSCAL/RKCAL/ORBOEM/DRCAL/AQCAL/QOCAL

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
180.000	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	MP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	MA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX,IROTY,IROTZ		1 2 3	
.300+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.150+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCH POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062578 TIME 023200

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 31

MODEL=SAMPLE CONFIG=CASE5 STEP=10002
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

+++++ NSTEP NO = 10002

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET OS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	WSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DATE 062070 TIME 023209

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC B VERSION

PAGE 32

MODEL=SAMPLE CONFIG=CASE5 STEP=10002
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/DRBGEN/DRCAL/AQCAL/QOCAL

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10002 TRUE ANOMALY = 180.00000 TIME = .73402
++++ IN THE SHADE ++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	+++++	.000	0	0
2	.00000	.00000	.0000	+++++	.034	0	0
3	.00000	.00000	.0000	+++++	.038	0	0
4	.00000	.00000	.0000	+++++	.045	0	0
11	.00000	.00000	.0000	+++++	.049	0	0
12	.00000	.00000	.0000	+++++	.053	0	0
13	.00000	.00000	.0000	+++++	.058	0	0
14	.00000	.00000	.0000	+++++	.064	0	0
200	.00000	.00000	.0000	+++++	.068	0	0
21	.00000	.00000	.0000	+++++	.072	0	0
22	.00000	.00000	.0000	+++++	.076	0	0
23	.00000	.00000	.0000	+++++	.080	0	0
24	.00000	.00000	.0000	+++++	.084	0	0
25	.00000	.00000	.0000	+++++	.088	0	0
26	.00000	.00000	.0000	+++++	.092	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 414.518 SECONDS

DATE 062070 TIME 023210 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 33

MODEL=SAMPLE CONF10=CASE5 STEP=10002

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

DIRECT IRRADIATION CALCULATION LINK.

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10002 TRUE ANOMALY = 180.00000 TIME = .73402
 ++++ IN THE SHADE ++++

NODE NUMBER	COMPUT	---DIRECT ALBEDO	INCID. FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS-- ALBEDO	PLAN	CP TIME (SECONDS)	---ELEMENTS-- PLAN	SURF	SHAD SURF
1	+++++	.000	.000	.000	.000	.000	.000	.001	0	0	0
2	+++++	.000	.000	.000	.000	.000	.000	.031	0	0	0
3	+++++	.000	.000	.000	.000	.000	.000	.038	0	0	0
4	+++++	.000	.000	.000	.000	.000	.000	.042	0	0	0
11	+++++	.000	.000	.000	.000	.000	.000	.047	0	0	0
12	+++++	.000	.000	.000	.000	.000	.000	.051	0	0	0
13	+++++	.000	.000	.000	.000	.000	.000	.058	0	0	0
14	+++++	.000	.000	.000	.000	.000	.000	.060	0	0	0
200	+++++	.000	.144+02	.000	.000	.000	.000	.065	0	0	0
21	+++++	.000	.742+02	.000	.000	.000	.000	.072	0	0	0
22	+++++	.000	.268+02	.000	.000	.000	.000	.077	0	0	0
23	+++++	.000	.264+02	.000	.000	.000	.000	.081	0	0	0
24	+++++	.000	.268+02	.000	.000	.000	.000	.088	0	0	0
25	+++++	.000	.264+02	.000	.000	.000	.000	.091	0	0	0
26	+++++	.000	.457+01	.000	.000	.000	.000	.095	0	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 414.830 SECONDS

S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 155

DATE 082878 TIME 023213 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 34
 MODEL=SAMPLE CONFIG=CASE5 STEP=10003 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEM/DRCAL/AQCAL/QOCAL
 DIRECT IRRADIATION CALCULATION LINK.

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD.NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
105.720	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- 1ROTX,1ROTY,1ROTZ		1 2 3	
.359+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.104+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCM=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCM POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062878 TIME 023213 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 35
 MODEL=SAMPLE CONFIG=CASE5 STEP=10003 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
 DIRECT IRRADIATION CALCULATION LINK.

+++++ NSTEP NO = 10003

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.000	STAR CIGHAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET OS EMISS POWER	HOS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	HSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAY CONSTANT	GRAY		.42900+03	SOLAR CONSTANT AT PSD	SOL

DATE 062870 TIME 023214 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 36

MODEL=SAMPLE CONFIG=CASE5 STEP=10003 SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/OROGEN/DRCAL/AOCAL/QOCAL
DIRECT IRRADIATION CALCULATION LINK.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10003 TRUE ANOMALY = 105.71977 TIME = .43111
++++ IN THE SUN +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	CALC	.000	9	0
2	.00000	.69478+01	.0000	CALC	.048	9	4
3	.00000	.41697+03	.0000	CALC	.104	81	7
4	.00000	.00000	.0000	CALC	.114	9	0
11	.00000	.00000	.0000	CALC	.124	9	0
12	.00000	.00000	.0000	CALC	.134	9	0
13	.00000	.41697+03	.0000	CALC	.190	81	7
14	.00000	.00000	.0000	CALC	.200	9	0
200	.24401+03	.36601+03	.6667	CALC	.285	70	8
21	.10066+03	.10066+03	1.0000	CALC	.359	55	9
22	.41698+03	.41698+03	1.0000	CALC	.460	70	9
23	.69478+01	.69478+01	1.0000	CALC	.478	9	5
24	.00000	.00000	.0000	CALC	.494	8	0
25	.00000	.00000	.0000	CALC	.504	9	0
26	.00000	.00000	.0000	CALC	.513	8	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 415.581 SECONDS

DATE 062878 TIME 023215 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 37

MODEL=SAMPLE CONFIG=CASE5 STEP=10003
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10003 TRUE ANOMALY = 105.71977 TIME = .43111
++++ IN THE SUM +++++

NODE NUMBER	COMPUT	---DIRECT ALBEDO	INCID. FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS-- ALBEDO	PLAN	CP TIME (SECONDS)	---ELEMENTS-- PLAN	SURF	SHAD SURF
1	+++++	.000	.000	.000	.000	.000	.000	.001	0	8	0
2	+++++	.000	.000	.000	.000	.000	.000	.032	0	8	0
3	+++++	.000	.000	.000	.000	.000	.000	.037	0	8	0
4	+++++	.000	.000	.000	.000	.000	.000	.042	0	8	0
11	+++++	.000	.000	.000	.000	.000	.000	.046	0	8	0
12	+++++	.000	.000	.000	.000	.000	.000	.051	0	8	0
13	+++++	.000	.000	.000	.000	.000	.000	.056	0	8	0
14	+++++	.000	.000	.000	.000	.000	.000	.060	0	8	0
200	+++++	.000	.144+02	.000	.000	.000	.000	.065	0	8	0
21	+++++	.000	.742+02	.000	.000	.000	.000	.070	0	8	0
22	+++++	.000	.268+02	.000	.000	.000	.000	.075	0	8	0
23	+++++	.000	.264+02	.000	.000	.000	.000	.079	0	8	0
24	+++++	.000	.268+02	.000	.000	.000	.000	.084	0	8	0
25	+++++	.000	.264+02	.000	.000	.000	.000	.089	0	8	0
26	+++++	.000	.457+01	.000	.000	.000	.000	.094	0	8	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DICOMP

TOTAL ELAPSED TIME IN PROBLEM = 415.691 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO TAPE, LAST RESTART RECORD WRITTEN = 169

MODEL=SAMPLE CONFIO=CASE5 STEP=10004
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 :- FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

INPUT VALUE	DESCRIPTION	USER OPTIONS	DEFAULT VALUE	VARIABLE NAME
++++ BASIC CONTROL PARAMETERS +++++				
SHAD	SHADOWING OVERRIDE FLAG	SHAD,NOSH	SHAD	DINOSH
.250	PLANETARY ACCURACY FACTOR		0.25	DIACC
.100	SHADOWING ACCURACY FACTOR		0.10	DIACCS
10000	STEP NO. FOR PLANET-ORIENTED DATA		0	NSPFF
105.920	TRUE ANOMALY ANGLE, DEGREES		0.0	TRUEAN
.000	INITIAL TIME (AT PERIAPSIS)		0.0	TIMEST
++++ BASIC ORBIT DATA +++++				
.000	LONGITUDE OF ASCENDING NODE, DEGREES		0.0	ALAN
.000	ARGUMENT OF PERIFOCUS, DEGREES		0.0	APER
.000	ORBIT INCLINATION, DEGREES		0.0	OINC
.60800+06	ORBIT ALTITUDE AT PERIAPSIS		0.0	HP
.60800+06	ORBIT ALTITUDE AT APOAPSIS		0.0	HA
.000	ORBIT ECCENTRICITY		0.0	ECC
.000	SUN RA ANGLE, DEGREES		0.0	SUNRA
.000	SUN DEC ANGLE, DEGREES		0.0	SUNDEC
.000	REFERENCE STAR RA ANGLE, DEGREES		0.0	STRRA
.000	REFERENCE STAR DEC ANGLE, DEGREES		0.0	STRDEC
++++ PLANET-ORIENTED, ORIENTATION DATA +++++				
300.000	ROTATION ABOUT VCS X-AXIS TO CCS		0.0	ROTX
270.000	ROTATION ABOUT VCS Y-AXIS TO CCS		0.0	ROTY
.000	ROTATION ABOUT VCS Z-AXIS TO CCS		0.0	ROTZ
1 2 3	ROTATION ORDER -- IROTX,IROTY,IROTZ		1 2 3	
.359+03	SUN LOOK ANGLE - CLOCK, DEGREES		0.0	SUNCL
.104+03	SUN LOOK ANGLE - CONE, DEGREES		0.0	SUNCO
.000	PLANET LOOK ANGLE - CLOCK, DEGREES		0.0	PLCL
.180+03	PLANET LOOK ANGLE - CONE, DEGREES		0.0	PLCO
++++ SPIN DATA +++++				
.000	CLOCK ANGLE, DEGREES (ABOUT CCS Z-AXIS CCH=POSITIVE)		0.0	CLOCK
.000	CONE ANGLE, DEGREES		0.0	CONE
.000	ROTATION RATE- CCH POSITIVE		0.0	RATE
.000	TIME SPIN BEGINS		0.0	TIMSP

DATE 062078 TIME 023219 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 39

MODEL=SAMPLE CONFIO=CASE5 STEP=10004 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
DIRECT IRRADIATION CALCULATION LINK.

+++++ NSTEP NO = 10004

++++ COMPUTED OR INPUT ORBIT DATA +++++

VALUE	VARIABLE DESCRIPTION	***	VALUE	VARIABLE DESCRIPTION
60.000	SUN BETA ANGLE, DEGREES		.000	SUN CIGMA ANGLE, DEGREES
.000	STAR BETAS ANGLE, DEGREES		.900	STAR CIGMAS ANGLE, DEGREES

++++ PLANET --EARTH -- DATA +++++

VALUE	DESCRIPTION	NAME	***	VALUE	DESCRIPTION	NAME
.300	PLANET ALBEDO	PALB		.75073+02	PLANET DS EMISS POWER	WDS
.20900+08	PLANET RADIUS	PRAD		.75073+02	PLANET SS EMISS POWER	WSS
.14679+01	ORBIT PERIOD	PERIOD				
.41731+09	PLANET GRAV CONSTANT	GRAV		.42900+03	SOLAR CONSTANT AT PSD	SOL

DATE 062878 TIME 023220

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE5 STEP=10004
DIRECT IRRADIATION CALCULATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/ORBGEN/DRCAL/AOCAL/QOCAL

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10004 TRUE ANOMALY = 105.91977 TIME = .43193
++++ IN THE SHADE +++++

NODE NUMBER	DIRECT FLUX(QDS)	UNSHADOWED FLUX	SHADOW FACTOR	COMPUTATION	CP TIME (SECONDS)	SURFACE ELEMENTS	SHADOWING SURFACES
1	.00000	.00000	.0000	+++++	.000	0	0
2	.00000	.00000	.0000	+++++	.028	0	0
3	.00000	.00000	.0000	+++++	.033	0	0
4	.00000	.00000	.0000	+++++	.037	0	0
11	.00000	.00000	.0000	+++++	.041	0	0
12	.00000	.00000	.0000	+++++	.043	0	0
13	.00000	.00000	.0000	+++++	.050	0	0
14	.00000	.00000	.0000	+++++	.055	0	0
200	.00000	.00000	.0000	+++++	.059	0	0
21	.00000	.00000	.0000	+++++	.065	0	0
22	.00000	.00000	.0000	+++++	.070	0	0
23	.00000	.00000	.0000	+++++	.074	0	0
24	.00000	.00000	.0000	+++++	.079	0	0
25	.00000	.00000	.0000	+++++	.084	0	0
26	.00000	.00000	.0000	+++++	.088	0	0

NOTE--

FLUX VALUES FLAGGED (+++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP, OR FORCED TO ZERO IN DICOM

TOTAL ELAPSED TIME IN PROBLEM = 416.216 SECONDS

DATE 062070 TIME 023220

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC D VERSION PAGE 41

MODEL=SAMPLE CONFIG=CASE5 STEP=10004

SAMPLE CASE 5 - FFCAL/RBCAL/GSCAL/RKCAL/GABGEN/DRCAL/AQCAL/QOCAL

DIRECT IRRADIATION CALCULATION LINK.

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO. = 10004 TRUE ANOMALY = 105.91977 TIME = .43193
 **** IN THE SHADE ****

NODE NUMBER	COMPUT	---DIRECT INCID. ALBEDO	FLUX-- PLANETARY	---UNSHADOWED ALBEDO	FLUX--- PLANETARY	---SHADOW FACTORS--- ALBEDO	PLAN	CP TIME (SECONDS)	---ELEMENTS--- PLAN	SURF	SHAD SURF
1	++++++	.000	.000	.000	.000	.000	.000	.001	0	0	0
2	++++++	.000	.000	.000	.000	.000	.000	.032	0	0	0
3	++++++	.000	.000	.000	.000	.000	.000	.038	0	0	0
4	++++++	.000	.000	.000	.000	.000	.000	.043	0	0	0
11	++++++	.000	.000	.000	.000	.000	.000	.048	0	0	0
12	++++++	.000	.000	.000	.000	.000	.000	.052	0	0	0
13	++++++	.000	.000	.000	.000	.000	.000	.057	0	0	0
14	++++++	.000	.000	.000	.000	.000	.000	.064	0	0	0
200	++++++	.000	.144+02	.000	.000	.000	.000	.068	0	0	0
21	++++++	.000	.742+02	.000	.000	.000	.000	.073	0	0	0
22	++++++	.000	.269+02	.000	.000	.000	.000	.078	0	0	0
23	++++++	.000	.264+02	.000	.000	.000	.000	.084	0	0	0
24	++++++	.000	.268+02	.000	.000	.000	.000	.089	0	0	0
25	++++++	.000	.264+02	.000	.000	.000	.000	.097	0	0	0
26	++++++	.000	.457+01	.000	.000	.000	.000	.102	0	0	0

NOTE--

FLUX VALUES FLAGGED (++++++) MAY HAVE COME FROM RT1, THE FLUX DATA BLOCK, STUFFED FROM ANOTHER STEP OR FORCED TO ZERO IN DCOMP

TOTAL ELAPSED TIME IN PROBLEM = 416.333 SECONDS
 S.A.P. FLUXES HAVE BEEN WRITTEN TO REJ TAPE. LAST RESTART RECORD WRITTEN = 181

DATE 062878 TIME 023223 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 42
 MODEL=SAMPLE CONFIG=CASE5 STEP=10010 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEM/DRCAL/AQCAL/QOCAL
 DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 9 TRUE ANOMALY = .00000 TIME = .00000
 ++++ IN THE SUN ++++

NODE NUMBER	DIRECT FLUX (QDS)	DIRECT ABS. FLUX
1	.00000	.00000
2	.94028+02	.84625+02
3	.00000	.00000
4	.16512+03	.14861+03
11	.00000	.00000
12	.00000	.00000
13	.10055+02	.90492+01
14	.91734+02	.82561+02
200	.00000	.00000
21	.00000	.00000
22	.10725+03	.21450+02
23	.18576+03	.37152+02
24	.00000	.00000
25	.00000	.00000
26	.18687+03	.37374+02

TOTAL ELAPSED TIME IN PROBLEM = 416.676 SECONDS

DATE 062070 TIME 023223

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 43

MODEL=SAMPLE CONFIG=CASE5 STEP=10010

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO 9 TRUE ANOMALY = .00000 TIME = .00000
 ++++ IN THE SUN ++++

NODE NUMBER	COMPUT	---DIRECT INCID. FLUX-- ALBEDO	PLANETARY	---DIRECT ABS. FLUX--- ALBEDO	PLANETARY
1		.000	.000	.000	.000
2		.000	.000	.000	.000
3		.000	.000	.000	.000
4		.000	.000	.000	.000
11		.000	.000	.000	.000
12		.000	.000	.000	.000
13		.000	.000	.000	.000
14		.000	.000	.000	.000
200		.215+02	.144+02	.215+01	.144+01
21		.110+03	.742+02	.220+02	.868+02
22		.402+02	.268+02	.805+01	.241+02
23		.400+02	.264+02	.800+01	.238+02
24		.391+02	.268+02	.783+01	.241+02
25		.382+02	.264+02	.765+01	.238+02
26		.859+01	.457+01	.132+01	.411+01

TOTAL ELAPSED TIME IN PROBLEM = 418.757 SECONDS
 S.A.P FLUXES HAVE BEEN WRITTEN TO RSO. LAST RESTART RECORD WRITTEN = 184

DATE 062870 TIME 023224

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE5 STEP=10010

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBOEN/DRCAL/AQCAL/QOCAL

ABSORBED Q COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
IAQSDS	10010	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10010	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10010	CURRENT STEP NO	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

DATE 062070 TIME 023226

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS)

UNIVAC EXEC 8 VERSION

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MODEL=5SAMPLE CONFIO=CASE5 STEP=10010
 ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QOCAL

ABSORBED HEATING RATES FOR ORBIT POINT = 10010 TRUE ANOMALY = .0000 TIME = .0000
 UNITS ARE ENERGY PER UNIT TIME

++++ IN THE SUN +++++

NODE	SOLAR		ALBEDO		PLANETARY		TOTAL HEAT RATES	
	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL
1	.00000	.59530+01	.00000	.40089+00	.00000	.26715+00	.00000	.66210+01
2	.84625+02	.88420+02	.00000	.28120+00	.00000	.18739+00	.84525+02	.88897+02
3	.00000	.54750+01	.00000	.14461+00	.00000	.96367+01	.00000	.57160+01
4	.14861+03	.15002+03	.00000	.34009+00	.00000	.22717+00	.14861+03	.15139+03
11	.00000	.34174+01	.00000	.40089+00	.00000	.26715+00	.00000	.40854+01
12	.00000	.33593+01	.00000	.28120+00	.00000	.18739+00	.00000	.38279+01
13	.90492+01	.11836+02	.00000	.14461+00	.00000	.96367+01	.90492+01	.12127+02
14	.82561+02	.83356+02	.00000	.34009+00	.00000	.22717+00	.82561+02	.83824+02
200	.00000	.59547+00	.43066+01	.43126+01	.28712+01	.28739+01	.71753+01	.77819+01
21	.00000	.00000	.45564+02	.45574+02	.13765+03	.13765+03	.18302+03	.18302+03
22	.44196+02	.44196+02	.16542+02	.16552+02	.49744+02	.49744+02	.11052+03	.11052+03
23	.38653+02	.38653+02	.83275+01	.83275+01	.24746+02	.24746+02	.71727+02	.71727+02
24	.00000	.00000	.16131+02	.16131+02	.49668+02	.49668+02	.65799+02	.65799+02
25	.00000	.00000	.79547+01	.79547+01	.24746+02	.24746+02	.32701+02	.32701+02
26	.77005+02	.77005+02	.27165+01	.27165+01	.84736+01	.84736+01	.88195+02	.88195+02

TOTAL ELAPSED TIME IN PROBLEM = 417.183 SECONDS

ABSORBED Q STORED IN STEP 10010

TOTAL TIME TO COMPUTE ABSORBED Q .37

DATE 062878 TIME 023228 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 46
 MODEL=SAMPLE CONFIG=CASE5 STEP=10011 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
 DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 10 TRUE ANOMALY = 90.00000 TIME = .36701
 ++++ IN THE SUN ++++

NODE NUMBER	DIRECT FLUX (QDS)	DIRECT ABS. FLUX
1	.00000	.00000
2	.00000	.00000
3	.00000	.00000
4	.22877+03	.20589+03
11	.00000	.00000
12	.00000	.00000
13	.00000	.00000
14	.22877+03	.20589+03
200	.30335+03	.30335+02
21	.00000	.00000
22	.42900+03	.85800+02
23	.00000	.00000
24	.00000	.00000
25	.00000	.00000
26	.00000	.00000

TOTAL ELAPSED TIME IN PROBLEM = 417.856 SECONDS

DATE 062878 TIME 023229

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 47

MODEL=SAMPLE CONFIG=CASE5 STEP=10011

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/URDGEN/DRCAL/AQCAL/QOCAL

DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO 10 TRUE ANOHALY = 90.00000 TIME = .36701
 ++++ IN THE SUN ++++

NODE NUMBER	COMPUT	---DIRECT INCID. FLUX--		---DIRECT ABS. FLUX --	
		ALBEDO	PLANETARY	ALBEDO	PLANETARY
1		.000	.000	.000	.000
2		.000	.000	.000	.000
3		.000	.000	.000	.000
4		.000	.000	.000	.000
11		.000	.000	.000	.000
12		.000	.000	.000	.000
13		.000	.000	.000	.000
14		.000	.000	.000	.000
200		.120+01	.144+02	.120+00	.144+01
21		.143+01	.742+02	.285+00	.658+02
22		.206+01	.268+02	.412+00	.241+02
23		.638+00	.264+02	.128+00	.238+02
24		.000	.268+02	.000	.241+02
25		.634+00	.264+02	.127+00	.238+02
26		.000	.457+01	.000	.411+01

TOTAL ELAPSED TIME IN PROBLEM = 417.936 SECONDS

S.A.P FLUXES HAVE BEEN WRITTEN TO R.O. LAST RESTART RECORD WRITTEN = 193

DATE 062878 TIME 023230 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 40

MODEL=SAMPLE CONFIG=CASE5 STEP=10011 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/OMSGEN/DPCAL/AQCAL/QOCAL
ABSORBED Q COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10011	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10011	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10011	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

DATE 062070 TIME 023231

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS)

UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE5 STEP=10011

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

ABSORBED Q COMPUTATION LINK.

ABSORBED HEATING RATES FOR ORBIT POINT = 10011 TRUE ANOMALY = 90.0000 TIME = .3670.
UNITS ARE ENERGY PER UNIT TIME

++++ IN THE SUN +++++

NODE	SOLAR		ALBEDO		PLANETARY		TOTAL HEAT RATES	
	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL
1	.00000	.11533+02	.00000	.22339-01	.00000	.26715+00	.00000	.11822+02
2	.00000	.93697+01	.00000	.15569-01	.00000	.18739+00	.00000	.95727+01
3	.00000	.74731+01	.00000	.80580-02	.00000	.95367-01	.00000	.75775+01
4	.20589+03	.21117+03	.00000	.18995-01	.00000	.22717+00	.20589+03	.21142+03
11	.00000	.11533+02	.00000	.22339-01	.00000	.26715+00	.00000	.11822+02
12	.00000	.93697+01	.00000	.15569-01	.00000	.18739+00	.00000	.95727+01
13	.00000	.74731+01	.00000	.80579-02	.00000	.96367-01	.00000	.75775+01
14	.20589+03	.21117+03	.00000	.18995-01	.00000	.22717+00	.20589+03	.21142+03
200	.60670+02	.61530+02	.24009+00	.24031+00	.28712+01	.28739+01	.63781+02	.64645+02
21	.00000	.00000	.58914+00	.58914+00	.13765+03	.13765+03	.13824+03	.13824+03
22	.17678+03	.17678+03	.84940+00	.84940+00	.49744+02	.49744+02	.22737+03	.22737+03
23	.00000	.00000	.13273+00	.13273+00	.24746+02	.24746+02	.24879+02	.24879+02
24	.00000	.00000	.00000	.00000	.49660+02	.49660+02	.49660+02	.49660+02
25	.00000	.00000	.13197+00	.13197+00	.24746+02	.24746+02	.24878+02	.24879+02
26	.00000	.00000	.00000	.00000	.84736+01	.84736+01	.84736+01	.84736+01

TOTAL ELAPSED TIME IN PROBLEM = 418.357 SECONDS

ABSORBED Q STORED IN STEP 10011

TOTAL TIME TO COMPUTE ABSORBED Q .38

DATE 062070 TIME 023234 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 50

MODEL=SAMPLE CONFIG=CASE5 STEP=10012 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 11 TRUE ANOMALY = 180.00000 TIME = .73402
++++ IN THE SHADE +++++

NODE NUMBER	DIRECT FLUX (QDS)	DIRECT ABS. FLUX
1	.00000	.00000
2	.00000	.00000
3	.00000	.00000
4	.00000	.00000
11	.00000	.00000
12	.00000	.00000
13	.00000	.00000
14	.00000	.00000
200	.00000	.00000
21	.00000	.00000
22	.00000	.00000
23	.00000	.00000
24	.00000	.00000
25	.00000	.00000
26	.00000	.00000

TOTAL ELAPSED TIME IN PROBLEM = 419.134 SECONDS

DATE 062878 TIME 023235

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS)

UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE5 STEP=10012

SAMPLE CASE 5 - FFCAL/RBCAL/OBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO 11 TRUE ANOMALY = 180.00000 TIME = .73402
 +---+ IN THE SHADE +---+

NODE NUMBER	COMPUT	---DIRECT INCID. FLUX---		---DIRECT ABS. FLUX---	
		ALBEDO	PLANETARY	ALBEDO	PLANETARY
1		.000	.000	.000	.000
2		.000	.000	.000	.000
3		.000	.000	.000	.000
4		.000	.000	.000	.000
11		.000	.000	.000	.000
12		.000	.000	.000	.000
13		.000	.000	.000	.000
14		.000	.000	.000	.000
200		.000	.144+02	.000	.144+01
21		.000	.742+02	.000	.668+02
22		.000	.268+02	.000	.241+02
23		.000	.264+02	.000	.238+02
24		.000	.268+02	.000	.241+02
25		.000	.264+02	.000	.238+02
26		.000	.457+01	.000	.411+01

TOTAL ELAPSED TIME IN PROBLEM = 419.216 SECONDS

S.A.P FLUXES HAVE BEEN WRITTEN TO RSO. LAST RESTART RECORD WRITTEN = 202

DATE 062878 TIME 023236

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 52

MODEL=SAMPLE CONFIG=CASE5 STEP=10012

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

ABSORBED Q COMPUTATION LINK.

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10012	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10012	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10012	CURRENT STEP NO	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

DATE 062070 TIME 023230

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS)

UNIVAC EXEC 8 VERSION

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MODEL=SAMPLE CONFIG=CASE5 STEP=10012

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QOCAL

ABSORBED Q COMPUTATION LINK.

ABSORBED HEATING RATES FOR ORBIT POINT = 10012 TRUE ANOMALY = 180.0000 TIME = .7340
UNITS ARE ENERGY PER UNIT TIME

♦♦♦♦ IN THE SHADE ♦♦♦♦

NODE	SOLAR		ALBEDO		PLANETARY		TOTAL HEAT RATES	
	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL
1	.00000	.00000	.00000	.00000	.00000	.26715+00	.00000	.26715+00
2	.00000	.00000	.00000	.00000	.00000	.18739+00	.00000	.18739+00
3	.00000	.00000	.00000	.00000	.00000	.96367-01	.00000	.96367-01
4	.00000	.00000	.00000	.00000	.00000	.22717+00	.00000	.22717+00
11	.00000	.00000	.00000	.00000	.00000	.26715+00	.00000	.26715+00
12	.00000	.00000	.00000	.00000	.00000	.18739+00	.00000	.18739+00
13	.00000	.00000	.00000	.00000	.00000	.96367-01	.00000	.96367-01
14	.00000	.00000	.00000	.00000	.00000	.22717+00	.00000	.22717+00
200	.00000	.00000	.00000	.00000	.28712+01	.28739+01	.28712+01	.28739+01
21	.00000	.00000	.00000	.00000	.13765+03	.13765+03	.13765+03	.13765+03
22	.00000	.00000	.00000	.00000	.49744+02	.49744+02	.49744+02	.49744+02
23	.00000	.00000	.00000	.00000	.24746+02	.24746+02	.24746+02	.24746+02
24	.00000	.00000	.00000	.00000	.49668+02	.49668+02	.49668+02	.49668+02
25	.00000	.00000	.00000	.00000	.24746+02	.24746+02	.24746+02	.24746+02
26	.00000	.00000	.00000	.00000	.84736+01	.84736+01	.84736+01	.84736+01

TOTAL ELAPSED TIME IN PROBLEM = 419.666 SECONDS

ABSORBED Q STORED IN STEP 10012

TOTAL TIME TO COMPUTE ABSORBED Q .40

DATE 062878 TIME 023241 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 54
 MODEL=SAMPLE CONFIG=CASE5 STEP=10013 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
 DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 12 TRUE ANOMALY = 105.71977 TIME = .43111
 ++++ IN THE SUN ++++

NODE NUMBER	DIRECT FLUX (QDS)	DIRECT ABS. FLUX
1	.40259+02	.36233+02
2	.37050+01	.33345+01
3	.00000	.00000
4	.18529+03	.16676+03
11	.40259+02	.36233+02
12	.00000	.00000
13	.00000	.00000
14	.18529+03	.16676+03
200	.24401+03	.24401+02
21	.10066+03	.20132+02
22	.41696+03	.83393+02
23	.69478+01	.13896+01
24	.00000	.00000
25	.00000	.00000
26	.00000	.00000

TOTAL ELAPSED TIME IN PROBLEM = 420.637 SECONDS

DATE 062978 TIME 023241

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 55

MODEL=SAMPLE CONFIG=CASE5 STEP=10013

SAMPLE CASE 5 - FFCAL/RBCAL/QBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO 12 TRUE ANOMALY = 105.71977 TIME = .43111
 +---+ IN THE SUN +---+

NODE NUMBER	COMPUT	---DIRECT INCID FLUX-- ALBEDO	PLANETARY	---DIRECT ABS. FLUX--- ALBEDO	PLANETARY
1		.000	.000	.000	.000
2		.000	.000	.000	.000
3		.000	.000	.000	.000
4		.000	.000	.000	.000
11		.000	.000	.000	.000
12		.000	.000	.000	.000
13		.000	.000	.000	.000
14		.000	.000	.000	.000
200		.000	.144+02	.000	.144+01
21		.000	.742+02	.000	.668+02
22		.000	.268+02	.000	.241+02
23		.000	.264+02	.000	.238+02
24		.000	.263+02	.000	.241+02
25		.000	.264+02	.000	.238+02
26		.000	.457+01	.000	.411+01

TOTAL ELAPSED TIME IN PROBLEM = 420.706 SECONDS
 S.A.P FLUXES HAVE BEEN WRITTEN TO RSO. LAST RESTART RECORD WRITTEN = 211

DATE 082078 TIME 023243

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 56

MODEL=SAMPLE CONFIG=CASE5 STEP=10013
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
1AQSDS	10013	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
1AQSDA	10013	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
1AQSDP	10013	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

DATE 062876 TIME 023244 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 57

MODEL=SAMPLE CONFIG=CASE5 STEP=10013 SAMPLE CASE 5 - FFCAL/RBCAL/GDCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL
 ABSORBED Q COMPUTATION LINK.

ABSORBED HEATING RATES FOR ORBIT POINT = 10013 TRUE ANOMALY = 105.7198 TIME = .4311
 UNITS ARE ENERGY PER UNIT TIME

++++, IN THE SUN +++++

NODE	SOLAR		ALBEDO		PLANETARY		TOTAL HEAT RATES	
	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL
1	.36233+02	.46055+02	.00000	.00000	.00000	.26715+00	.36233+02	.46322+02
2	.33345+01	.11970+02	.00000	.00000	.00000	.18739+00	.33345+01	.12157+02
3	.00000	.72246+01	.00000	.00000	.00000	.96367-01	.00000	.73210+01
4	.16676+03	.17212+03	.00000	.00000	.00000	.22717+00	.16676+03	.17235+03
11	.36233+02	.45996+02	.00000	.00000	.00000	.26715+00	.36233+02	.46264+02
12	.00000	.86579+01	.00000	.00000	.00000	.18739+00	.00000	.86453+01
13	.00000	.71652+01	.00000	.00000	.00000	.96367-01	.00000	.72615+01
14	.16676+03	.17206+03	.00000	.00000	.00000	.22717+00	.16676+03	.17229+03
200	.48802+02	.49671+02	.00000	.00000	.28712+01	.28739+01	.51673+02	.52545+02
21	.41479+02	.41479+02	.00000	.00000	.13765+03	.13765+03	.17913+03	.17913+03
22	.17182+03	.17182+03	.00000	.00000	.49744+02	.49744+02	.22157+03	.22157+03
23	.14457+01	.14457+01	.00000	.00000	.24746+02	.24746+02	.26192+02	.26192+02
24	.00000	.00000	.00000	.00000	.49668+02	.49668+02	.49668+02	.49668+02
25	.00000	.00000	.00000	.00000	.24746+02	.24746+02	.24746+02	.24746+02
26	.00000	.00000	.00000	.00000	.84736+01	.84736+01	.84736+01	.84736+01

TOTAL ELAPSED TIME IN PROBLEM = .421.143 SECONDS

ABSORBED Q STOPPED IN STEP 10013

TOTAL TIME TO COMPUTE ABSORBED Q .39

DATE 062870 TIME 023247 THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 0 VERSION PAGE 50

MODEL=SAMPLE CONFIG=CASE5 STEP=10014 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORDGEN/ORCAL/AOCAL/QOCAL
DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

SOLAR DIRECT INCIDENT FLUX FOR STEP NO 13 TRUE ANOMALY = 105.91977 TIME = .43193
++++ IN THE SHADE +++++

NODE NUMBER	DIRECT FLUX (QDS)	DIRECT ABS. FLUX
1	.40758+02	.36683+02
2	.37993+01	.34194+01
3	.00000	.00000
4	.18515+03	.16664+03
11	.40758+02	.36682+02
12	.00000	.00000
13	.00000	.00000
14	.18515+03	.16664+03
200	.00000	.00000
21	.00000	.00000
22	.00000	.00000
23	.00000	.00000
24	.00000	.00000
25	.00000	.00000
26	.00000	.00000

TOTAL ELAPSED TIME IN PROBLEM = 422.062 SECONDS

DATE 062879 TIME 0232:7

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 59

MODEL=SAFPLE CONFIG=CASE5 STEP=10014 SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RNCAL/ORBGGEN/DRCAL/AQCAL/QOCAL
DIRECT IRRADIATION CALCULATION WITH SPECULAR SURFACES.

ALBEDO AND PLANETARY DIRECT INCIDENT FLUXES FOR STEP NO 13 TRUE ANOMALY = 105.91977 TIME = .43193
++++ IN THE SHADE +++++

NODE NUMBER	COMPUT	---DIRECT INCID. FLUX-- ALBEDO	PLANETARY	---DIRECT ABS. FLUX--- ALBEDO	PLANETARY
1		.000	.000	.000	.000
2		.000	.000	.000	.000
3		.000	.000	.000	.000
4		.000	.000	.000	.000
11		.000	.000	.000	.000
12		.000	.000	.000	.000
13		.000	.000	.000	.000
14		.000	.000	.000	.000
200		.000	.144+02	.000	.144+01
21		.000	.742+02	.000	.668+02
22		.000	.268+02	.000	.241+02
23		.000	.264+02	.000	.238+02
24		.000	.268+02	.000	.241+02
25		.000	.264+02	.000	.238+02
26		.000	.457+01	.000	.411+01

TOTAL ELAPSED TIME IN PROBLEM = 422.137 SECONDS
S.A.P FLUXES HAVE BEEN WRITTEN TO RSO. LAST RESTART RECORD WRITTEN = 220

DATE 052878 TIME 023249

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION

PAGE 60

MODEL=SAMPLE CONFIG=CASE5 STEP=10014
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEM/DRCAL/AQCAL/QOCAL

VARIABLE NAME	CURRENT VALUE	DEFAULT	ABSORBED HEAT DEFINITION	OPTIONS
IAQSDS	10014	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR SOLAR DI	N/A
IAQSDA	10014	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR ALBEDO DI	N/A
IAQSDP	10014	CURRENT STEP NO.	STEP NUMBER REFERENCE FOR PLANETARY DI	N/A

DATE 062878 TIME 023250

THERMAL RADIATION ANALYSIS SYSTEM (TRADYS)

UNIVAC EXEC 8 VERSION

PAGE , 61

MODEL=SAMPLE CONFIG=CASE5 STEP=10014
ABSORBED Q COMPUTATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

ABSORBED HEATING RATES FOR ORBIT POINT = 10014 TRUE ANOMALY = 105.9198 TIME = .4319
UNITS ARE ENERGY PER UNIT TIME

*** IN-THE SHADE ***

NODE	SOLAR		ALBEDO		PLANETARY		TOTAL HEAT RATES	
	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL	DIRECT	TOTAL
1	.36683+02	.41968+02	.00000	.00000	.00000	.26715+00	.36683+02	.42235+02
2	.34194+01	.88797+01	.00000	.00000	.00000	.18739+00	.34194+01	.90571+01
3	.00000	.55391+01	.00000	.00000	.00000	.96367-01	.00000	.56955+01
4	.16664+03	.16815+03	.00000	.00000	.00000	.22717+00	.16664+03	.16838+03
11	.36682+02	.41907+02	.00000	.00000	.00000	.26715+00	.36682+02	.42174+02
12	.00000	.54836+01	.00000	.00000	.00000	.18739+00	.00000	.56710+01
13	.00000	.55381+01	.00000	.00000	.00000	.96357-01	.00000	.56345+01
14	.16664+03	.16809+03	.00000	.00000	.00000	.22717+00	.16664+03	.16872+03
200	.00000	.82513+00	.00000	.00000	.28712+01	.28739+01	.28712+01	.30010+01
21	.00000	.00000	.00000	.00000	.13765+03	.13765+03	.13765+03	.13765+03
22	.00000	.00000	.00000	.00000	.49744+02	.49744+02	.49744+02	.49744+02
23	.00000	.00000	.00000	.00000	.24746+02	.24746+02	.24746+02	.24746+02
24	.00000	.00000	.00000	.00000	.49668+02	.49668+02	.49668+02	.49668+02
25	.00000	.00000	.00000	.00000	.24746+02	.24746+02	.24746+02	.24746+02
26	.00000	.00000	.00000	.00000	.84736+01	.84736+01	.84736+01	.84736+01

TOTAL ELAPSED TIME IN PROBLEM = 422.592 SECONDS

ABSORBED Q STORED IN STEP 10014

TOTAL TIME TO COMPUTE ABSORBED Q .41

DATE 062878 TIME 023252

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 62

MODEL=SAMPLE CONFIG=CASE5 STEP=10014
 ABSORBED Q OUTPUT COMPUTATION LINK.

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

VARIABLE NAME	CURRENT VALUE	DEFAULT	DEFINITION	OPTIONS
IQOTHE	1	1	TIME ARRAY ID NUMBER FLUX TABLES START AT IQOTHE + 1	N/A
QOTAPE	NO	2HNO	PARAMETER TO OUTPUT TO BCD TAPE	(4HTAPE,2HNO)
QOPNCH	NO	2HNO	PUNCH/NO PUNCH PARAMETER FOR OUTPUT	(3HPUN,2HNO)
QOAMPF	1.0000	1.0	AREA MULTIPLYING FACTOR	N/A
QOFMPF	1.0000	1.0	FLUX MULTIPLYING FACTOR	N/A
QOTMPF	1.0000	1.0	TIME MULTIPLYING FACTOR	N/A
QOTYPE	BOTH	NONE	PARAMETER TO DETERMINE TYPE OF OUTPUT	(3HTAB,2HAV,4HBOTH)
IQOARY	ALL	NONE	STEP NO. ARRAY DIRECTIVE	(3HALL,ARRAY NAME)

DATE 062878 TIME 023253

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS)

UNIVAC EXEC 8 VERSION

PAGE . 63

MODEL=SAMPLE CONFIG=CASE5 STEP=10014

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QOCAL

ABSORBED Q OUTPUT COMPUTATION LINK.

ABSORBED HEAT RATE TABLES PUNCHED

Q = INPUT * RMPF WHERE RMPF = .10000+01
 TIME = INPUT * TMPF WHERE TMPF = .10000+01
 AREA IS ON SUBROUTINE CALL CARDS

```

1$ TIME ARRAY
.000 . .367+00. .431+00. .432+00. .734+00
END$
2$ HEAT RATE ARRAY
.662+01. .118+02. .463+02. .422+02. .267+00
END$
3$ HEAT RATE ARRAY
.889+02. .957+01. .122+02. .907+01. .187+00
END$
4$ HEAT RATE ARRAY
.572+01. .758+01. .732+01. .570+01. .964-01
END$
5$ HEAT RATE ARRAY
.151+03. .211+03. .172+03. .168+03. .227+00
END$
6$ HEAT RATE ARRAY
.409+01. .118+02. .463+02. .422+02. .267+00
END$
7$ HEAT RATE ARRAY
.383+01. .957+01. .885+01. .567+01. .187+00
END$
8$ HEAT RATE ARRAY
.121+02. .758+01. .726+01. .563+01. .964-01
END$
9$ HEAT RATE ARRAY
.839+02. .211+03. .172+03. .168+03. .227+00
END$
10$ HEAT RATE ARRAY
.778+01. .646+02. .525+02. .370+01. .287+01
END$
11$ HEAT RATE ARRAY
.183+03. .138+03. .179+03. .138+03. .138+03
END$
12$ HEAT RATE ARRAY
.111+03. .227+03. .222+03. .497+02. .497+02
END$
13$ HEAT RATE ARRAY
.717+02. .249+02. .262+02. .247+02. .247+02
END$
  
```

DATE 062078 TIME 023254

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 64

MODEL=SAMPLE CONFIG=CASE5 STEP=10014

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBGEN/DRCAL/AQCAL/QOCAL

ABSORBED Q OUTPUT COMPUTATION LINK.

ABSORBED HEAT RATE TABLES PUNCHED

Q = INPUT * RMPF WHERE RMPF = .10000+01
TIME = INPUT * THPF WHERE THPF = .10000+01
AREA 'S ON SUBROUTINE CALL CARDS

14\$ HEAT RATE ARRAY
.658+02. .497+02. .497+02. .497+02. .497+02
END\$
15\$ HEAT RATE ARRAY
.327+02. .249+02. .247+02. .247+02. .247+02
END\$
16\$ HEAT RATE ARRAY
.882+02. .847+01. .847+01. .847+01. .847+01
END\$

DATE 062878 TIME 023254

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC D VERSION PAGE 65

MODEL= SAMPLE CONFIG=CASE5 STEP=10014

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QDCAL

ABSORBED Q OUTPUT COMPUTATION LINK.

DA11HC SUBROUTINE CALL CARDS

```
AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000+01
DA11HC(1.46792175E 0.TIMEN,A1 .A2 .1.00000000E 0.Q1 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A3 .1.00000000E 0.Q2 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A4 .1.00000000E 0.Q3 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A5 .1.00000000E 0.Q4 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A6 .1.00000000E 0.Q11 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A7 .1.00000000E 0.Q12 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A8 .1.00000000E 0.Q13 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A9 .1.00000000E 0.Q14 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A10 .1.00000000E 0.Q200 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A11 .1.00000000E 0.Q21 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A12 .1.00000000E 0.Q22 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A13 .1.00000000E 0.Q23 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A14 .1.00000000E 0.Q24 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A15 .1.00000000E 0.Q25 )$
DA11HC(1.46792175E 0.TIMEN,A1 .A16 .1.00000000E 0.Q26 )$
```

DATE 062970 TIME 023254

THERMAL RADIATION ANALYSIS SYSTEM (TRASYS) UNIVAC EXEC 8 VERSION PAGE 66

MODEL=SAMPLE CONFIG=CASE5 STEP=10014

SAMPLE CASE 5 - FFCAL/RBCAL/GBCAL/RKCAL/ORBCEN/DRCAL/AQCAL/QOCAL

ABSORBED Q OUTPUT COMPUTATION LINK.

AVERAGE ORBITAL HEATING RATE AND AREA CARDS PUNCHED

VALUES ARE RATE = INPUT (UNITS) * RMPF WHERE RMPF = .10000+01
VALUES ARE AREA = INPUT (UNITS) * AMPF WHERE AMPF = .10000+01

Q1 =1.59449475E 1
Q2 =2.74823542E 1
Q3 =5.17319250E 0
Q4 =1.42343797E 2
Q11 =1.52960157E 1
Q12 =5.36798030E 0
Q13 =6.76049656E 0
Q14 =1.25462862E 2
Q200 =2.46076262E 1
Q21 =1.51001135E 2
Q22 =1.24700516E 2
Q23 =3.65944627E 1
Q24 =5.37007242E 1
Q25 =2.67737916E 1
Q26 =2.04939971E 1

TOTAL TIME TO COMPUTE ABSORBED Q OUT .52

NORMAL TERMINATION BY PROCESSOR

8PHD.FLE8

8BRKPT PRINTS